# Appendix C Geotechnical Design Analysis

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### **ATTACHMENTS**

Attachment A Subsurface Investigation Program and Field Logs

Attachment B Geotechnical Laboratory Testing

Attachment C Supplemental Geotechnical Information by Others

### **ABBREVIATIONS**

ARCS Assessment and Remediation of Contaminated Sediments

BODR Basis of Design Report
CPT cone penetrometer test

CR compression ratio

DER Pre-Design Investigation Data Evaluation Report

EAA early action area

ENR enhanced natural recovery

EPA U.S. Environmental Protection Agency

FFP full-flow penetrometer
FNC federal navigation channel

ft<sup>2</sup> square foot

GWT groundwater table elevation

H:V horizontal to vertical kip one thousand pounds lb/ft pounds per foot

ib/it pounds per root

LDW Lower Duwamish Waterway

LTMMP Long-Term Maintenance and Monitoring Plan

MHHW mean higher high water
MLLW mean lower low water

N/A not applicable

pcf pounds per cubic foot
pci pounds per cubic inch
PDI Pre-Design Investigation
PGA peak ground acceleration
psf pounds per square foot
RAL remedial action level
RD remedial design

RM river mile

ROD Record of Decision

SPT standard penetration test
USACE U.S. Army Corps of Engineers

USGS U.S. Geological Survey VST vane shear testing



### 1 Introduction

This *Geotechnical Design Analysis* presents the results of the geotechnical engineering evaluation performed by Anchor QEA, LLC, to determine the basis of design for the upper reach (river miles [RMs] 3.0 to 5.0) of the Lower Duwamish Waterway (LDW) Superfund Site in King County, Washington. The remedial actions associated with the upper reach include dredging and, potentially, capping of areas within the waterway, including areas that have waterfront or overwater structures; placing thin cover of clean material for enhanced natural recovery (ENR); and backfilling dredge areas within elevation ranges that support habitat as described in the Intermediate (60%) Remedial Design (RD) *Basis of Design Report* (BODR) to which this *Geotechnical Design Analysis* is an appendix.

### 1.1 Locations Studied

The proposed work requires remediation within the actively managed federal navigation channel (FNC), areas adjacent to waterfront and offshore structures, and early action areas (EAAs) over a range of subtidal and intertidal elevations. Subtidal areas are defined as areas below elevation -4 feet mean lower low water (MLLW). Intertidal areas represent elevations between -4 feet MLLW and the mean higher high water line (MHHW; equal to +11.4 feet MLLW), which horizontally defines the limit of sediment cleanup actions in the upper reach. The MHHW line occurs along sloped embankments or vertical bulkheads. Upland areas are locations above MHHW that abut and include shoreline property where buildings and structures may be encountered.

# 1.2 Report Structure

This Geotechnical Design Analysis includes the following six main sections:

- Section 1 is the introduction.
- Section 2 discusses the subsurface conditions underlying the site in more detail than
  presented in the *Pre-Design Investigation Data Evaluation Report* (DER) (Anchor QEA and
  Windward 2022); this section also describes the soil engineering parameters assigned to the
  major stratigraphic units.
- Section 3 describes the geotechnical engineering analyses performed for each of the following design elements:
  - Dredge prism side slope stability
  - Bank side slope stability
  - Prospective cap bearing capacity and settlement evaluations
  - Backfill design
- Section 4 presents geotechnical engineering recommendations to be used by the structural engineer for the assessment of the following:
  - Bulkhead design, including lateral earth pressures and tieback design soil parameters

- Pile design, including vertical and lateral pile capacity
- Section 5 discusses seismic (earthquake) evaluations for the site.
- Section 6 presents references that were used to support this work.

Attachments to this Geotechnical Design Analysis include the following:

- Attachment A Subsurface Investigation Program and Field Logs
- Attachment B Geotechnical Laboratory Testing
- Attachment C Supplemental Geotechnical Information by Others

### 2 Subsurface Geotechnical Conditions

Subsurface geotechnical conditions at the site were investigated by Anchor QEA to supplement the existing geotechnical information that was collected during past projects in the vicinity of the upper reach. Details regarding these prior investigations can be found in the DER (Anchor QEA and Windward 2022).

Subsurface geotechnical conditions in the upper reach of the LDW were investigated by Anchor QEA as part of the Phase I and Phase II Pre-Design Investigation (PDI) efforts completed in 2021 and 2022. The geotechnical PDI included the following numbers and types of geotechnical investigations, which were advanced to a range of depths below ground surface:

- 29 rotosonic borings
- 20 cone penetrometer tests (CPTs)
- 5 vane shear tests (VSTs)
- 7 full-flow penetrometer (FFP) tests
- 2 hand auger borings
- 2 dynamic CPTs

The locations of these geotechnical investigations are presented in Figures C1-1a and C1-1b. Logs from these investigations are presented in Attachment A, and geotechnical laboratory testing results are presented in Attachment B.

The scope of the geotechnical PDI was developed considering existing geotechnical information within the upper reach. Studies by others provide supplemental subsurface geotechnical data in upland areas adjacent to the upper reach and at in-water locations. Attachment C presents the locations with supplemental geotechnical information and lists the studies that have been identified as providing useful subsurface geotechnical data in the upper reach.

The following sections provide a more comprehensive discussion of subsurface conditions encountered at the site than is presented in the DER.

# 2.1 Subsurface Stratigraphy

BODR Section 8.2 summarizes the stratigraphy. The following section provides more detailed information on the geotechnical properties for the three major stratigraphic units described in the DER (Anchor QEA and Windward 2022) and BODR for the purposes of geotechnical engineering design and analysis later described in this report.

### 2.1.1 Fill

Fill soils were encountered at two locations during the Phase II PDI and at several other upland locations investigated by others. The specific geologic interpretation of fill is indicated on historical boring logs from Boeing Plant 2, both the east and west banks at the South Park Bridge, and at several properties that are not adjacent to remedial action level (RAL) exceedance areas (e.g., near RM 3.0 west and between RMs 3.5 and 3.6 west at Terminal 117). Given the river history of channelization, fill is likely present along many banks of the upper reach that have not been geotechnically investigated.

Generally, the fill material had been placed to regrade the existing fluvial plain created by the Duwamish River to support shoreline development and re-channelization of the LDW. The unit weight of this material is assumed to vary, but, to prepare design recommendations, the material is assumed to be conservatively represented by an overall average value of 135 pounds per cubic foot (pcf) based on laboratory direct shear test results. Grain size distribution tests show that this material is predominately sand with varying amounts of silt. In areas where fill was more randomly placed, it would be expected to contain anthropogenic materials such as debris, which would be typical of historical shoreline development filling activities in active industrial areas. The moisture content in the fill unit generally ranges from 6% to 28%. Direct shear testing of the fill indicates a peak friction angle average of 36 degrees and a residual friction angle average of 33 degrees.

The findings associated with the two upland borings completed in 2021 are in general agreement with historical investigations completed by others.

### 2.1.2 Recent Sediments

Recent sediments are defined as material that has deposited on top of the alluvium layer and are distinctly characterized by finer gradation and soft consistency compared to the alluvium layer below. Recent sediments were encountered throughout the intertidal and subtidal areas, having been naturally deposited by flows to the LDW upper reach from Green River upstream. The thickness of this unit across the site varies widely and is observed to be thickest in areas of historical dredge activities.

Based on a review of laboratory testing results, a total unit weight of 100 pcf was assumed to best represent average overall conditions, with percent moisture content ranging from 34% to 97%. Atterberg limits (plasticity) testing indicates that this material is typically non-plastic to very low plasticity, an indication that the finer fractions are predominantly silt rather than clay. Direct shear testing indicates a peak friction angle of 34 degrees for the recent sediments and a residual friction angle of 33 degrees, whereas VST and FFP testing indicate undrained shear strengths ranging as shown in Figure C2-1. Grain size analyses indicate that this material is approximately 30% sand and 70% silt and clay, with silt content ranging from 22% to 62% and clay content ranging from 2% to 7%.

### 2.1.3 Alluvium

Investigations prior to the PDI describe the alluvium by referencing an upper alluvium unit and a lower alluvium unit. Because the distinction between the upper alluvium and lower alluvium is not important in the context of the sediment cleanup, in the DER, the description of the alluvium was simplified by combining the upper alluvium and lower alluvium into a single alluvium unit, recognizing that there are some gradational changes in the alluvium with depth (Anchor QEA and Windward 2022). Alluvium was observed to underly the recent sediments and be predominately coarse-grained material with pockets, lenses, and layers of silt and clay. Silt content of the fine-grained layers was as high as 76%, and clay content was as high as 16%; silt and clay content was observed to be as low as 1.5%. The alluvium unit has a typical specific gravity of 2.5 to 2.7; is non-plastic; and has a typical total unit weight of 125 pcf, a measured peak friction angle ranging from 32 to 40 degrees (average 37 degrees), and a measured residual friction angle ranging from 28 to 37 degrees (average 32 degrees).

### 2.2 Groundwater and Surface Water Elevations

Groundwater and surface water affect the geotechnical behavior of soils and sediments. Water surface elevations are used in geotechnical engineering evaluations to calculate porewater pressures and effective stresses, which govern the shear strength of soils. Changes in effective stress (which occur due to changes in porewater pressure) also lead to consolidation settlement. Thus, water surface elevations are a key input parameter for geotechnical engineering evaluations. This section summarizes general observations of groundwater and surface water levels made during the geotechnical investigation and as summarized in other reports.

### 2.2.1 Groundwater

Groundwater has been observed in shoreline groundwater wells along the upper reach. At locations nearest the LDW, groundwater elevations vary regularly in accordance with the water level in the river. Farther from the shoreline, groundwater levels are less affected by the adjacent surface water level but are still expected to vary seasonally. Table C2-1 summarizes typically observed groundwater levels at selected locations along the upper reach for exploration locations adjacent to the LDW, which are used as a basis for geotechnical engineering evaluations described in this report.

Table C2-1
Summary of Selected Groundwater Levels for Exploration Locations Adjacent to the LDW

Location	River Mile	Observed Groundwater Elevation Range (feet MLLW)	Observed Depth to Groundwater Range Below Ground Surface (feet)	Reference
Boeing Plant 2	2.9 E	7 to 11	6 to 11.5	AMEC 2012
Boeing Isaacson/Thompson	3.8 E	3 to 10	11 to 17	Landau and AMEC 2014
Terminal 117	3.6 W	8 to 10	3 to 20	GeoEngineers 2014
Dallas Avenue Drainage Project	3.6 W	8	10	SPU 2014
Delta Boat Lift	4.2 W	8	7	AMEC 2002
SPU Duwamish Substation	4.5 W	6 to 8	10 to 12	SPU 2012

Note:

MLLW: mean lower low water SPU: Seattle Public Utilities

### 2.2.2 Surface Water

The upper reach is tidally influenced, and water levels are also affected by inflows from Green River upstream. Upstream inflows are controlled by the Howard Hansen Dam, so tidal influences tend to dominate the river stage (surface water elevation) on a daily basis. In the project vertical datum, the MHHW elevation is 11.3 feet, and the MLLW elevation is 0 feet.

# 2.3 Soil Engineering Modeling Parameters

This section summarizes the geotechnical engineering properties that were assigned to each lithologic unit for geotechnical evaluations. Engineering properties were derived using correlations to in situ CPT results, VST results, FFP test results, and geotechnical laboratory testing results. For cap aggregates, habitat materials, and backfill, engineering parameters were assigned using best professional judgment and from past project experience considering the method of placement (under water) and the typical materials used for these applications (sand and gravel). Soil parameters are presented in Table C2-2.

Table C2-2
Soil Parameters for Slope Stability Analysis of Dredge Prism Side Slopes

		Undrained Shear Strength <sup>1</sup>		Drained Shear Strength		Compressibility
Soil Layer	Total Unit Weight (pcf)	Cohesion (psf)	Internal Friction Angle, φ΄ (degrees)	Cohesion (psf)	Internal Friction Angle, φ΄ (degrees)	Compression Ratio (unitless)
Fill	135	N/A	N/A	0	33	See Note 2
Recent sediments	100	10+38*Z; ≤200	0	0	27	0.17
Alluvium	125	100+30*Z; ≤1800	0	0	32	0.09
Cap, habitat and backfill materials	110	N/A	N/A	0	32	See Note 2
Armor Rock	135	N/A	N/A	0	40	See Note 2

#### Notes:

- 1. Z = depth below top of layer surface elevation
- 2. The fill, cap, habitat, backfill, and armor rock materials, being primarily granular, were not considered compressible for purposes of consolidation calculations. See discussion of compressibility.

N/A: not applicable. See discussion of Undrained Shear Strength.

pcf: pounds per cubic foot

psf: pounds per square foot

# 2.3.1 Undrained Shear Strength

Undrained shear strength can be directly estimated from the tip resistance measured during advancement of the cone during CPT and FFP testing, allowing for a near-continuous relationship of undrained shear strength versus depth (Robertson and Cabal 2010). For the proposes of this report, undrained shear strength values were determined by inspection of the FFP test and VST results at each location. This inspection was completed by plotting undrained shear strength with depth.

Figure C2-1 presents the measured undrained shear strength with depth. Analysis of this plot shows that the undrained shear strength for the recent sediments, as well as for the compressible layers within the alluvium, increases linearly with depth. Thus, the design assumes undrained shear strength is variable, as presented in Table C2-2. Undrained shear strength is not relevant for cohesionless materials (e.g., sand and gravel), which rely on inter-particle friction to develop strength. Thus, the undrained shear strength for sand and gravel type materials (fill, cap, habitat, and backfill) is not applicable because these materials are not expected to behave in an undrained manner.

### 2.3.2 Drained Shear Strength

Drained shear strength applies to the long-term behavior of fine-grained materials and both the short- and long-term behavior of granular materials, which drain very rapidly under applied loads. Drained shear strength can be correlated to in situ tests (e.g., standard penetration test blow counts, CPT records) and can be measured in laboratory geotechnical tests.

For this project, a series of direct shear tests was conducted on representative undisturbed samples from each major stratigraphic unit to evaluate drained shear strength behavior in terms of peak and residual friction angles. In general, average peak friction angles ranged from 34 to 37 degrees, and average residual friction angles ranged from 32 to 33 degrees.

Laboratory testing is conducted under ideal conditions and reflects assumed loading rates and drainage conditions that potentially will not apply under full-scale conditions. It is expected that actual soil behavior will be more variable and reflect inherent uncertainty that cannot be captured by laboratory testing alone. Thus, the laboratory test results were reviewed by an experienced geotechnical engineer, who applied engineering judgment to reduce the friction angle (drained shear strength) selected for design to reflect values more typically used regionally in engineering design. See Table C2-2 for a summary of friction angles that were selected for design for each major geologic unit.

## 2.3.3 Compressibility

Consolidation settlement (i.e., compression) occurs over time as new loads are applied to fine-grained soil or sediment and as water is driven out of the soil/sediment pore space due to the applied loading (i.e., drainage).

Compressibility parameters were assessed using the laboratory one-dimensional oedometer consolidation test. The test incrementally loads an undisturbed sample and measures the corresponding settlement, which is plotted as a relationship between stress (load) and strain (settlement). When stress is plotted in log scale and strain in natural scale, the resulting plot is generally linear over the range of virgin compression, and the slope of this line is referred to as the Compression Ratio. The Compression Ratio can be used to calculate anticipated consolidation under load.

Four oedometer tests were conducted: one in the recent sediment unit, two within the sandy alluvium, and one in the silty alluvium. The results of these tests were evaluated to develop the consolidation parameters summarized in Table C2-2.

The time rate of consolidation is affected by the distance that water must travel when drainage is occurring. Through inspection of the CPT porewater pressure profiles, a maximum drainage path



 $(H_{dr})$  length of 3.5 feet was determined. Lastly, for the purposes of the analysis for this project, a design coefficient of consolidation of 0.08 square feet (ft<sup>2</sup>) per day was assumed.

# 3 Geotechnical Engineering Analysis

This section discusses the following geotechnical engineering analyses prepared in support of the RD:

- Dredge prism side slope stability
- Bank excavation slope stability
- Cap bearing capacity and settlement

### 3.1 General Dredge Prism Side Slope Stability

Dredge prism side slope stability was evaluated using limit equilibrium methods and confirmed using an alternate method. This section describes the evaluation of dredge prism side slope stability including the following:

- Limit equilibrium model background
- Limit equilibrium model development
- Limit equilibrium method model results
- Alternative method model background, development, and results

### 3.1.1 Limit Equilibrium Model Background

The stability of dredge prism side slopes was evaluated using Rocscience Slide2 limit equilibrium software model. For a given evaluation, a geologic cross section was developed, and soil layers and soil geotechnical engineering parameters were input into the model.

The limit equilibrium model software calculates load (soil stress) and resistance (soil strength) for numerous trial "slip surface" geometries to generate a factor of safety for each trial slip surface. The slip surface with the lowest factor of safety is considered the "critical" slip surface for a particular stability cross section. Slip surfaces are generated using an automated search routine within the software so that an appropriate number of trial surfaces are checked when identifying the critical slip surface. The calculation method (General Limit Equilibrium) satisfies both force and moment equilibrium for each trial slip surface.

Acceptable (i.e., target) factors of safety are as follows, in accordance with a common U.S. Army Corps of Engineers (USACE) reference for slope stability (USACE 2003):

- Short-term 1.3 or greater
- Long-term 1.5 or greater
- Rapid draw down 1.3 or greater

The short-term case represents conditions during construction (e.g., for a temporary dredge cut slope prior to backfilling). The long-term case represents conditions once construction is complete



(e.g., for backfilled slopes) and soils/sediments have equilibrated to the stress conditions associated with the post-construction slope geometry.

The rapid draw down condition, typically assessed for engineered dams and levees, was also required by the U.S. Environmental Protection Agency (EPA) for the upper reach stability evaluation and represents a stability case where changes in water levels along shoreline banks occur when the tide is receding, but adjacent upland water levels have not equilibrated to river water levels. A range (1.1 to 1.3) of acceptable factors of safety is published for the rapid draw down case in USACE (2003). The high end of the range (1.3) was selected for this evaluation because upland water surface elevations are considered to be more akin to the maximum storage pool case than the maximum surcharge pool case.

### 3.1.2 Limit Equilibrium Model Development

An assumed dredge cut slope and sediment properties (Table C2-2) were input to the limit equilibrium model, and a search routine was run by the software to locate the critical slip surface. Table C3-1 summarizes the factors of safety calculated in this evaluation.

Stability was evaluated for existing slopes and a range of potential dredge slopes for both short-term (undrained) and long-term (drained) conditions.

Based on bathymetric survey conducted during the PDI, the natural angles of the subtidal to nearshore slopes range from 4 horizontal to 1 vertical (4H:1V) to 17.5H:1V.

The limit equilibrium slope stability evaluation was conducted for two different assumed slope cut angles (2H:1V and 3H:1V) and assuming water levels that correspond to both intertidal and subtidal slopes. For the subtidal evaluation, the dredge cut slope was assumed to be entirely submerged. For the intertidal evaluation, the water level was assumed to be 2 feet below the top of the dredge cut slope.

For the rapid draw down evaluation, it was assumed that the top of the slope on the upland side of the dredge cut would be fully submerged, and a low tide condition (water level 0 feet MLLW) was assumed on the river side of the dredge cut. It was also assumed the slope itself would not drain during the tidal cycle; thus, undrained shear strength parameters were assumed for the dredge cut slope. The rapid draw down condition was assessed for intertidal slopes only, where water levels within the slope would be changing. For submerged slopes, the dredge cut would be sufficiently distant from the influence of upland water levels to affect the slope stability factor of safety during changing tides.

## 3.1.3 Limit Equilibrium Method Model Results

Table C3-1 summarizes the results of the dredge cut slope stability evaluation for the short-term, long-term, and rapid drawdown cases.

Table C3-1
Limit Equilibrium Method Factors of Safety Summary for Dredge Cut Slope Stability

Dredge Cut				Factor o	of Safety
Thickness (feet)	Scenario	Target Factor of Safety	Side Slope	Subtidal Slope <sup>1</sup>	Intertidal Slope <sup>2</sup>
	Short-term	1.2	2H:1V	4.2	2.1
	Short-term	1.3	3H:1V	5.3	2.5
5	long torm	1.5	2H:1V	1.1	N/A
5	Long-term	1.5	3H:1V	1.6	N/A
	Rapid	1.2	2H:1V	N/A	2.1
	drawdown	1.3	3H:1V	N/A	2.5
	Short-term	1.3	2H:1V	4.5	2.4
	Short-term	1.5	3H:1V	5.0	2.6
7		4.5	2H:1V	1.0	N/A
/	Long-term	1.5	3H:1V	1.6	N/A
	Rapid	Rapid	2H:1V	N/A	2.4
	drawdown 1.3	1.3	3H:1V	N/A	2.6

#### Notes:

H:V: horizontal to vertical (ratio)

N/A: not applicable

ROD: Record of Decision

In the short-term condition (i.e., during construction), temporary cut slopes of 2H:1V meet the target factor of safety in both subtidal and intertidal areas.

Long-term slopes constructed at 2H:1V do not meet target factors of safety for subtidal dredged slopes. Long-term subtidal slopes constructed at 3H:1V do meet target factors of safety. In intertidal areas, dredge cut slopes will be backfilled, so there is no need to assess long-term dredge cut stability in these areas.



<sup>1.</sup> The rapid drawdown case does not change conditions for the subtidal slopes because all water surfaces are above the submerged slope and the submerged slope is sufficiently distant from the influence of upland water surface conditions; thus, there is no need for a rapid drawdown evaluation of subtidal slopes created by dredging.

<sup>2.</sup> Intertidal dredge areas will be backfilled in the long-term condition in accordance with the ROD (EPA 2014); thus, there is no long-term intertidal slope condition created by dredging.

Conclusions for the rapid drawdown stability assessment are the same as the short-term stability assessment.

Based on the slope stability evaluation, short-term dredge cut slopes of 2H:1V can be used for the temporary scenario prior to backfilling. For long-term dredge cut slopes (i.e., areas that will not be backfilled), 3H:1V slopes should be used.

# 3.1.4 Alternative Method Model Background, Development, and Results

As required by EPA, the conclusions of the limit equilibrium modeling method were checked using an alternative method of assessment—specifically slope stability chart solutions, as presented in USACE (2003) Appendix E.

Table C3-2 compares the chart solutions with the limit equilibrium solutions (Table C3-1) for the short-term (undrained) case and a 5-foot-deep dredge cut. As demonstrated by Table C3-2, the limit equilibrium method used provides a more conservative result; therefore, it is being carried forward as the appropriate tool for assessing slope stability.

Table C3-2
Slope Stability Comparison – Alternative Method and Limit Equilibrium Method Solutions

Case	Alternative Method (Chart Solution) Factor of Safety	Limit Equilibrium Method Solution Factor of Safety (Table C3-1)
2H:1V Slope – 5-foot cut depth Subtidal	6.5	4.2
2H:1V Slope – 5-foot cut depth Intertidal	3.6	2.1
3H:1V Slope – 5-foot cut depth Subtidal	8.5	5.3
3H:1V Slope – 5-foot cut depth Intertidal	4.7	2.5

Notes:

Comparison for short term (undrained) evaluations.

H:V: horizontal to vertical (ratio)

# 3.2 Bank Excavation Slope Stability

### 3.2.1 General Bank Slope Stability Considerations

In most locations along the banks of the upper reach, bank excavations will require removal of surficial soils or sediment. Where excavations on banks are on the order of 1 to 2 feet deep, the evaluation of bank excavation slope stability is not warranted because removal of thin cuts will not materially affect the stability of the bank itself. Experience conducting similar work on other shoreline projects has demonstrated that minor bank excavations (1 to 2 feet deep) can be accomplished without causing slope stability problems.

Bank slope stability is a key consideration for areas where deeper cuts are required at the toe of a bank area or on the bank itself. In these situations, the deeper cut can undermine the toe of the bank and can potentially cause slope instability if not accounted for in the design. For the 30% RD, one bank area met the criteria for a location-specific bank slope stability evaluation—the South Park Marina. As previously discussed, the need for dredging in this area will be re-evaluated during the Pre-Final (90%) RD based on Phase III PDI data. For the 60% RD, an additional bank at Container Properties was identified for location-specific bank slope stability evaluation as described in this section. The stability of other intertidal banks will be evaluated in more detail, if appropriate, during the Pre-Final (90%) RD after shoreline dredge prisms are refined.

### 3.2.2 South Park Marina

For the Preliminary (30%) RD, the stability of the bank at South Park Marina was evaluated to determine whether dredging at the toe of slope could increase the risk of slope movement. The slope in this area is reported to be marginally stable (Spadaro 2022); slope stability issues have occurred during previous shoreline work. Because modifications, if any, to the dredge design in this location will be assessed during the Pre-Final (90%) RD using Phase III PDI data, no updates to the evaluation described in this section were made for this Intermediate (60%) RD submittal.

The stability of the bank slope in the South Park Marina where RAL exceedance Area 13 is located was modeled using limit equilibrium methods. Both short-term and long-term conditions were assessed for the existing slope configuration and for a post-dredge slope configuration assuming a 2H:1V dredge cut at the toe of slope, to a depth of -9 feet MLLW. Figure C3-1 depicts the cross section that was evaluated and shows the critical slip surface identified in the model results for the long-term condition for both the pre-dredge and post-dredge conditions. The slope stability modeling identified the following considerations for RD:

• The long-term factor of safety for the existing slope configuration is marginally higher than 1.0. This conclusion is consistent with reports that the slope in this area is considered only marginally stable.



- The long-term factor of safety for the post-dredge configuration suggests that the dredging side slopes would be stable, but the overall slope would continue to be marginally stable with the same factor of safety (and same critical slip surface location) as the existing long-term condition.
- The short-term factor of safety (during construction) for the dredge cut assumed in Figure C3-1 has a factor of safety less than 1.0. This suggests that, for the modeling assumptions used, the dredge cut cannot be accomplished without destabilizing the slope.

Based on these considerations, the design of the dredge cut at RAL exceedance Area 13, as assumed in Figure C3-1, will need to be refined.

One option in this area would be to develop an integrated remedy that includes any potential remediation of the uplands being performed during the same remedial construction in water. In this case, the geotechnical design assumptions would be revisited, and the slope stability reevaluated considering the geometry of the proposed integrated remedial approach. In this case, construction in the South Park Marina basin would occur on a separate timeline from other LDW upper reach remedial actions. Coordination of the cleanup at RAL exceedance Area 13 with work in the adjacent uplands is further discussed in the body of the BODR.

If the sediment remediation proceeds prior to any additional upland/bank remediation, there are several options to be considered for refining the design in this area, including the following:

- Flatten the dredge cut side slopes. This refinement alone may not be sufficient to achieve an acceptable short-term factor of safety.
- Offset the dredge cut sufficiently so that the dredge cut does not influence the short-term stability of the adjacent slope.
- Reduce the depth of required dredging in this area. Based on conversations with
  representatives of the South Park Marina, the marina is considering a reduced berth depth in
  this area to help mitigate issues associated with the marginally stable slope.
- Install temporary shoring, such as a sheetpile wall at the toe of slope. The dredge cut would likely need to be backfilled, and the overall slope would continue to be marginally stable after the temporary shoring is removed.
- Collect additional subsurface geotechnical information on the slope in this area. The model
  currently assumes the slope beneath the riprap consists of recent sediments, which have
  relatively low undrained shear strength. If conditions in this area are better than assumed in
  the model, the slope stability factor of safety would improve. However, because this area has
  been observed to be marginally stable, it is not expected that additional data collection would
  significantly modify the modeling conclusions.

As described in the BODR, further agency coordination is needed to develop the preferred path forward for integrating in-water and upland cleanup designs at the South Park Marina.

### 3.2.3 Container Properties

The Intermediate (60%) RD includes bank excavation along the slopes at Container Properties. The existing bank transitions from the upland to an intertidal mud flat and dredging and excavation will occur on the mud flat and banks, respectively. Dredge cut depths range from 2.5 to 3.5 feet at the toe of bank, and the same minimum thickness cut will be performed on the bank itself at a slope no steeper than 2H:1V. Additional excavation thickness will be added on the bank and at the toe, as necessary so that the final reconstructed bank does not raise the bathymetry above pre-construction conditions. This additional thickness will be developed during the Pre-Final (90%) RD.

Following excavation, the bank will be reconstructed with layers of sand backfill beneath armor rock as described elsewhere in the BODR.

To evaluate the stability of bank cuts, a limit equilibrium model was developed for the most critical stability case—that is, the cross section corresponding to the deepest dredge cut at the toe of bank. Stability analyses were run for the existing condition to check model calibration and assumed input parameters, and for the short-term condition (during bank cut) and long-term post-construction condition (including backfill sand and armor rock).

Table C3-3 summarizes the resulting factors of safety for the bank stability evaluation at Container Properties.

Table C3-3
Slope Stability Results – Container Properties

Case	Side Slope (H:V)	Target Factor of Safety	Modeled Factor of Safety
Existing condition	2H:1V	N/A	1.22
Short-term	2H:1V	1.3	1.33
Long-term	2H:1V	1.5	1.49

Notes:

H:V: horizontal to vertical N/A: not applicable

As demonstrated in Table C3-3, the short-term and long-term stability cases have acceptable factors of safety, indicating that the temporary slope cut of 2H:1V is appropriate and that the long-term armored slope will be stable after construction.

### 3.3 Prospective Cap Geotechnical Design Evaluation

The Intermediate (60%) RD does not include capping as a planned remedy technology, although caps could be needed as an element of the reconstructed shoreline slope at Container Properties. Capping may be determined to be needed at other locations following review and integration of the Phase III PDI data into the design during the Pre-Final (90%) RD. Thus, geotechnical capping evaluations prepared for the Preliminary (30%) RD were retained and updated to support this Intermediate (60%) RD in the event that caps will be needed in the future.

This section describes prospective cap bearing capacity and subgrade settlement evaluations completed for the Intermediate (60%) RD of the upper reach sediment remedy. These bracketing level evaluations consider a range of potential cap thicknesses and will be updated, if needed, for the Pre-Final (90)% RD.

This section also describes the cap static stability evaluation. Seismic cap performance evaluations are discussed in Section 5.

### 3.3.1 Bearing Capacity

Bearing capacity caps were evaluated using methods described in Appendix C of the Assessment and Remediation of Contaminated Sediments (ARCS) Program, "Guidance for *In situ* Subaqueous Capping of Contaminated Sediments" (Palermo et al. 1998). When cap material is placed on the surface of soft sediments, there is the potential for a bearing capacity failure directly through the in situ sediment. The initial cap lift thickness must be thin enough to maintain an acceptable factor of safety under the new loading caused by the weight of the cap.

In typical foundation design problems, a factor of safety of 3.0 is used for calculations wherein there is the potential for structural damage or impacts on human safety. This is the suggested factor of safety presented in the ARCS guidance. However, experience on other capping projects has shown that a factor of safety of 3.0 can be overly conservative when considering cap construction lift thickness. Because life safety and structural foundation stability are not design considerations for caps, and because slope stability evaluations use similar factors of safety, a factor of safety of 1.5 was considered appropriate for use in this analysis for evaluating the cap bearing capacity. Subaquatic cap placement has been successfully demonstrated at other sediment cleanup sites when designed using a bearing capacity factor of safety of 1.5, including the Whatcom Waterway sediment cleanup project (Anchor QEA 2015) and the San Jacinto River Superfund Site Time Critical Removal Action (Anchor QEA 2011).

This analysis evaluates the steady-state, short-term stability of the cap and soft sediments during construction. Once the cap has been placed, consolidation of fine-grained in situ sediments will



occur, increasing the shear strength of the sediment. Thus, the long-term stability of the cap against bearing capacity failure will be greater than the short-term stability.

The in situ sediments must have sufficient internal strength to prevent local shear failure. To evaluate this condition, the ultimate bearing capacity was calculated with the Terzaghi equations for local failure (Palermo et al. 1998) using the undrained shear strengths described in Section 2.3:

$$q_{ult} = \left(\frac{2}{3}\right) s_u * N_c$$
 (Equation 3-1)

Where:

 $q_{ult}$  = ultimate bearing capacity of sediment (psf)

 $s_u$  = undrained shear strength of in situ sediments (psf)

 $N_c$  = bearing capacity factor (dimensionless) = 5.14 for continuous strip footing (Terzaghi and Peck 1967)

This equation applies to a cap placed on the surface of an entirely cohesive soil with an angle of internal friction,  $\phi'$ , equal to zero. For the caps placed in the upper reach, it is assumed that at least 2 feet of dredging would be performed before cap placement. Therefore, the shear strength at the 3-foot depth interval is considered appropriate for evaluating cap bearing capacity. Based on the shear strength assumptions presented in Table C2-2, the undrained shear strength of recent sediments below the 2-foot depth interval is 86 psf.

The ultimate bearing capacity was calculated as follows:

$$q_{ult} = \left(\frac{2}{3}\right)86 * 5.14 = 295 \, psf$$

A factor of safety of 1.5 was used to compute the allowable bearing capacity:

$$q_{all} = \left(\frac{q_{ult}}{FOS}\right)$$
 (Equation 3-2)

Where:

 $q_{all}$  = Allowable bearing capacity (psf)

FOS = Factor of Safety = 1.5

$$q_{all} = \left(\frac{295}{1.5}\right) = 196 \, psf$$



The initial cap lift thickness that could be supported by the lowest strength in situ sediments at an appropriate factor of safety was calculated using the allowable bearing capacity and the following equation:

$$h = \left(\frac{q_{all}}{\gamma'}\right)$$
 (Equation 3-3)

Where:

h = lift thickness

 $\gamma'$  = buoyant unit weight of cap material (pcf)

 $\gamma' = \gamma - \gamma_w$ 

 $\gamma$  = total unit weight of cap material (pcf)

 $\gamma_w$  = unit weight of water (64 pcf)

 $\gamma' = 110 \text{ pcf} - 64 \text{ pcf} = 46 \text{ pcf}$ 

$$h = \frac{196 \, psf}{46 \, pcf} = 4.2 \, feet \approx 48 \, inches$$

This analysis, which uses the minimum in situ shear strength selected for modeling, indicates that a cap of 48 inches can be placed while maintaining an appropriate factor of safety for sediment bearing capacity during construction, assuming a dredge depth of 2 feet prior to capping. In this configuration, the post-cap surface would project 2 feet above the pre-construction ground surface.

Caps and backfill will generally be constructed to match existing grade and not project above the pre-construction ground surface. However, this evaluation indicates that caps could still project above the pre-construction surface (up to 2 feet) while maintaining an appropriate factor of safety.

The Intermediate (60%) RD does not identify the need for caps that project more than 2 feet above the pre-construction ground surface. If the need for caps is identified during the Pre-Final (90%) RD that could project more than 2 feet above the pre-construction surface, or if caps would be needed in locations that are partially emergent above the water line, the bearing capacity evaluation will be revisited and, if necessary, measures to control lift placement will be defined for inclusion in the project specifications. Further, any caps that project above the pre-construction surface grade would need to be considered separately as part of the habitat assessment.

# 3.3.2 Subgrade Consolidation Settlement

Subgrade consolidation beneath the load imposed by a cap was assessed for two different scenarios. In Scenario 1, the constructed cap would be placed after dredging, and the post-cap grade would be the same as the pre-dredge mudline elevation. The new loads imposed on the subgrade would be caused by the greater unit weight of cap material than the in situ unit weight of the sediments that



would have been dredged. Scenario 1, developed to reflect the ROD requirements for capping, would apply most of the time that caps would be used.

Scenario 2 reflects the use of caps where dredging would be limited (e.g., in offset areas that would be specified to protect structures). The top of cap in Scenario 2 would be at a higher elevation than the original pre-construction mudline, so new loads would also be caused by additional cap material placed above the pre-construction mudline elevation.

Both scenarios assume a 4-foot-thick cap. In Scenario 1, 4 feet of dredging is assumed. In Scenario 2, 2 feet of dredging is assumed prior to cap placement. Two different in situ sediment thicknesses were evaluated to bracket the range of predicted settlement. Table C3-4 summarizes the scenarios evaluated for subgrade consolidation.

Table C3-4
Subgrade Consolidation Modeling Scenarios

Scenario	Pre-Dredge Sediment Thickness (feet)	Dredge Depth (feet)	Post Dredge Sediment Thickness (feet)	Cap Thickness (feet)	Net Stress Increase (psf) <sup>1</sup>
1a	7	4	3	4	40
1b	15	4	11	4	40
2a	7	2	3	4	240
2b	15	2	11	4	240

#### Notes:

Subgrade consolidation was calculated according to the following relationship:

$$\Delta H = H \times CR \times \log \left( \frac{\sigma'_{vo} + \Delta \sigma'_{vo}}{\sigma'_{vo}} \right)$$
 (Equation 3-4)

Where:

 $\Delta H$  = consolidation settlement

*H* = consolidating layer thickness

CR = compression ratio of subgrade sediment (Table C2-2)

 $\sigma'_{vo}$  = in situ vertical effective stress  $\Delta \sigma'_{v}$  = net stress increase (Table C3-2)

Table C3-5 summarizes the results of the subgrade consolidation evaluation.

<sup>1.</sup> Assumes cap imposes total unit weight (above the water line) on the subgrade. psf: pounds per square foot

Table C3-5
Subgrade Consolidation Summary

Scenario	Estimated Consolidation Settlement (inches)
1a	2
1b	3
2a	5
2b	10

As shown in Table C3-5, the subgrade in dredge and cap areas is predicted to settle approximately 2 to 3 inches after cap placement. Although not anticipated, if caps were to be placed to a final elevation that is 2 feet above the pre-construction mudline, a range of subgrade settlement of 5 to 10 inches is predicted.

The time rate over which consolidation occurs is a function of the distance porewater must travel (drainage path length) and the coefficient of consolidation of the subgrade. Time rate of consolidation was evaluated according to the following equation:

$$T = \frac{c_v t}{H_{DR}^2}$$
 (Equation 3-5)

Where:

T = time factor = 0.8 for 90% consolidation (Lambe and Whitman 1969)

 $c_v$  = coefficient of consolidation (Section 2.3)

t = time to achieve 90% consolidation  $H_{DR}$  = drainage path length (Section 2.3)

Based on Equation 3-5, it is estimated that subgrade consolidation would be 90% complete approximately 120 days after cap construction.

Subgrade consolidation settlement can confound the interpretation of bathymetric survey results if bathymetry surveys are used to confirm the thickness of caps. When subgrade consolidation settlement occurs, bathymetry comparisons (i.e., isopach mapping) can be incorrectly interpreted as indicating "thinning" of cap material. Therefore, supplemental cap confirmation approaches such as thickness probing would also be included in Long-Term Maintenance and Monitoring Plan (LTMMP) planning to address potential issues associated with subgrade consolidation if caps are to be constructed.



# 3.3.3 Static Slope Stability of Caps

The Preliminary (30%) RD for the upper reach identified the potential need for a cap along the shoreline at RAL exceedance Area 18. The Intermediate (60%) RD does not include the same approach in this area; the Intermediate (60%) RD includes the potential need for a cap within the armored revetment to be constructed along the Container Properties shoreline (RAA 27). The cap at Container Properties would be placed following excavation, resulting in a cap surface that generally matches the pre-construction grade or flatter in the capping area. This section describes the static slope stability evaluation of prospective caps, if needed, using RAL exceedance Area 18 as an example location that is representative of typical intertidal slopes and Container Properties (RAA 27) as a location where an intertidal cap would be constructed on the bank.

Cap slope stability was evaluated using limit equilibrium methods. A geologic profile was developed for both RAL exceedance Area 18 and Container Properties using soil and sediment geotechnical engineering parameters presented in Table C2-2. The modeling software was set to search for the critical slip surface for any location along the slope on the water side of the bulkhead along RAL exceedance Area 18 or within the slope at Container Properties.

Figure C3-2 presents the geologic profile for RAL exceedance Area 18 and depicts the critical slip surface and factor of safety. The factor of safety for the cap is 2.25, which is greater than the target long-term factor of safety of 1.5, indicating acceptable static slope stability for caps. At Container Properties, the factor of safety for the cap is 1.49, which is also considered acceptable. If additional caps on slopes are identified as an element of the 90% RD, this evaluation will be updated, as appropriate, based on the location where caps would be constructed.

# 3.4 Backfill Design

This section describes the gradation and stability design of backfill materials.

# 3.4.1 Backfill Gradation

The selection of backfill considers several engineering considerations, including the following:

- Commercially available, natural aggregate materials
- Appropriate proportion of gravel within the aggregate mixture to provide stability to backfill placed on slopes, as evaluated in Section 3.4.2
- Limiting the percentage fines (material that passes the U.S. No. 200 Sieve) to protect water quality by minimizing turbidity during placement

Table C3-6 presents a recommended backfill gradation that achieves these objectives. The remedial contractor may identify material that is very similar to this gradation and that may be acceptable for



use as backfill. The engineer should review any proposed deviations from this specification and may approve an alternate gradation in consultation with EPA.

Table C3-6
Backfill Gradation Specifications

Sieve Size	Percent Passing
2-inch	100
1.5-inch	80 to 95
0.75-inch	50 to 90
U.S. No 4	30 to 50
U.S. No. 200	0 to 5

In addition to engineering considerations, there may be additional habitat considerations that would be evaluated separately in consultation with EPA. Further, backfill material must meet or be lower than chemical concentration limits that will be defined in the project specifications based on cleanup levels for human health and benthic protection.

### 3.4.2 Backfill Stability

Backfill will be placed in habitat areas (elevations greater than -10 feet MLLW) in accordance with the ROD (EPA 2014). In some dredge areas, backfill may need to be sloped below elevation -10 feet MLLW until it meets the post-dredge surface at depth. This section presents the evaluation of stable backfill slope angles to support the backfill grading design.

Backfill slope stability was evaluated using infinite slope stability theory, in accordance with Duncan and Wright (2005). For this evaluation, the factor of safety for a 3H:1V backfill slope was computed using the following equation:

$$FOS = \frac{\tan{(\emptyset')}}{\tan{(i)}}$$
 (Equation 3-6)

Where:

FOS = Factor of Safety

 $\phi'$  = backfill friction angle (Table C2-2)

I = slope angle

The factor of safety for backfill placed at a 3H:1V slope is 1.9, which is greater than the target long-term slope stability factor of safety. Thus, a 3H:1V slope angle should be used for the design of backfill slopes.



Where steeper slopes may be needed, armor rock could be used to protect the backfill surface. Shoreline armor has a higher friction angle than sand and gravel backfill and is typically assumed to range from 38 to 42 degrees for angular rock (USDA 1989). Assuming an armor rock friction angle of 38 degrees, slopes of 2H:1V have a factor of safety of 1.6, which is greater than the minimum long-term factor of safety of 1.5. Thus, backfill can be placed on 2H:1V slopes if angular armor rock is used.

# 4 Geotechnical Engineering Recommendations to Support Structural Engineering Evaluations

This section presents geotechnical engineering recommendations to support structural evaluations of vertical structures such as bulkheads and bridge piers, and to design replacement piles that may be needed as part of remedy construction in the upper reach. Necessary structural engineering evaluations were developed for the Intermediate (60%) RD based in part on the recommendations provided in this section.

### 4.1 Vertical Structure Evaluation Geotechnical Recommendations

This section provides recommendations for the structural engineer to use for the evaluation of existing vertical structures adjacent to RAL exceedance areas.

### 4.1.1 Lateral Earth Pressures for Shoreline Structures

The following lateral earth pressure recommendations are provided for structural evaluation of cantilevered shoreline bulkhead walls. This information can be used to assess the need for offsets or other measures if dredging needs to be performed in front of bulkheads.

Lateral earth pressures acting on the bulkhead will depend primarily on the following:

- Fill material placed behind the wall, and the degree of compaction immediately adjacent to the wall
- Flexibility of the wall, and the degree of movement that the wall undergoes
- The presence of any surcharges or concentrated loads adjacent to the bulkhead
- Wall drainage
- Seismic loading

If the bulkhead is permitted to yield such that the top can move laterally at least 0.1% of the bulkhead's retained height when loaded, active earth pressures will develop. If this level of deflection is intolerable, the wall should be evaluated using at-rest soil pressures.

To design for lateral earth pressures, the parameters provided in Table C4-1 should be used. Earth pressures may be computed assuming a triangular pressure distribution applied from the top of the bulkhead to the base of the sheeting, as shown in Figure C4-1. Passive pressures will also be applied in a triangular distribution, from the mudline downward.

Table C4-1
Bulkhead Lateral Earth Pressure Parameters

Parameter	Design Value
GWT behind bulkhead	6 feet MLLW
Upland soil effective unit weight above GWT	135 pcf
Upland soil effective unit weight below GWT	71 pcf
Upland soil effective friction angle (φ')	33 degrees
Upland soil cohesion c	0 psf
Waterway sediment effective unit weight above waterline	100 pcf
Waterway sediment effective unit weight below waterline	36 pcf
Waterway sediment effective friction angle (φ')	27 degrees
Waterway sediment cohesion (c)	0 psf
K <sub>A</sub> – active pressure coefficient for upland soils – flexible walls	0.29
K <sub>O</sub> – at rest pressure coefficient for upland soils – rigid walls	0.46
K <sub>P</sub> – passive pressure coefficient for waterway sediments <sup>1</sup>	2.66

#### Notes:

1. Passive pressures are presented as ultimate values and do not include a factor of safety.

ft: foot

GWT: groundwater table elevation MLLW: mean lower low weight pcf: pounds per cubic foot psf: pounds per square foot

As noted in Table C4-1, using the passive pressure coefficient provided would result in calculating ultimate passive soil resistance, which would be an appropriate assumption for calculating the potential reduction in passive resistance at the toe of the wall when dredging occurs. Figure C4-1 depicts the pressure distribution for active and passive earth pressure conditions and provides recommendations for temporary tieback no-load zone and tentative tieback adhesion values.

# 4.1.2 Effect of Prohibiting Surcharge Loads Above Bulkheads During Adjacent Dredging

Bulkheads retain soil loads and surcharges in the form of active or at rest lateral earth pressures. These earth pressures are resisted at the toe of the bulkhead by passive earth pressures provided by the sediments in front of the bulkhead. The following discussion evaluates how much of the passive earth pressure is needed to resist surcharge loads alone and the effect to prohibiting surcharge loads



during dredging. This assessment was developed using generalized soil and sediment conditions and thus is applicable to structures throughout the upper reach.

It is assumed that shoreline bulkheads were designed and constructed to support temporary surcharge loads at the top of the bulkheads. Typically, a temporary surcharge of 250 psf (or higher) can be accommodated by marine shoreline structures in good condition. Assuming a bulkhead backfill unit weight of 135 pcf, 250 psf is effectively equivalent to a soil surcharge height of approximately 2 feet.

One way to protect structures during adjacent dredging is to prohibit surcharge loading during dredging. This effectively allows for the "design surcharge capacity" of the wall to be used to offset the temporary loss of passive pressure in front of the wall due to dredging.

To evaluate this factor, the bulkhead adjacent to the Port of Seattle Sliver Property at RAL exceedance Area 18 was selected as a representative example. The bulkhead at this location currently has a retained soil height of approximately 15 feet. The active lateral earth pressure behind the wall (no surcharge) is calculated as follows:

$$P_A = \frac{1}{2} K_A \gamma h^2 \qquad \text{(Equation 4-1)}$$

Where:

 $P_A$  = Active earth pressure resultant force (pound per foot [lb/ft])

 $K_A$  = Active earth pressure coefficient for retained soil (Table C4-1)

 $\gamma$  = unit weight of retained soil (Table C4-1)

*h* = retained height of soil (ft)

For the RAL exceedance Area 18 bulkhead, the resultant active earth pressure is calculated to be 4,400 pounds per foot (lb/ft).

Adding 1.85 feet of retained height for the surcharge loading condition (equivalent to a retained soil height of 16.85 feet), the active lateral earth pressure is calculated to be 5,560 lb/ft, which means that prohibiting surcharge during dredging could offset the loss of 1,160 lb/ft of passive pressure.



Passive earth pressure is calculated as follows:

$$P_P = \frac{1}{2} K_P \gamma d^2 \qquad \text{(Equation 4-2)}$$

Where:

 $P_P$  = passive earth pressure resultant force (lb/ft)

 $K_P$  = passive earth pressure coefficient for sediments (Table C4-1)

 $\gamma$  = unit weight of sediments (Table C4-1)

d = depth below mudline (ft)

For the passive pressure coefficients for sediments presented in Table C4-1, a depth of approximately 5 feet below mudline is required to achieve a passive pressure of 1,160 lb/ft when sediments are submerged (buoyant unit weight providing passive pressure) or approximately 3 feet below mudline when sediments are not submerged (total unit weight providing passive pressure).

Based on this evaluation, for shoreline bulkheads in good condition that were designed to support an upland surcharge of at least 250 psf, prohibiting surcharges during dredging would allow for 3 to 5 feet of dredging to occur while maintaining passive pressure support comparable to the surcharge loading condition with no dredging.

Note that this assessment considers the soil loads only and does not account for the condition of the bulkhead wall nor the stresses in the wall structure that might be imposed by removing passive support during dredging.

## 4.1.3 Effect of Dredging on Passive Pressure

As previously discussed, dredging adjacent to structures reduces lateral toe support (i.e., passive pressure), which can increase the loads on the structure. This section describes the evaluations performed to determine appropriate reductions in passive pressure considering the following:

- Dredge cut slope angle
- Dredge cut depth
- Horizontal offset of dredge cut from the structure

The analyses presented in this section were developed specific to the Recent Sediments material that would be removed by dredging and is applicable to any vertical structure in the upper reach (e.g., bulkheads, bridge piers). To conduct this analysis, the total available passive pressure (no dredging) was compared to the weight of the passive wedge that would remain after dredging. The reduction factor was calculated as follows:



Reduction Factor = 
$$\frac{w_w}{P_P}$$
 (Equation 4-3)

Where:

W<sub>w</sub> = Buoyant weight of passive soil wedge between structure and toe of dredge cut (lb/ft)

P<sub>R</sub> = Passive earth pressure force for the no dredging scenario calculated at the evaluated depth of dredging (lb/ft)

Offsets of 0, 2, and 4 feet from the structure were considered. A range of dredge depths from 5 to 15 feet deep was evaluated. Dredge cut side slopes of 2H:1V, 1.5H:1V, and 1H:1V were assessed.

Key conclusions from this evaluation, in the form of passive earth pressure reduction factors, are presented in Table C4-2.

Table C4-2
Passive Earth Pressure Reduction Factors

Offset Distance	Reduction Factor		
(feet)	2H:1V	1.5H:1V	1H:1V
0	0.75	0.56	0.38
2	0.85	0.66	0.48
4	0.95	0.76	0.58

Note:

H:V: horizontal to vertical (ratio)

As shown in Table C4-2, when the dredge prism is not offset, the passive earth pressure could be significantly reduced, particularly if the dredge cut is over-steepened beyond the recommended 2H:1V temporary cut slope. Reduced passive pressure increases the risk of damaging structures.

Based on this evaluation, a minimum horizontal dredging offset of 5 feet is recommended to minimize the potential for reduced passive earth pressure, unless structural engineering assessments conducted during the Pre-Final (90%) RD conclude that the offset can be reduced or eliminated. The reduction factors presented in Table C4-2, in conjunction with the earth pressure recommendations in Table C4-1, can be used by the structural engineer to determine whether any structures can tolerate a dredging offset that is closer than 5 feet.

### 4.2 Pile Design Recommendations

Piles are anticipated to be removed at the South Park Marina floats to facilitate access for remedy construction. There may also be miscellaneous single piles or dolphin pile groups that need to be removed to accomplish construction. This section presents geotechnical engineering pile design recommendations for the structural engineer's use in designing replacement piles.

Based on discussion with the project structural engineer, replacement piles are likely to be hollow steel pipe piles, which lend themselves to vibratory installation and are capable of supporting the range of loads anticipated for this project. Timber piles are not considered for new installations for the upper reach because timber piles require chemical treatment to prevent decay.

Replacement piles for the South Park Marina floats are expected to be primarily laterally loaded. Replacement piles that support vertical loads are not expected to be needed for the upper reach. If such a need arises during the Pre-Final (90%) RD, the geotechnical recommendations will be updated to provide vertical compressive and uplift capacity estimates specific to the pile size(s) anticipated and the location(s) where they would be installed.

Pile design to resist lateral loads can be accomplished using L-PILE or similar software to assess pile deflection under loading and required depth to fixity below the mudline. Table C4-3 presents recommended L-PILE parameters to model the recent sediments and alluvium. Table C4-4 presents recommended mudline elevations and sediment unit thickness for pile design assessments at the South Park Marina floats. Note that the South Park Marina recommendations in Table C4-4 do not reflect current conditions—the elevations and thicknesses assume future maintenance dredging will be performed in the vicinity of the floats. This assumption for the South Park Marina will result in conservative embedment depths such that piles will perform as intended even if dredging is not performed.

The need for replacement piles at other locations may be identified during the Pre-Final (90%) RD. If additional areas require replacement piles, the recommendations in Table C4-4 will be updated accordingly.

Table C4-3 L-PILE Modeling Parameters

	Effective Unit Weight	Friction Angle				Strain Factor; @50% max E	
Layer	γ' (pcf)	ф (°)	c <sub>u</sub> (kip/ft²)	Model	k (pci)	<b>E50</b>	
Recent sediment	36	27	0.08	Soft clay (Matlock)	1	0.020	
Alluvium	61	32		Sand (Reese)	20		

Notes:

ft<sup>2</sup>: square foot

kip: one thousand pounds

pcf: pounds per cubic foot

pci: pounds per cubic inch

Table C4-4
Mudline Elevations and Sediment Unit Thicknesses for Lateral Pile Design

Location	Design Mudline Elevation for Replacement Piles (feet MLLW)	Recent Sediment Unit Thickness (feet)	Contact Elevation between Recent Sediments and Alluvium (feet MLLW)
South Park Marina floats	-12 <sup>1</sup>	9	-12

## Notes:

1. The design mudline elevation Is based on the Waterway Users Survey for this location.

MLLW: mean lower low water

## 5 Seismic Design

The upper reach of the LDW is located within the seismically active Puget Lowland, a region characterized by bedrock faults and tectonic plate movement and that has a documented history of earthquake activity. Earthquakes occur when energy accumulated during fault or tectonic plate movement is suddenly released over a short time span. The location of energy release, known as the epicenter of an earthquake, can occur at different places in a fault system.

The ground shaking caused by an earthquake can cause loose soils to lose strength as porewater pressure increases. This phenomenon, known as liquefaction, can cause soil movement and ground settlement. Earthquakes can also shake structures and impose loads on structural elements and foundations. Seismic risks are assessed in geotechnical engineering using a variety of tools.

This section describes the seismic design of the sediment remedy for the upper reach with a focus on the anticipated performance of remedial elements (primarily sediment caps) under earthquake loading. This section also provides recommended seismic design parameters for use by the structural engineer, as appropriate.

## 5.1 Seismic Site Class

Seismic behavior is generally assessed by evaluating the relative density of near-surface soils (the upper 100 feet below ground surface). For seismic design, relative density is often characterized by the average shear wave velocity of the soil column, which governs how earthquake energy is amplified or dampened by the near-surface soils. A Washington State-wide study by Cakir and Walsh (undated) summarized measurements of shear wave velocity at different sites across the state, including three locations in the Duwamish River basin near the upper reach. This study identified a typical seismic site class between Class D and Class E based on average shear wave velocities between 131 and 183 meters per second for the Duwamish River area in the vicinity of the upper reach.

## 5.2 Strong Motion Design Input Parameters

For seismic evaluations, earthquake peak ground acceleration (presented as a percentage of the force of gravity) and earthquake magnitude are key input parameters.

The U.S. Geological Survey (USGS) provides internet-based tools that, using mapped locations and seismic site classes, output peak ground accelerations, and earthquake magnitudes for different recurrence interval earthquakes.

For the upper reach sediment remedy, two different earthquake types were considered:

- A 100-year recurrence interval earthquake, consistent with typical protectiveness evaluations for other remedy elements such as cap contaminant modeling
- A 475-year recurrence interval earthquake, which has traditionally been the size of event considered on other regional Superfund projects based on a 10% probability of exceedance in a 50-year time frame

Table C5-1 provides the key USGS output parameters used for geotechnical seismic assessment for both events.

Table C5-1
Earthquake Parameters used in Geotechnical Engineering Evaluations

Event Recurrence Interval	PGA (% gravity)	Mean Magnitude
100 years	0.19	6.7
475 years	0.41	7.0

Notes:

Data developed for latitude 47.522, longitude -122.306.

Site Class D/E; Dynamic Conterminous United States model (2014 edition v4.2.0).

Model source: https://earthquake.usgs.gov/hazards/interactive.

PGA: peak ground acceleration

## 5.3 Liquefaction Evaluation

As described in Section 2, the site investigation included CPTs at 20 different locations in the upper reach. Digital records from these CPTs were processed by the analytical software Cliq (version 3.3.1.14), which facilitates liquefaction assessment and estimates of liquefaction-induced settlement using CPT measured parameters, earthquake peak ground accelerations, and earthquake magnitude.

For all locations investigated with a CPT, liquefaction was predicted during both the 100- and 475-year earthquakes. The estimated magnitude of liquefaction-induced settlement did not significantly vary between the two earthquakes, ranging from 3 to 14 (median 7) inches of settlement in the upper 30 feet below ground surface.

## 5.4 Seismic Performance of Capped Slopes

The seismic performance of capped slopes was evaluated using limit equilibrium methods, as described for the slope stability discussions in Section 3. Geologic cross sections of the slope at RAL exceedance Area 18 and at Container Properties (RAA 27) were modeled, and seismic forces



associated with both the 100- and 475-year earthquakes were added. For the 475-year earthquake, the resulting factor of safety was less than 1.0, indicating that some movement of the capped slope can be expected during a significant earthquake. For the 100-year earthquake, the factor of safety was 1.05 at RAL exceedance Area 18 and 1.15 at Container Properties. Figure C5-1 depicts the cross section evaluated for RAL exceedance Area 18, as well as the critical slip surface and factors of safety for both the 100-year and 475-year earthquakes at this location. If other slope areas are identified during 90% RD that will require caps, this evaluation will be updated to include those areas.

In general, shoreline slopes are susceptible to movement during strong earthquake shaking. Slopes designed to resist movement could require significant structural reinforcement that is not compatible with the habitat and human uses of shorelines. In part, due to issues like this, the geotechnical engineering community is moving toward a performance-based assessment of slopes, when appropriate, for seismic design. In the case of shoreline slopes where life safety and structures are not at risk, this type of assessment does not attempt to design for preventing movement; rather, a performance-based approach evaluates how much movement could be expected during an earthquake and what mitigation measures, if any, would need to be implemented after the earthquake had occurred.

Slope displacement was estimated for both the 100- and 475-year earthquakes in accordance with the methods presented in NCHRP (2008). Table C5-2 presents the estimated slope displacement for a proposed cap at RAL exceedance Area 18 and at Container Properties under both earthquake scenarios.

Table C5-2
Seismic Slope Displacement for RAL Exceedance Area 18 and Container Properties Caps

Earthquake Return Interval	RAL Exceedance Area 18 Estimated Displacement	Container Properties Cap Estimated Displacement
100 years	1 to 2 inches	< 0.5 inch
475 years	1 to 2 feet	8 to 16 inches

Note:

RAL: remedial action level

## 5.5 Conclusions on Seismic Performance of Sediment Remedy

Based on the liquefaction assessment and slope displacement estimates, the sediment remedy is expected to have acceptable seismic performance. Anticipated settlement and displacement under the 100-year event is expected to be significantly less than any design cap thicknesses. During a larger earthquake, the cap and sediments beneath may move down the slope, but any cap damage from such movement is expected to be easily repaired



Post-earthquake mitigation measures could include visual inspections and bathymetry surveys to evaluate cap condition. Cap repairs, if needed, could be readily implemented by adding more cap substrate to address any local thinning associated with post-earthquake deformation or settlement.

The LTMMP will consider these evaluations and set criteria for inspections following seismic events.

## 6 References

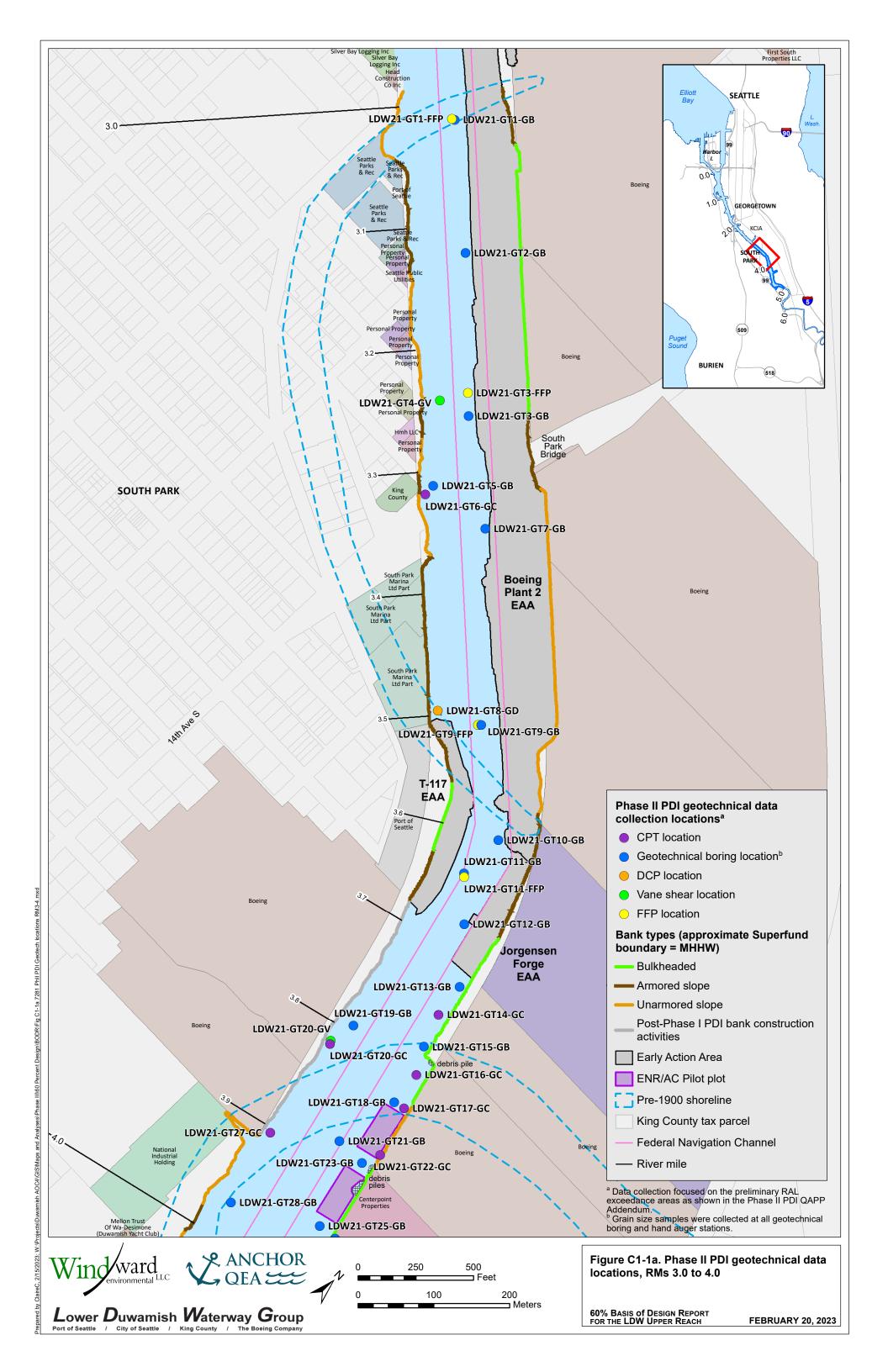
- AMEC, 2002. Limited Geotechnical Engineering Report Delta Marine Industries Boat Lift Pier 1608 S. 96th Street Seattle Washington. May 2002.
- AMEC, 2012. Geotechnical Engineering Report Habitat Project Boeing Plant 2 Seattle/Tukwila Washington. October 2012.
- Anchor QEA (Anchor QEA, LLC), 2011. Final Removal Action Work Plan San Jacinto River Waste Pits Superfund Site. Prepared for EPA Region 6 by Anchor QEA, Revised February 2011.
- Anchor QEA, 2015. Whatcom Waterway Final Engineering Design Report, Appendix B. Prepared for the Port of Bellingham by Anchor QEA. March 16, 2015.
- Anchor QEA and Windward, 2022. *Pre-Design Investigation Data Evaluation Report*. Final. Submitted to EPA July 15, 2022. Anchor QEA and Windward Environmental.
- Cakir and Walsh (undated). Shallow Seismic Site Characterizations of Near-Surface Geology at 20
  Strong Motion Stations in Washington State. Final Technical Report USCS/NEHRP Award
  Number G09AP00021. Recep Cakir and Timothy Walsh, Washington Department of Natural Resources.
- Duncan, J.M. and S.G. Wright, 2005. *Soil Strength and Slope Stability*. First Edition. New Jersey: John Wiley and Sons.
- EPA (U.S. Environmental Protection Agency), 2014. *Record of Decision*. Lower Duwamish Waterway Superfund Site.
- GeoEngineers, 2014. *Geotechnical Engineering Services Terminal 117 Site Restoration for Port of Seattle*. May 2014.
- Lambe and Whitman, 1969. Soil Mechanics. John Wiley and Sons.
- Landau and AMEC, 2014. Final Remedial Investigation Report Boeing Isaacson-Thompson Site Tukwila Washington. Prepared for The Boeing Company. April 21, 2014.
- NCHRP (National Cooperative Highway Research Program), 2008. Seismic Analysis and Design of Retaining Walls, Buried Structures, Slopes and Embankments. National Cooperative Highway Research Program Report 611. Transportation Research Board.

- Palermo, M., S. Maynord, J. Miller, and D. Reible, 1998. *Guidance for In-Situ Subaqueous Capping of Contaminated Sediments*. Great Lakes National Program Office, Chicago, Illinois. EPA 905-B96-004.AASHTO, 2010.AASHTO LRFD Bridge Design Specifications. 5th ed. American Association of State and Highway Transportation Officials, Washington, D.C.
- Robertson, P.K., and K.L. Cabal, 2010. *Guide to Cone Penetration Testing for Geotechnical Engineering*. Gregg Drilling and Testing, Inc. July 2010.
- Spadaro, Philip (The Intelligence Group), 2022. Personal communication with John Laplante (Anchor QEA, LLC). May 2, 2022.
- SPU (Seattle Public Utilities), 2012. Draft Geotechnical Report Seattle Substation Evaluation Seattle, Washington Duwamish Substation. Work Authorization NS12212 MG1. November 2012.
- SPU, 2014. Geotechnical Memorandum Dallas Avenue South Drainage Project Subsurface Infiltration Recommendations. June 2014.

Terzaghi and Peck, 1967. Soil Mechanics in Engineering Practice. 2<sup>nd</sup> ed. Wiley.

- USACE (U.S. Army Corps of Engineers), 2003. Slope Stability. Engineering Manual EM 1110-2-1902.
- USDA (U.S. Department of Agriculture), 1989. Loose Riprap Protection Minnesota Technical Note 3. United States Department of Agriculture Soil Conservation Service. July 1989.

## **Figures**



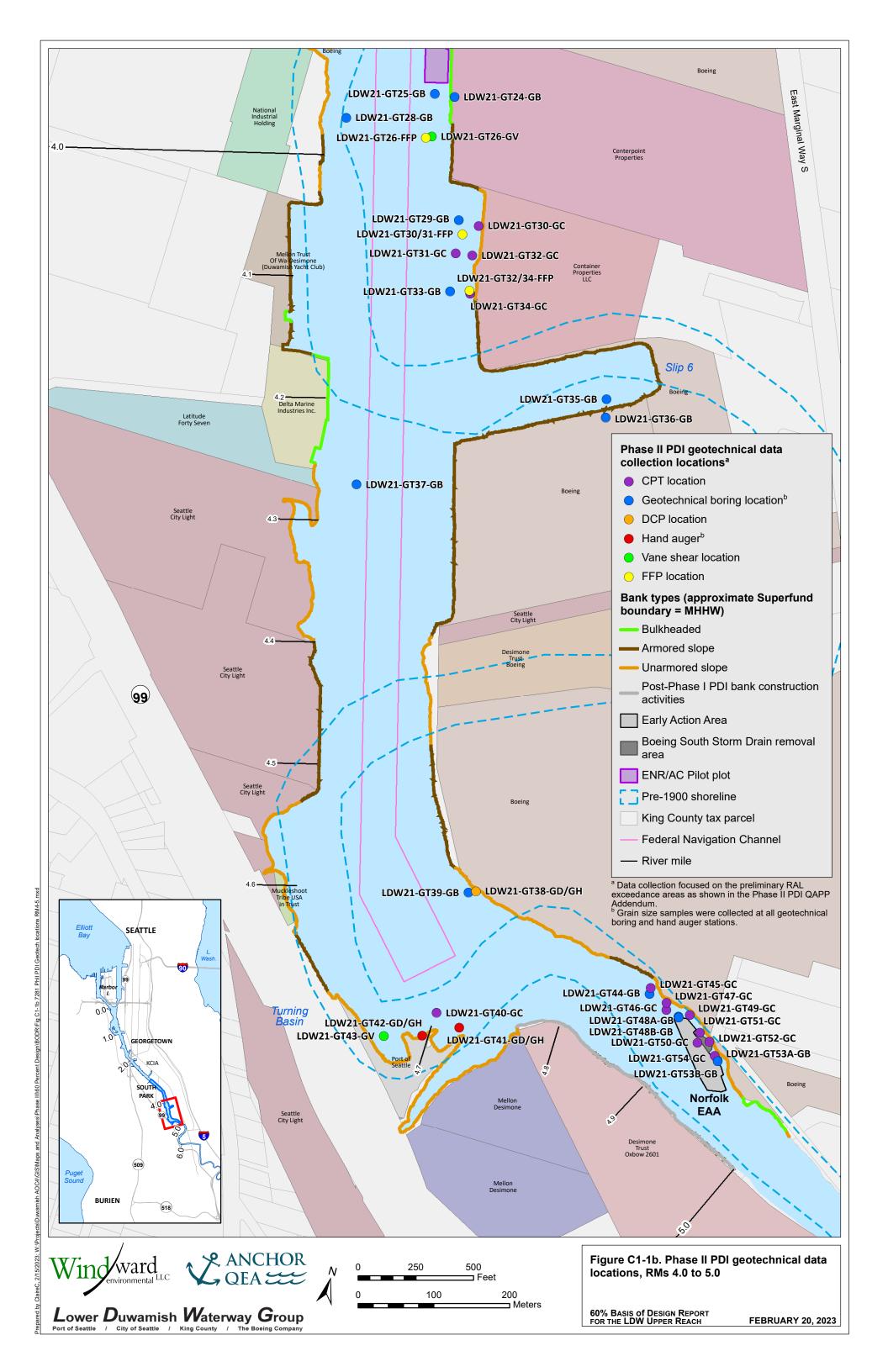
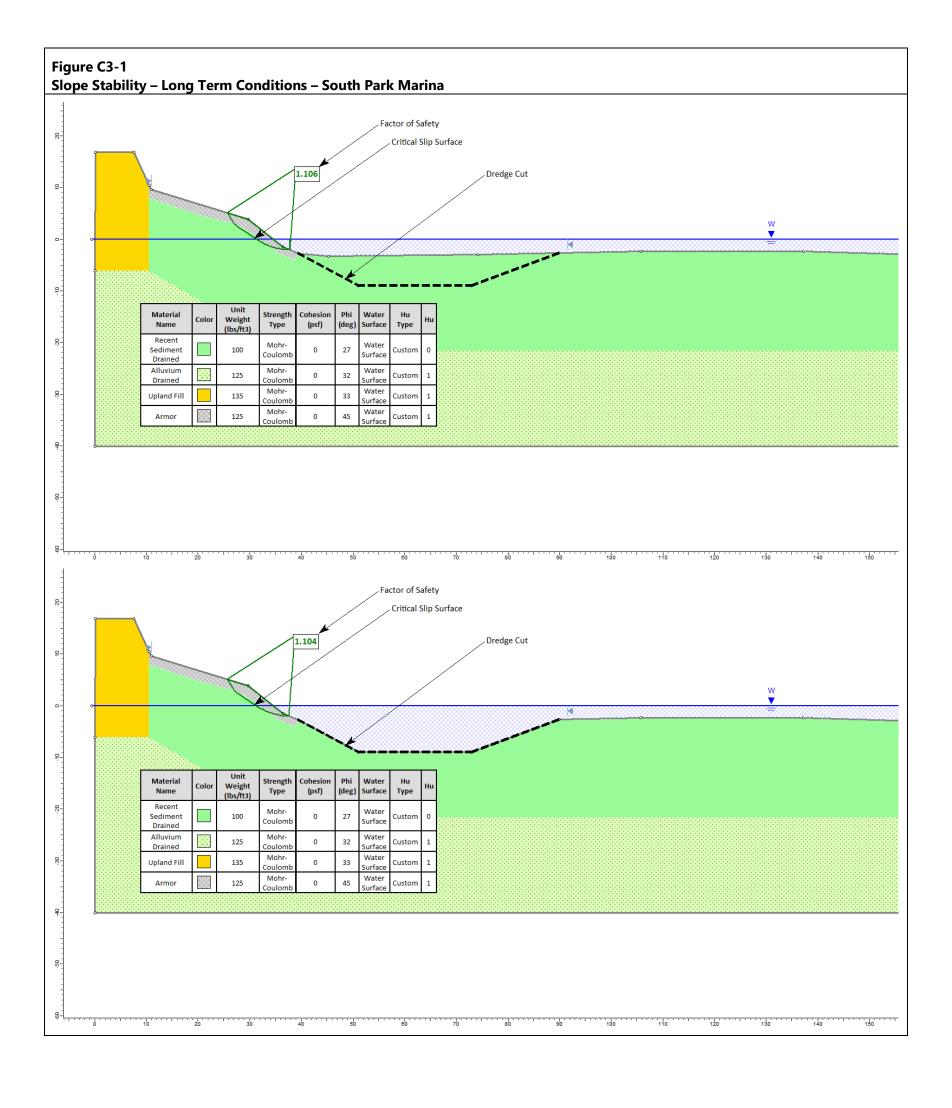


Figure C2-1 **Undrained Shear Strength Test Results and Design Assumptions** Undrained Shear Strength Measurements Peak Undrained Shear Strength (Su, PSF) 0 100 200 300 400 500 600 700 800 900 1000 0 1 2 3 4 Depth below mudline (ft) GT-01, A1 6 - GT-03, A5 GT-09, A13 GT-11, A16 7 **G**T-26, A30 **G**T-30/31, A31 • GT-32/34, A31 8 LDW21-GT04-GV LDW21-GT20-GV LDW21-GT-26-GV LDW21-GT43-GV - Design - Recent Sediments 10 • Design - Alluvium 11 12



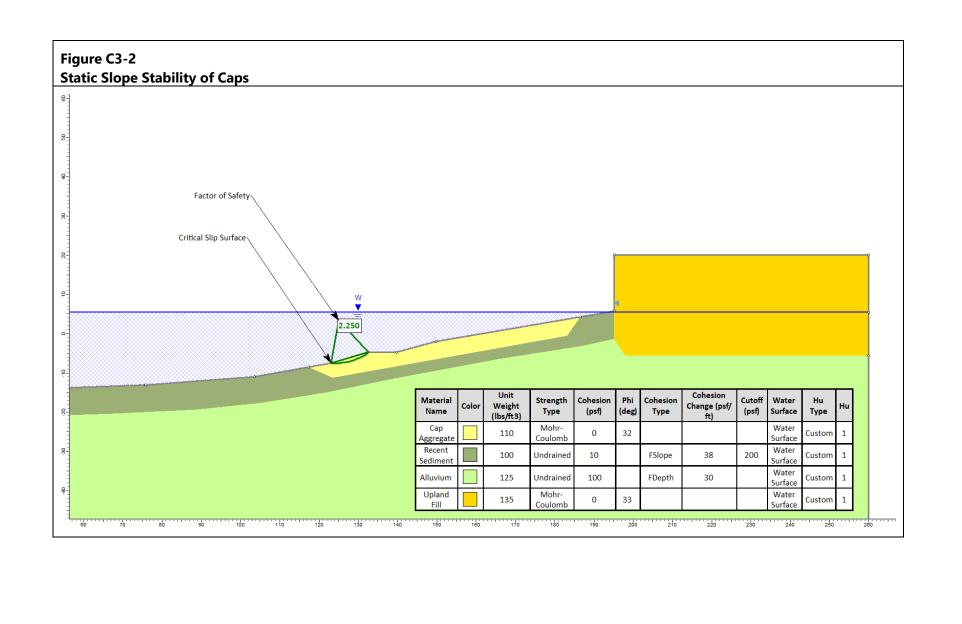
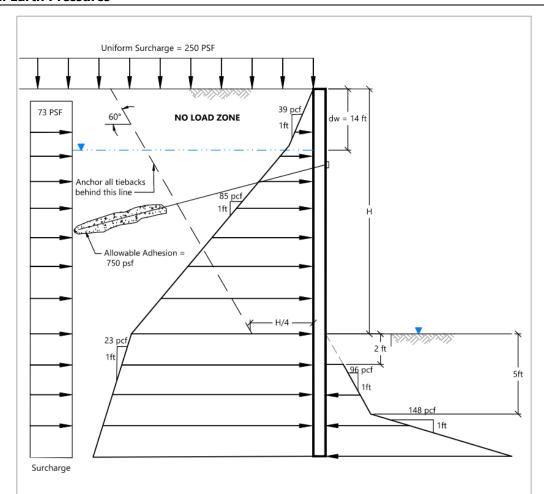


Figure C4-1 **Lateral Earth Pressures** 



- Yielding walls are those walls that will deform at least 0.001 times the height of the wall.
- 2. Passive pressures are Ultimate values and do not include a factor of safety. We recommend applying a factor of safety of at least 1.5 when computing static passive pressures.

  3. Ignore the contribution of the upper 2 feet of soil at the base of
- the wall when computing passive pressures.

  4. Active and at-rest earth pressures are for cantilever walls or walls supported by a single row of tiebacks.

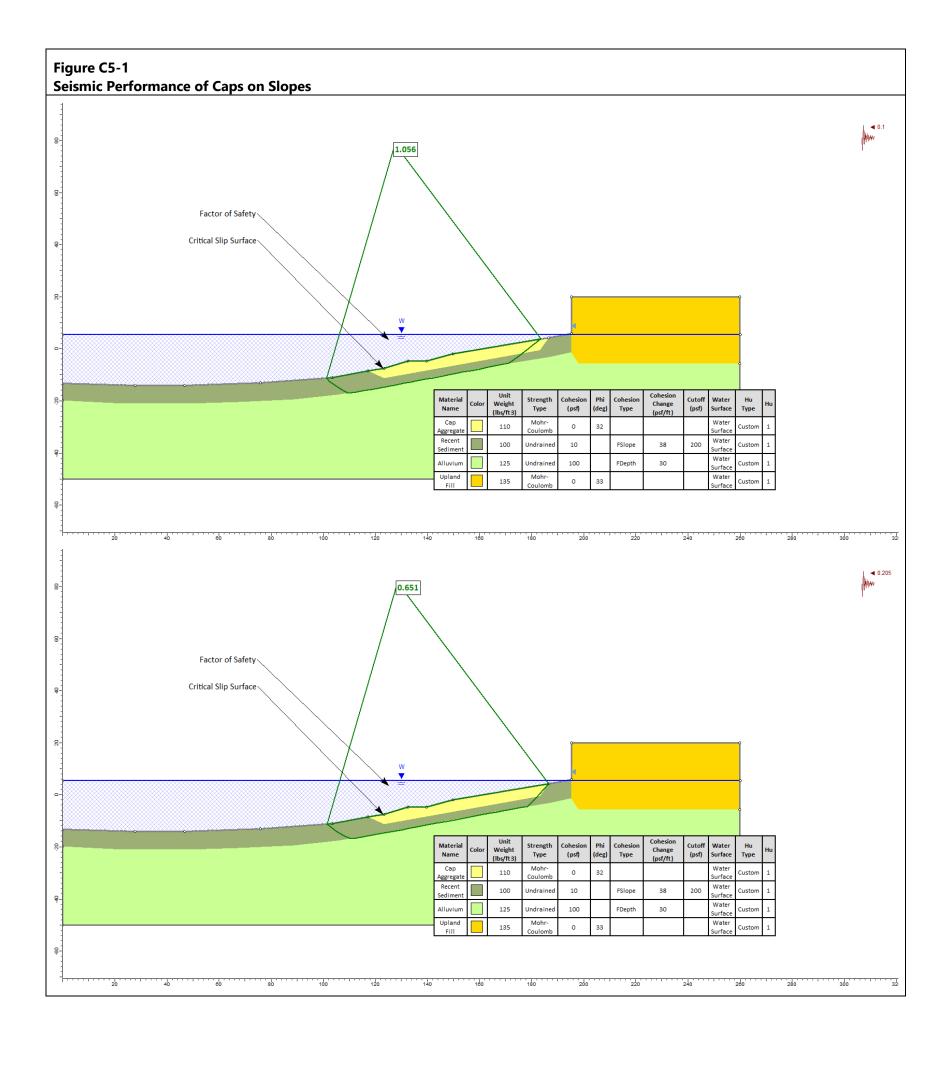
  5. Anchor pull out resistance is based on non-pressure-grouted
- straight shaft anchors. These values should be considered tentative and for planning purposes only. Actual values will need to be determined on the basis of field testing prior to construction.
- 6. Passive Pressure acts over 2 pile diameters.

Not to Scale

Passive Eart	h Pressure I	Reduction Fa	ctors
Offset Distance	Re	duction Fact	or
Offset Distance	2H:1V	1.5H:1V	1H:1V
0	0.75	0.56	0.38
2	0.85	0.66	0.48
4	0.95	0.76	0.58

Publish Date: 2023/01/23 10:03 AM | User: Jfoster Filepath: K\Projects\0067-RP-032 Lateral Earth Pressures.dwg Figure X





# Attachment A Subsurface Investigation Program and Field Logs

Boring Location: 47.511241606, -122. N:1277329.59455 E:			Hand Auger GT41 Date 8/3/21 Sheet 1 of 2 Job LDW21 Job No. 180067-02.03  Logged By Garrett Timm, Andrew B Weather 85 degrees & sunny  Excavated By Anchor QEA  Excavation Method Hand Auger 3.5' O.D.  Sampling Method NA  Bottom of Hand Auger 2 ft.
Elevation:	Datum:		Bottom of Hand Adger
SIZE (%) SAMPLE			
G S F  Max. Range Limits		Number m SAMPLE RECOVERY	DESCRIPTION: Den., moist., color, minor, MAJOR CONSTITUENT, NON-SOIL SUBSTANCES: Odor, staining, sheen, scrag, slag, etc.
	NA soil	1 0— - - 1—	(0 to 1.3 ft.) SM. very soft, moist, light brown and grey, medium grained SAND w/pockets of silt, occasional organics.
NA 90 10	NA soil	2 	(1.3 to 2 ft.)SP. very loose, wet, dark grey, SAND, minor black staining, some silt.  WT encountered @ 1.8ft.  End of Boring @ 2 feet
		3— 3— 4— 5— 6— 7— 8— 9— 10—	

Notes:

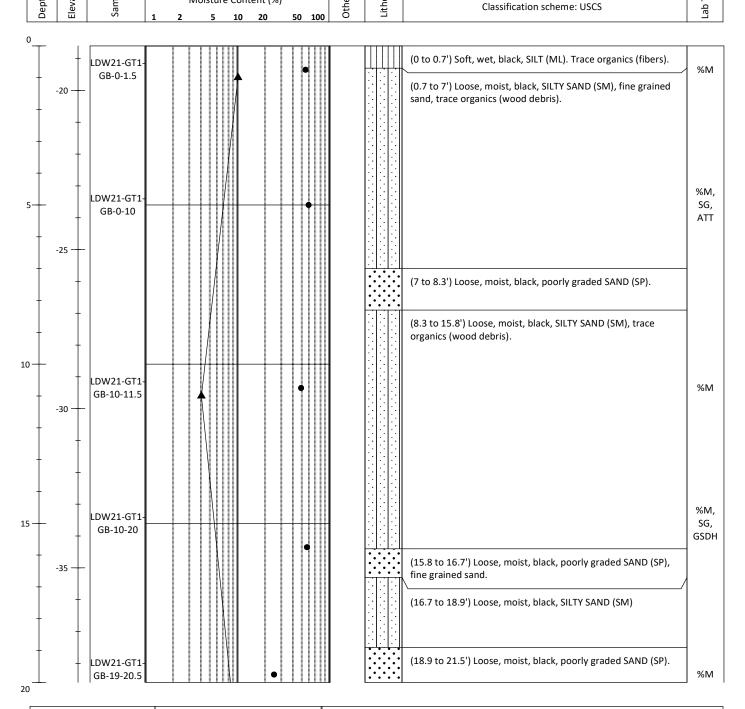


Boring Location: 47.511450999, -12 N: 1277475.27698			784999		Hand Auger GT42 Date 8/3/21 Sheet 2 of 2  Job LDW21 Job No. 180067-02.03  Logged By Garrett Timm, Andrew B Weather Excavated By Anchor QEA  Excavation Method Hand Auger 3.5' O.D.  Sampling Method NA  Bottom of Hand Auger 2.3 ft.				
Elevation:		Datum	1:						
SIZE (%)		SAM	/PLE						
G S F OO O		Number		DESCRIPTION: Den., moist., color, minor, MAJOR CONSTITUENT, NON-SOIL SUBSTANCES: Odor, staining, sheen, scrag, slag, etc.					
NA < 25 > 75	NA	soil	1		(0 to 0.2 ft.) ML. organic SILT, roots				
< 5 < 10 > 85	NA	soil	2	1—	(0.2 to 1.5 ft.)ML. very soft, moist, grey, SILT. Contains ocassional organics and brick pieces (fill) <0.5 inches				
NA > 95 < 5	NA	soil	3	2—	(1.5 to 2.3 ft.)SP. loose, moist, grey, SAND, medium grained.				
				3 — 4 — 5 — 6 — 7 — 8 — 9 — 10 — 10 — 10 — 10 — 10 — 10 — 10					

Notes:



## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1273353.682 Total Depth (ft): 21.5 N/LAT: 197701.636 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.09.21 Mudline Elevation (ft): -18.6 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)



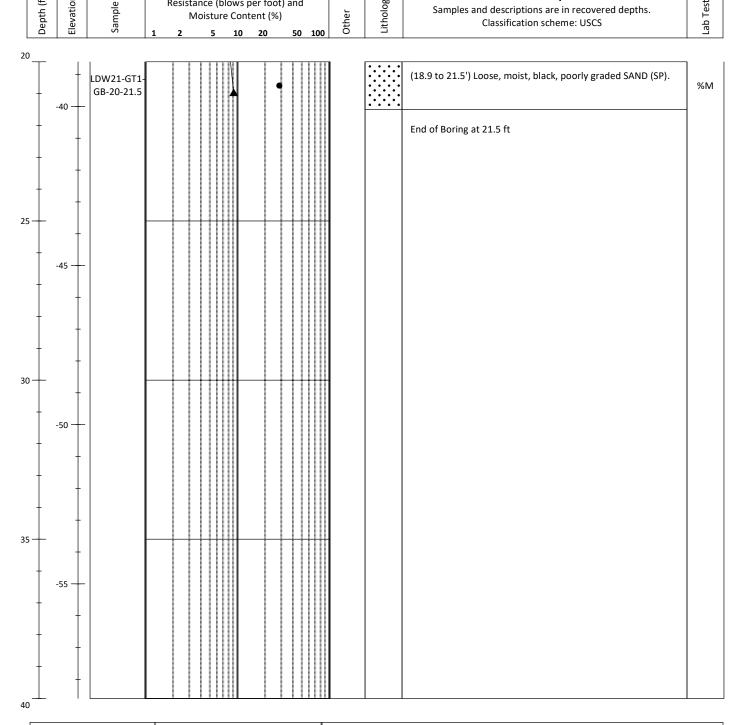


SPT N-Value

• Moisture Content (%)

## Notes:

## [DRAFT] Soil Boring Log Sheet 2 of 2 LDW21-GT1-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 197701.636 E/LONG: 1273353.682 Total Depth (ft): 21.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.09.21 Mudline Elevation (ft): -18.6 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Resistance (blows per foot) and Sample I





- SPT N-Value
- Moisture Content (%)

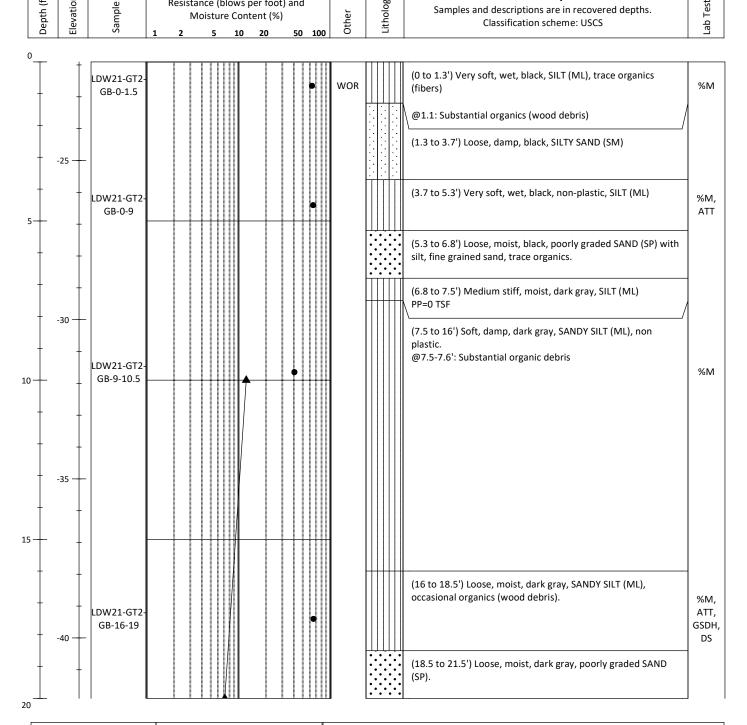
Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

Samples and descriptions are in recovered depths.

Classification scheme: USCS

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1273794.399 Total Depth (ft): 21.5 N/LAT: 197328.101 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.09.21 Mudline Elevation (ft): -21.9 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ Soil Description $\stackrel{\boxplus}{\exists}$ Elevation Resistance (blows per foot) and Test Samples and descriptions are in recovered depths. Moisture Content (%)





- SPT N-Value
- Moisture Content (%)

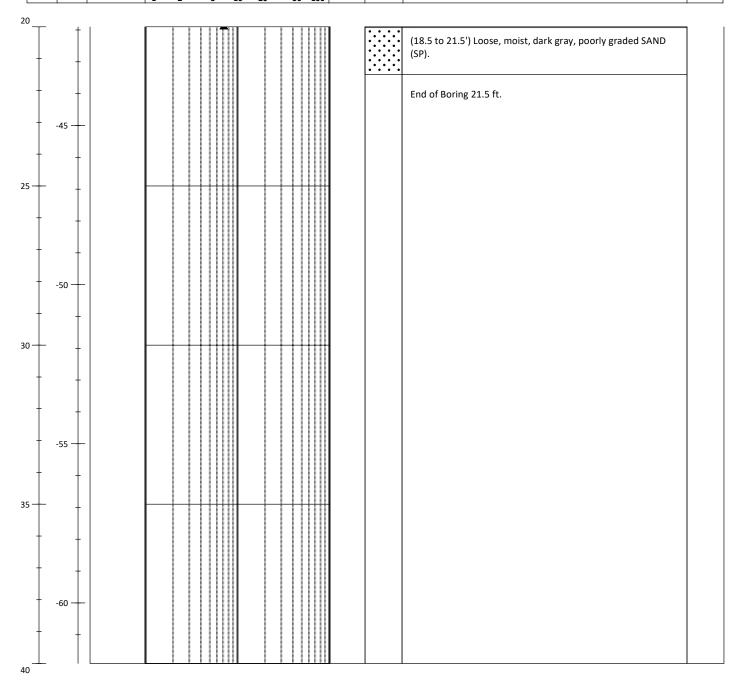
## Notes:

## [DRAFT] Soil Boring Log

Sheet 2 of 2

Project #: 180067-02.03	Project: LDW Upper Reach Phase 2 Investigation	Method: Rotary Sonic
Location: Seattle, WA	N/LAT: <b>197328.101</b> E/LONG: <b>1273794.399</b>	Total Depth (ft): 21.5
Client: Lower Duwamish Waterway Group	Horiz. Datum: Washington State Plane Coordinate North	Observed Depth to Mudline (ft): 23.2
Collection Date: 07.09.21	North American Datum of 1983, U.S. Feet	Mudline Elevation (ft): -21.9
Contractor: Holocene Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)	Hammer: 140-lb, 30-in drop, Auto
Logged By: Casey Janisch	Sampler(s): Split Spoon & Shelby Tube Sampler	Hammer Efficiency (%): 99

th (ft)	ation (ft)	ple ID	Uncorrected Standard Penetration Resistance (blows per foot) and	ı	ygolc	Soil Description Samples and descriptions are in recovered depths.	Fest
Depth	Elevati	Sampl	Moisture Content (%)	Other	Litholo	Samples and descriptions are in recovered depths.  Classification scheme: USCS	Lab Te

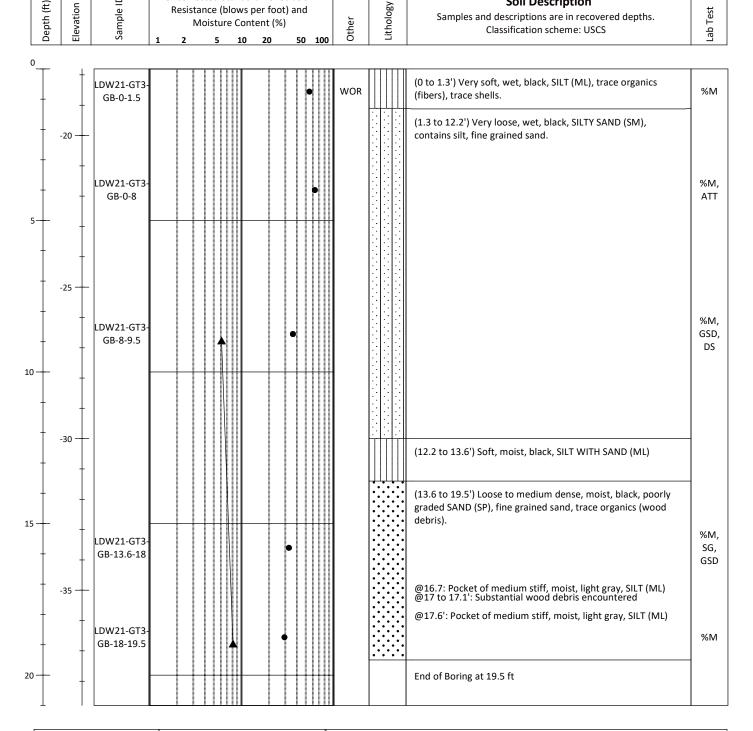




- SPT N-Value
- Moisture Content (%)

## lotes:

## [DRAFT] Soil Boring Log Sheet 1 of 1 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1274303.5483 Total Depth (ft): 19.5 N/LAT: 196838.0251 Client: Lower Duwamish Waterway Group Horiz. Datum: Washington State Plane Coordinate North Observed Depth to Mudline (ft): North American Datum of 1983, U.S. Feet Collection Date: 07.14.21 Mudline Elevation (ft): -17.8 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** $\equiv$ Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.



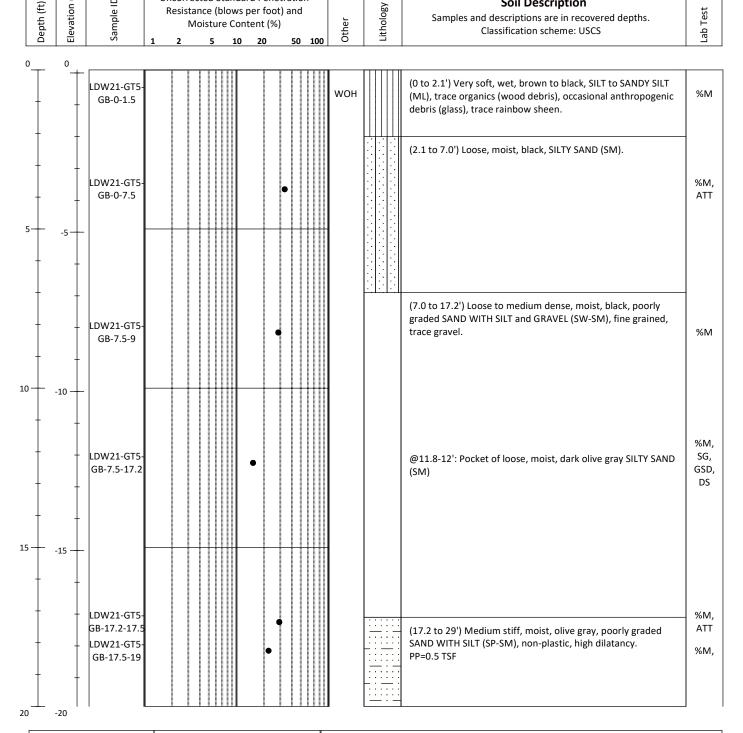


SPT N-Value

• Moisture Content (%)

## Notes:

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1274408.737 Total Depth (ft): 29 N/LAT: 196515.647 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 8.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.19.21 Mudline Elevation (ft): 0.1 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Resistance (blows per foot) and Test





SPT N-Value

Moisture Content (%)

Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

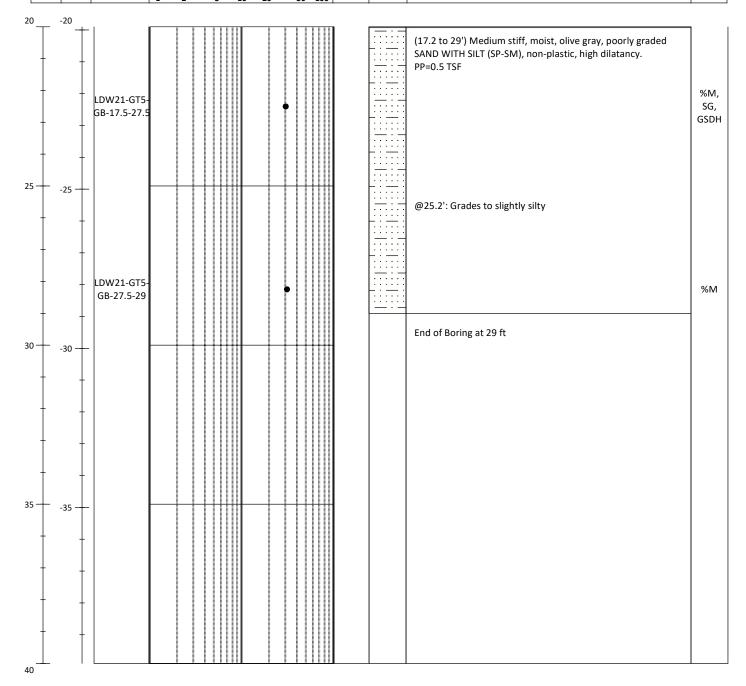
Samples and descriptions are in recovered depths.

## [DRAFT] Soil Boring Log LDW21-GT5-GB Project: LDW Upper Reach Phase 2 Investigation Method: Ro

Sheet 2 of 2

Project #: 180067-02.03	Project: LDW Upper Reach Phase 2 Investigation	Method: Rotary Sonic
Location: Seattle, WA	N/LAT: <b>196515.647</b> E/LONG: <b>1274408.737</b>	Total Depth (ft): 29
Client: Lower Duwamish Waterway Group	Horiz. Datum: Washington State Plane Coordinate North	Observed Depth to Mudline (ft): 8.5
Collection Date: 07.19.21	North American Datum of 1983, U.S. Feet	Mudline Elevation (ft): 0.1
Contractor: Holocene Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)	Hammer: 140-lb, 30-in drop, Auto
Logged By: Casey Janisch	Sampler(s): Split Spoon & Shelby Tube Sampler	Hammer Efficiency (%): 99

pth (ft)	evation (ft)	ımple ID	Uncorrected Standard Penetration Resistance (blows per foot) and Moisture Content (%)	her	:hology	Soil Description  Samples and descriptions are in recovered depths.  Classification scheme: USCS	b Test
Dер	Elev	San	1 2 5 10 20 50 100	Oth	Lith	Classification scheme: USCS	Lab





- SPT N-Value
- Moisture Content (%)

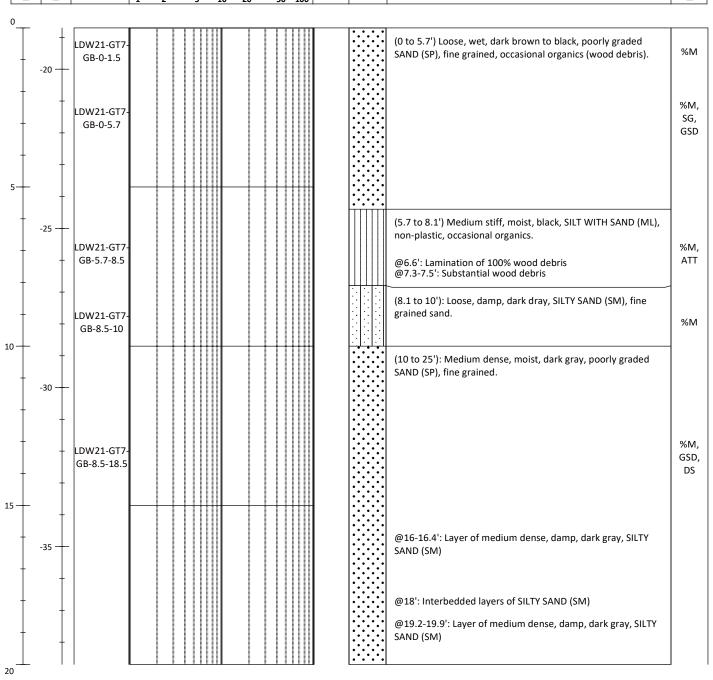
## Notes:

## [DRAFT] Soil Boring Log

Sheet 1 of 2

17.5
1
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th (ft)	ation (ft)	ple ID	Uncorrected Standard Penetration Resistance (blows per foot) and	er	logy	<b>Soil Description</b> Samples and descriptions are in recovered depths.	Fest
Depth	Elevati	Sampl	Moisture Content (%)	Other	Litholc	Samples and descriptions are in recovered depths. Classification scheme: USCS	Lab Te





- SPT N-Value
- Moisture Content (%)

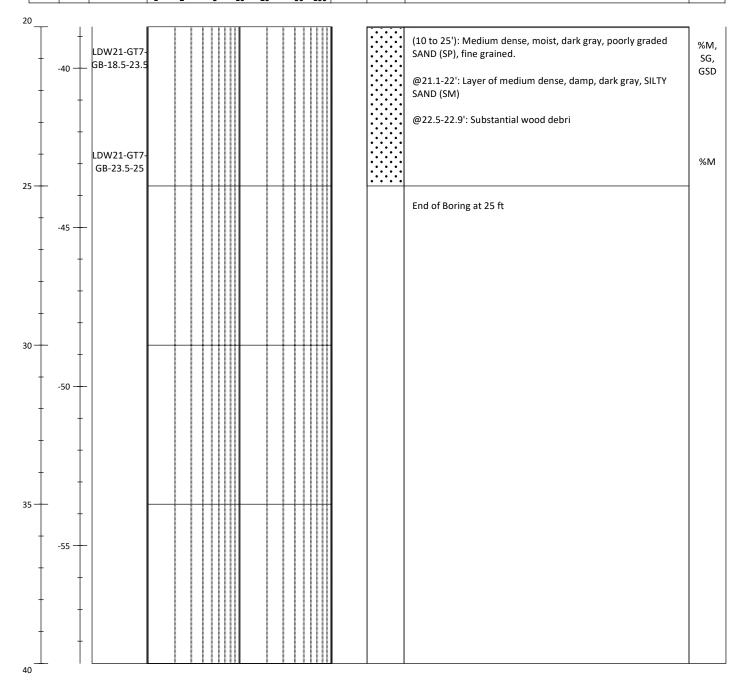
## lotes:

## [DRAFT] Soil Boring Log

Sheet 2 of 2

Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic	Project: LDW Upper Reach Phase 2 Inves	Project #: 180067-02.03		
N/LAT: 196544.595 E/LONG: 1274698.428 Total Depth (ft): 25	N/LAT: <b>196544.595</b> E/LONG:	Location: Seattle, WA		
Horiz. Datum: Washington State Plane Coordinate North Observed Depth to Mudline (ft): 17.5	Horiz. Datum: Washington State Plane Co	Client: Lower Duwamish Waterway Group  Collection Date: 07.09.21		
North American Datum of 1983, U.S. Feet Mudline Elevation (ft): -18.7	North American Datum of			
Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto	Vert. Datum: Mean Lower Low Water (ML	Contractor: Holocene Drilling, Inc		
Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99	Sampler(s): Split Spoon & Shelby Tube S	Logged By: Casey Janisch		
N/LAT: 196544.595 E/LONG: 1274698.428 Total Depth (ft): 25  Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet  Vert. Datum: Mean Lower Low Water (MLLW)  Total Depth (ft): 25  Observed Depth to Mudline (ft): 17  Mudline Elevation (ft): -18.7  Hammer: 140-lb, 30-in drop, Auto	N/LAT: 196544.595 E/LONG: Horiz. Datum: Washington State Plane Control North American Datum of Vert. Datum: Mean Lower Low Water (ML	Location: Seattle, WA  Client: Lower Duwamish Waterway Group  Collection Date: 07.09.21  Contractor: Holocene Drilling, Inc		

pth (ft)	evation (ft)	ımple ID	Uncorrected Standard Penetration Resistance (blows per foot) and Moisture Content (%)	her	hology	Soil Description  Samples and descriptions are in recovered depths.  Classification scheme: USCS	b Test
Dep	Elev	San	1 2 5 10 20 50 100	Oth	Lith	Classification scheme: USCS	Lab

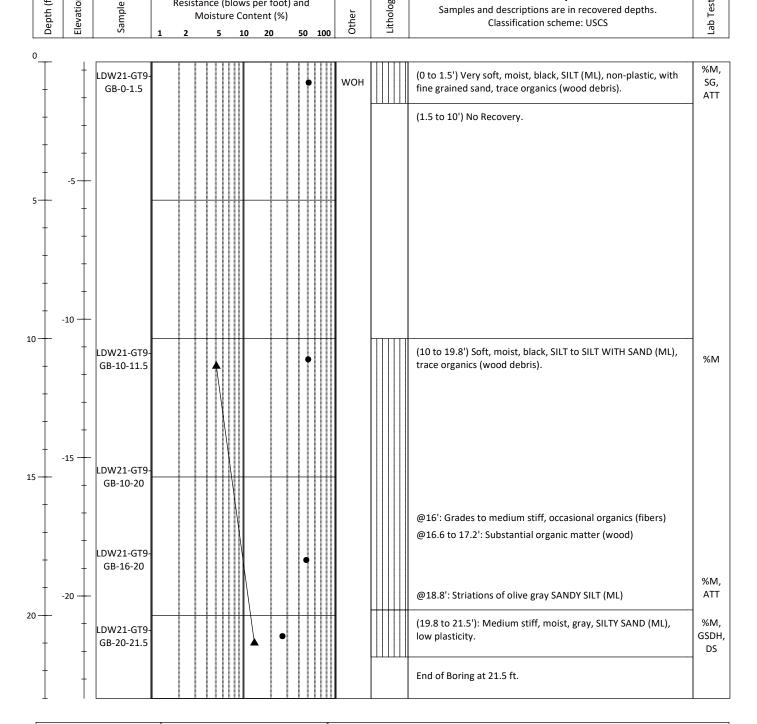




- SPT N-Value
- Moisture Content (%)

## Notes:

## [DRAFT] Soil Boring Log Sheet 1 of 1 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1275283.558 Total Depth (ft): 21.5 N/LAT: 195927.181 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 11.2 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.08.21 Mudline Elevation (ft): -0.7 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.



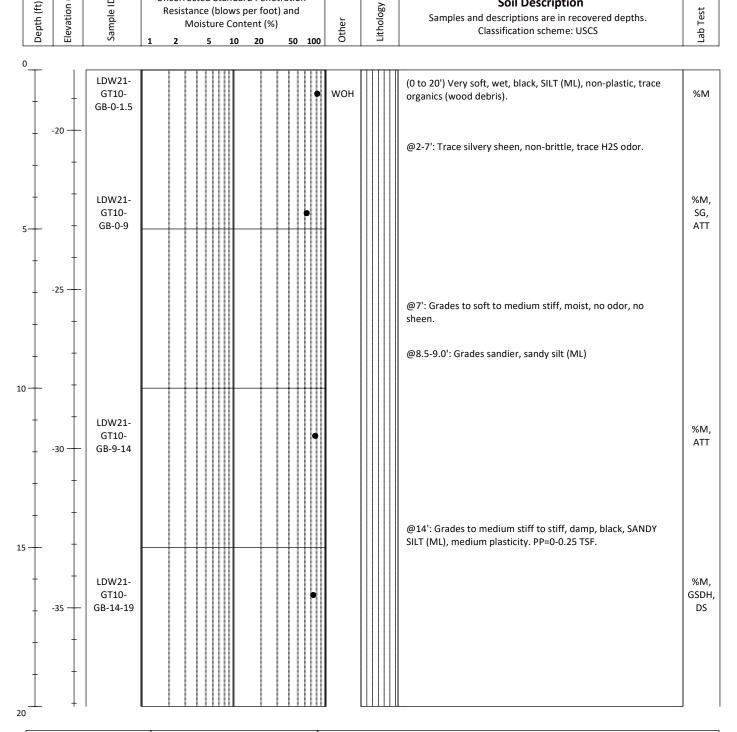


SPT N-Value

• Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT10-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 195631.266 E/LONG: 1275691.841 Total Depth (ft): 25.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.07.21 Mudline Elevation (ft): -18.1 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration**

Lithology





 $\Box$ 

Resistance (blows per foot) and

Moisture Content (%)

- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

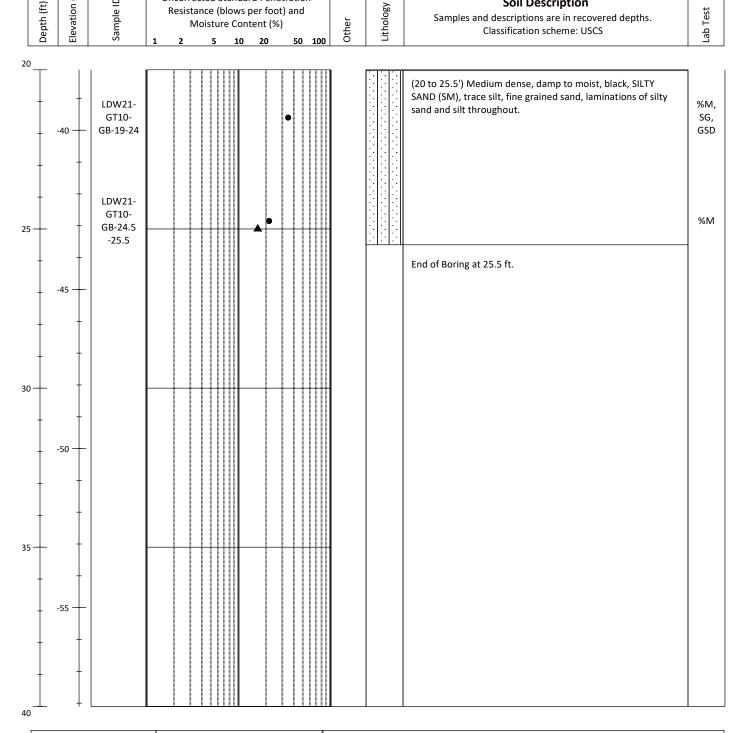
**Soil Description** 

Samples and descriptions are in recovered depths.

Classification scheme: USCS

Test

## [DRAFT] Soil Boring Log Sheet 2 of 2 LDW21-GT10-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 195631.266 E/LONG: 1275691.841 Total Depth (ft): 25.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.07.21 Mudline Elevation (ft): -18.1 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration**





 $\Box$ 

Resistance (blows per foot) and

Moisture Content (%)

SPT N-Value

Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

**Soil Description** 

Samples and descriptions are in recovered depths.

Classification scheme: USCS

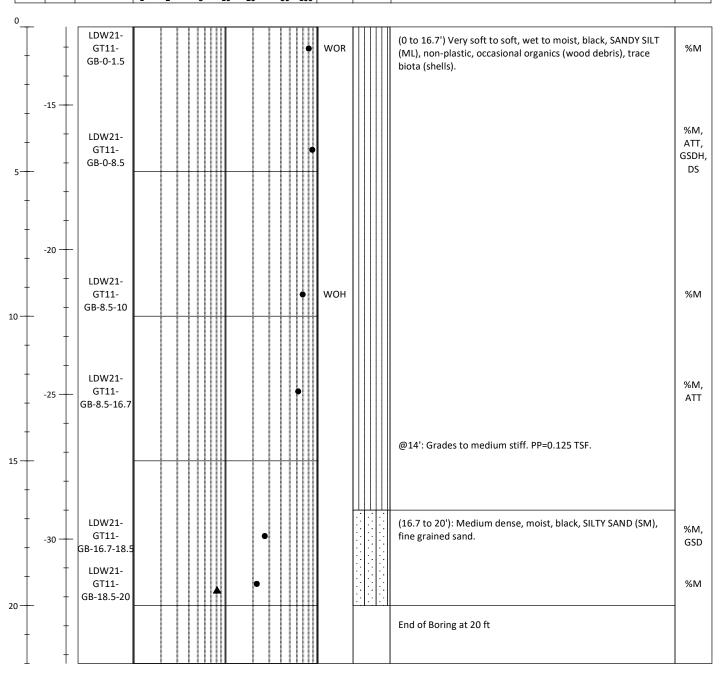
Test

## [DRAFT] Soil Boring Log

Sheet 1 of 1

Project #: 180067-02.03	Project: LDW Upper Reach Phase 2 Investigation	Method: Rotary Sonic
Location: Seattle, WA	N/LAT: <b>195423.544</b> E/LONG: <b>1275688.731</b>	Total Depth (ft): 20
Client: Lower Duwamish Waterway Group	Horiz. Datum: Washington State Plane Coordinate North	Observed Depth to Mudline (ft): 18.7
Collection Date: 07.08.21	North American Datum of 1983, U.S. Feet	Mudline Elevation (ft): -12.3
Contractor: Holocene Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)	Hammer: 140-lb, 30-in drop, Auto
Logged By: Casey Janisch	Sampler(s): Split Spoon & Shelby Tube Sampler	Hammer Efficiency (%): 99
		· · · · · · · · · · · · · · · · · · ·

Depth (ft)	ation (ft)	ple ID	Uncorrected Standard Penetration Resistance (blows per foot) and	er ology	Soil Description Samples and descriptions are in recovered depths.	lest
	Elevatio	Sample	Moisture Content (%)	Other	Samples and descriptions are in recovered depths.  Classification scheme: USCS	Lab Tes

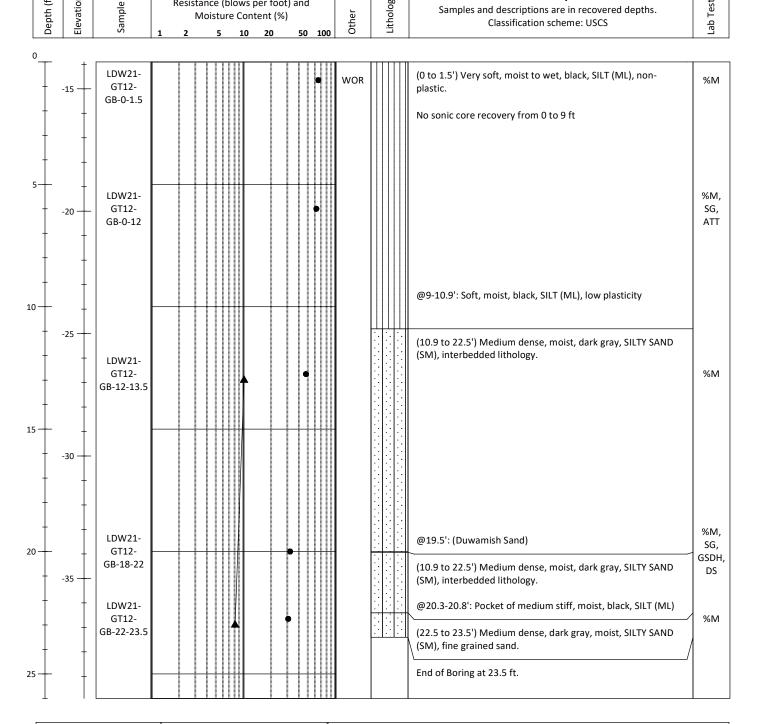




- SPT N-Value
- Moisture Content (%)

## lotes:

## [DRAFT] Soil Boring Log Sheet 1 of 1 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1275845.395 Total Depth (ft): 23.5 N/LAT: 195269.116 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.08.21 Mudline Elevation (ft): -13.9 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.

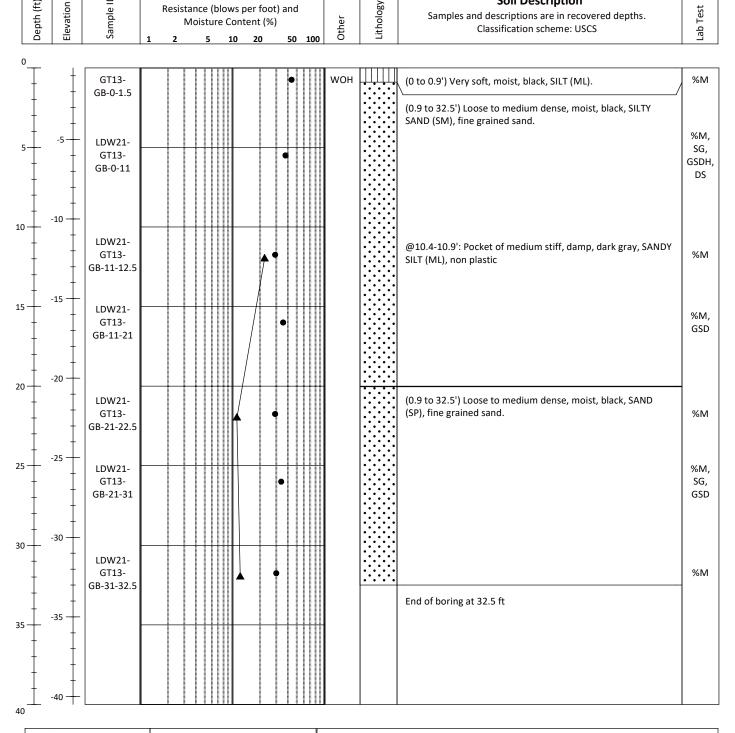




SPT N-Value

• Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 1 of 1 LDW21-GT13-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 195063.55 E/LONG: 1276022.385 Total Depth (ft): 32.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 5.0 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.12.21 Mudline Elevation (ft): -0.5 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Resistance (blows per foot) and





Moisture Content (%)

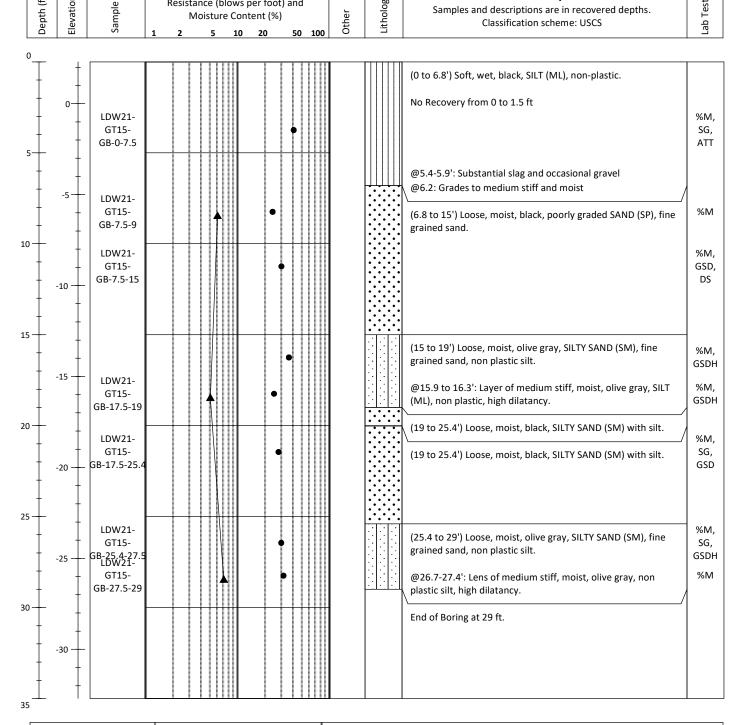
%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

Test

Samples and descriptions are in recovered depths.

Classification scheme: USCS

## [DRAFT] Soil Boring Log Sheet 1 of 1 LDW21-GT15-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1276096.292 Total Depth (ft): 29 N/LAT: 194770.977 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.12.21 Mudline Elevation (ft): 2.3 Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ Soil Description $\mathbb{E}$ Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.



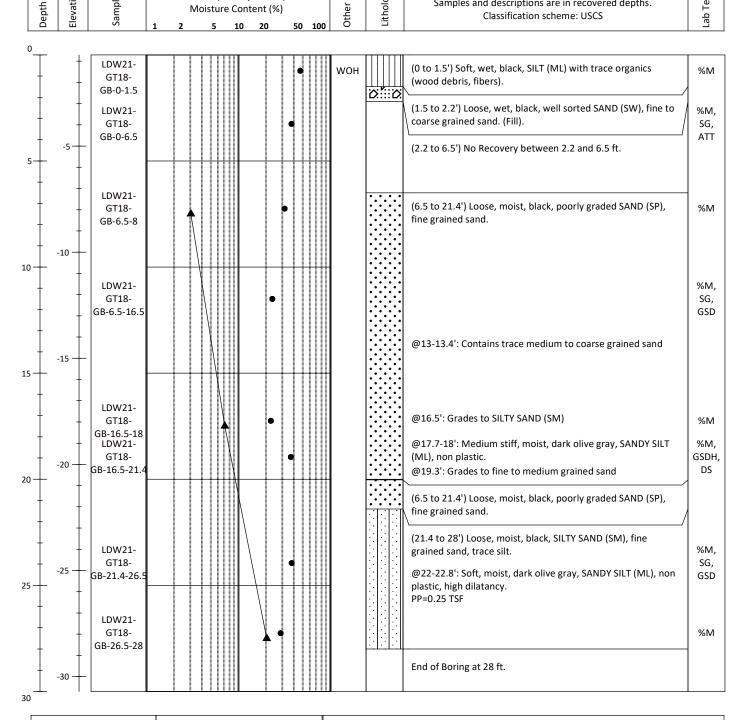


SPT N-Value

Moisture Content (%)

Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 1 of 1 LDW21-GT18-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1276175.936 Total Depth (ft): 28 N/LAT: 194509.577 Observed Depth to Mudline (ft): 9.5 Client: Lower Duwamish Waterway Group Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.13.21 Mudline Elevation (ft): -0.7 Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** Δ Soil Description $\mathbb{E}$ Elevation Resistance (blows per foot) and Lithology Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

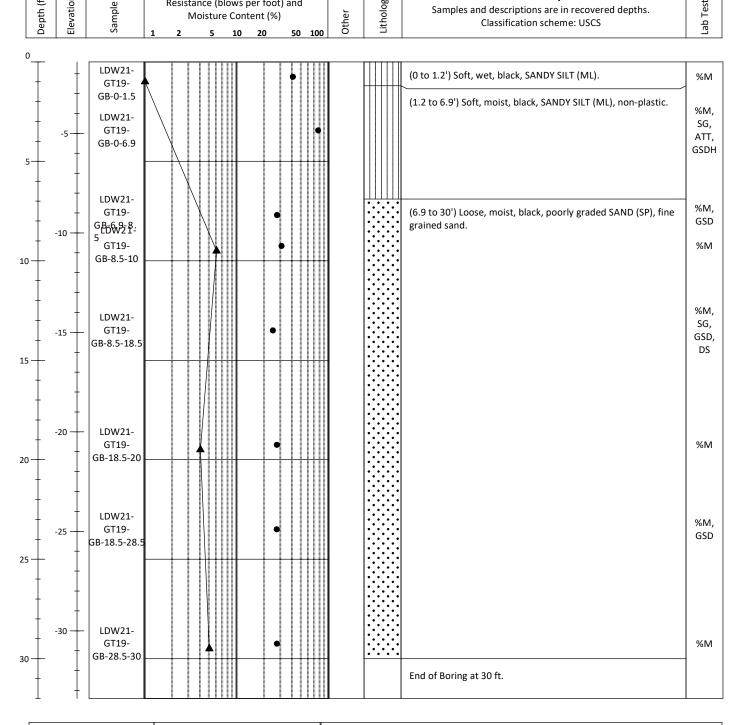




SPT N-Value

Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 1 of 1 LDW21-GT19-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 194619.686 E/LONG: 1275815.459 Total Depth (ft): 30 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.13.21 Mudline Elevation (ft): -1.4 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** $\stackrel{\boxplus}{\exists}$ Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths. Moisture Content (%)





- SPT N-Value
- Moisture Content (%)

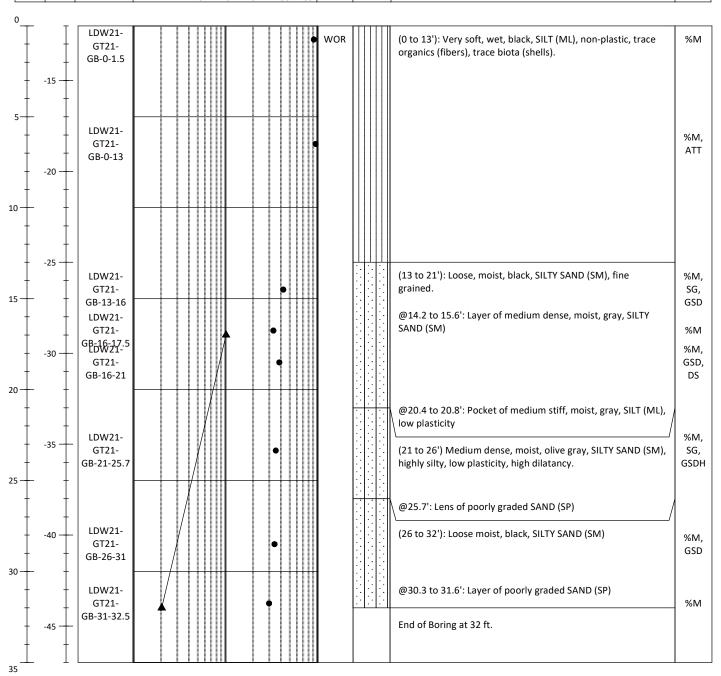
## lotes:

# [DRAFT] Soil Boring Log LDW21-GT21-GB

Sheet 1 of 1

Project #: 180067-02.03	Project: LDW Upper Reach Phase 2 Investigation	Method: Rotary Sonic
Location: Seattle, WA	N/LAT: <b>194223.416</b> E/LONG: <b>1276127.19</b>	Total Depth (ft): 32.5
Client: Lower Duwamish Waterway Group	Horiz. Datum: Washington State Plane Coordinate North	Observed Depth to Mudline (ft): 11.2
Collection Date: 07.08.21	North American Datum of 1983, U.S. Feet	Mudline Elevation (ft): -12.0
Contractor: Holocene Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)	Hammer: 140-lb, 30-in drop, Auto
Logged By: Casey Janisch	Sampler(s): Split Spoon & Shelby Tube Sampler	Hammer Efficiency (%): 99

pth (ft)	vation (ft)	mple ID	Uncorrected Standard Penetration Resistance (blows per foot) and Moisture Content (%)	ner hology	Soil Description Samples and descriptions are in recovered depths.	Test
Deptl	Eleva	Samp	Moisture Content (%)  1 2 5 10 20 50 100	Othe	Classification scheme: USCS	Lab T

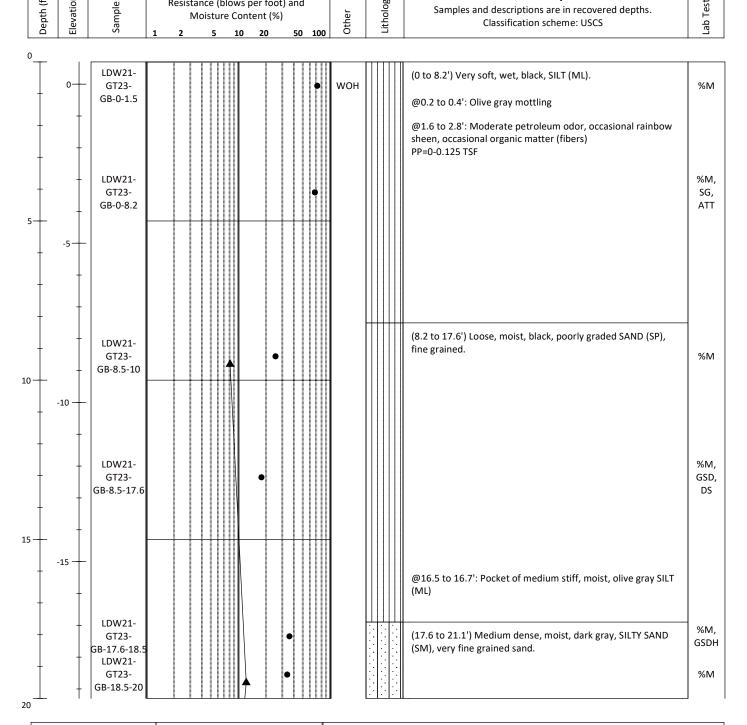




- SPT N-Value
- Moisture Content (%)

# Notes:

## [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT23-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1276262.681 Total Depth (ft): 32 N/LAT: 194225.679 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.16.21 Mudline Elevation (ft): 0.7 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Resistance (blows per foot) and Lithology Test Samples and descriptions are in recovered depths.



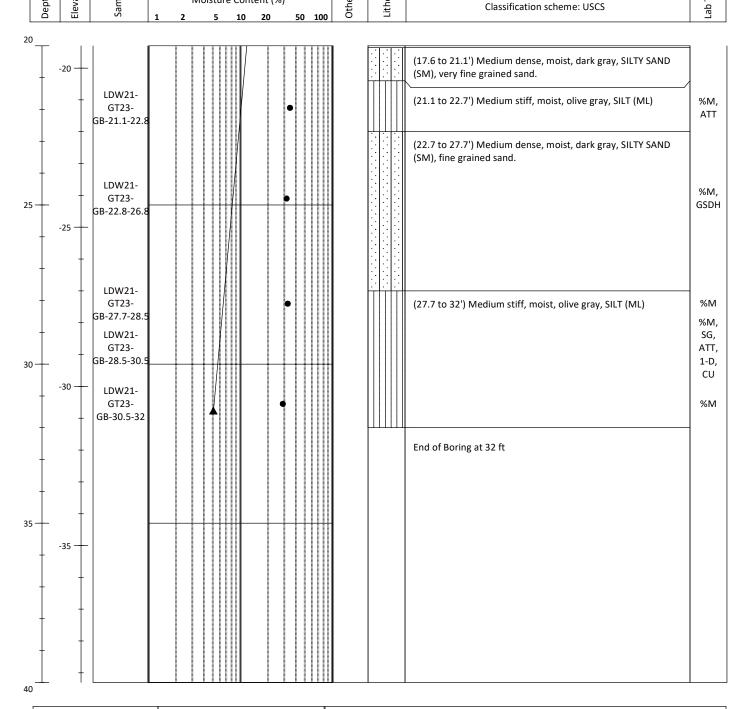


SPT N-Value

Moisture Content (%)

Moisture Content (%)

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 194225.679 E/LONG: 1276262.681 Total Depth (ft): 32 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.16.21 Mudline Elevation (ft): 0.7 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

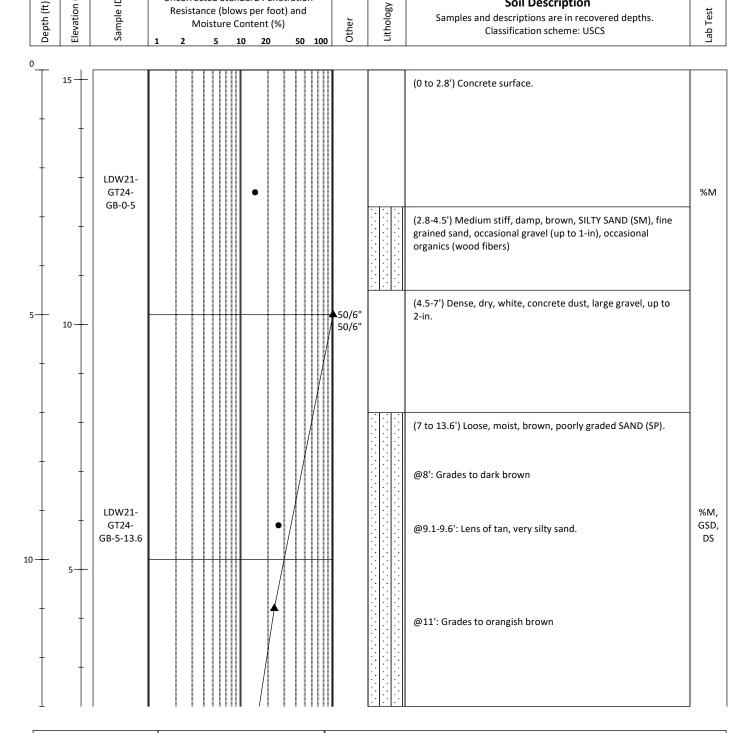




- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

## [DRAFT] Soil Boring Log Sheet 1 of 5 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193910.921 E/LONG: 1276412.765 Total Depth (ft): 61.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (MA Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 7.26.21 Surface Elevation (ft): 15.2 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Sam Giannakos Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Resistance (blows per foot) and Samples and descriptions are in recovered depths.

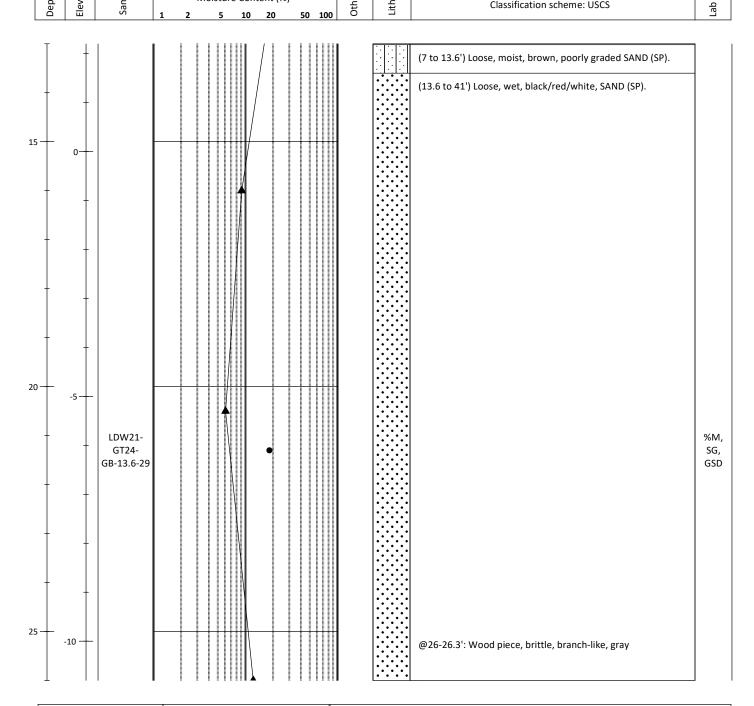




- SPT N-Value
- Moisture Content (%)

# Notes:

				_	il Bc -GT24	oring Log -GB	Sheet 2 o	f 5
Project #:	#: <b>180067-02.0</b> 3	3	Project: LDW Upper Reach Phase 2 Investigation				Method: Rotary Sonic	
Location:	: Seattle, WA		N/LAT: 193910.9	21	E,	/LONG: <b>1276412.765</b>	Total Depth (ft): 61.5	
Client: L	Lower Duwamis	sh Waterway Group	Horiz. Datum: Washington State Plane Coordinate North				Observed Depth to Mudline (14)	
Collection	on Date: <b>7.26.2</b>	1	North American Datum of 1983, U.S. Feet				Surface Elevation (ft): 15.2	
Contracto	tor: Holocene	Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)				Hammer: 140-lb, 30-in drop, Auto	)
Logged B	By: Sam Giann	akos	Sampler(s): Spl	it Spoon	& Shelb	y Tube Sampler	Hammer Efficiency (%): 99	
epth (f	Elevation (ft)	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and ntent (%)	Other	Lithology	Samples and descript	<b>Description</b> tions are in recovered depths. tion scheme: USCS	Lab Test



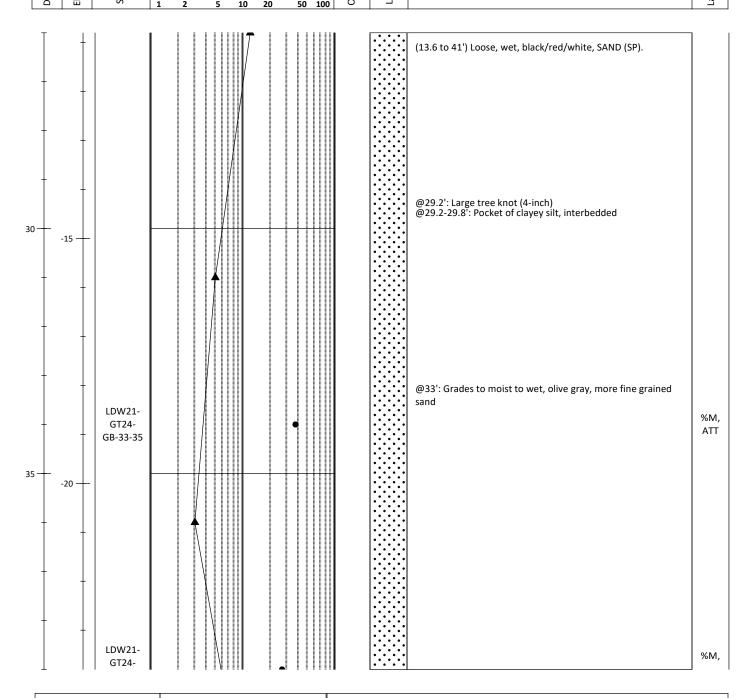


SPT N-Value

• Moisture Content (%)

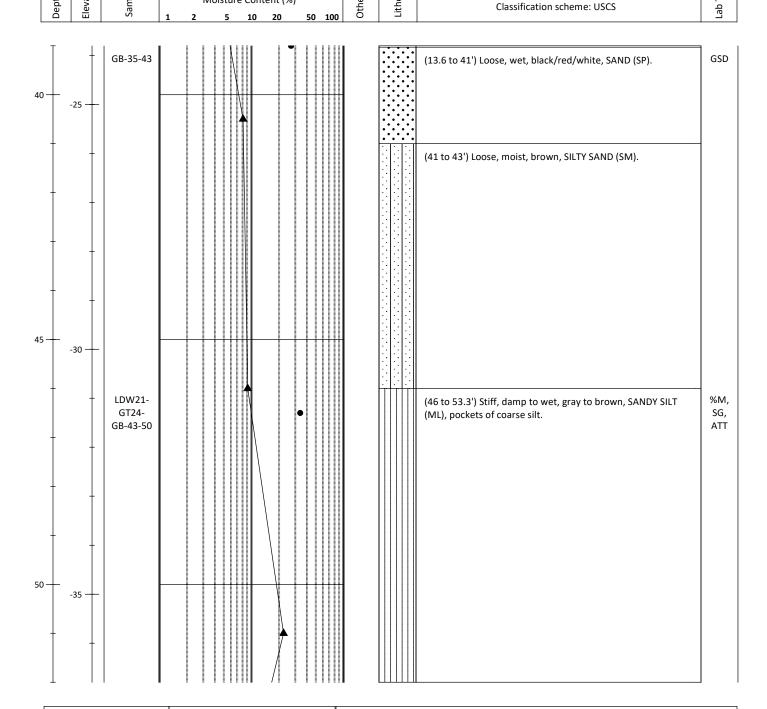
Notes:

#### [DRAFT] Soil Boring Log Sheet 3 of 5 LDW21-GT24-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193910.921 E/LONG: 1276412.765 Total Depth (ft): 61.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (M) Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 7.26.21 Surface Elevation (ft): Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Sam Giannakos Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I ab Test Samples and descriptions are in recovered depths. Moisture Content (%)





#### [DRAFT] Soil Boring Log Sheet 4 of 5 LDW21-GT24-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193910.921 E/LONG: 1276412.765 Total Depth (ft): 61.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (NA Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 7.26.21 Surface Elevation (ft): Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Sam Giannakos Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)

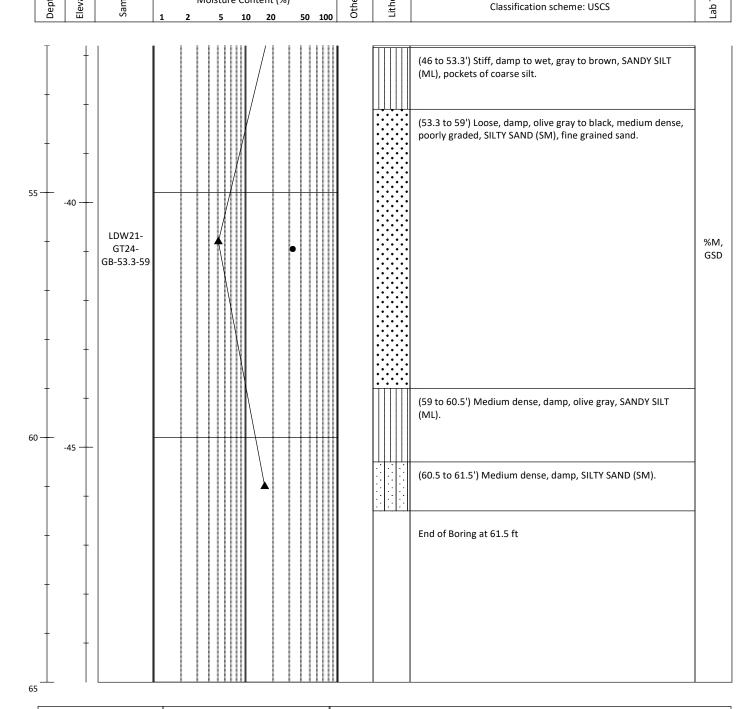




SPT N-Value

• Moisture Content (%)

[DRAFT] Soil Boring Log LDW21-GT24-GB								Sheet 5 o	f 5
Proje	ct #: 1	80067-02.03		Project: LDW Upper Reach Phase 2 Investigation				Method: Rotary Sonic	
Locat	tion: S	eattle, WA		N/LAT: 193910.921 E/LONG: 1276412.765			Total Depth (ft): 61.5		
Clien	t: Low	er Duwamish	Waterway Group	Horiz. Datum: Washington State Plane Coordinate North				Observed Depth to Mudline (NA	
Colle	ction D	ate: <b>7.26.21</b>		N	orth Am	erican Da	Surface Elevation (ft): 15.2		
Cont	ractor:	Holocene D	rilling, Inc	Vert. Datum: Me	an Lowe	r Low W	Hammer: 140-lb, 30-in drop, Auto		
Logg	ed By:	Sam Giannak	cos	Sampler(s): Spl	it Spoon	& Shelb	y Tube Sampler	Hammer Efficiency (%): 99	
th (ft)	ation (ft)	nple ID	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and	er foot) and Samples and descriptions			Description tions are in recovered depths.	Test

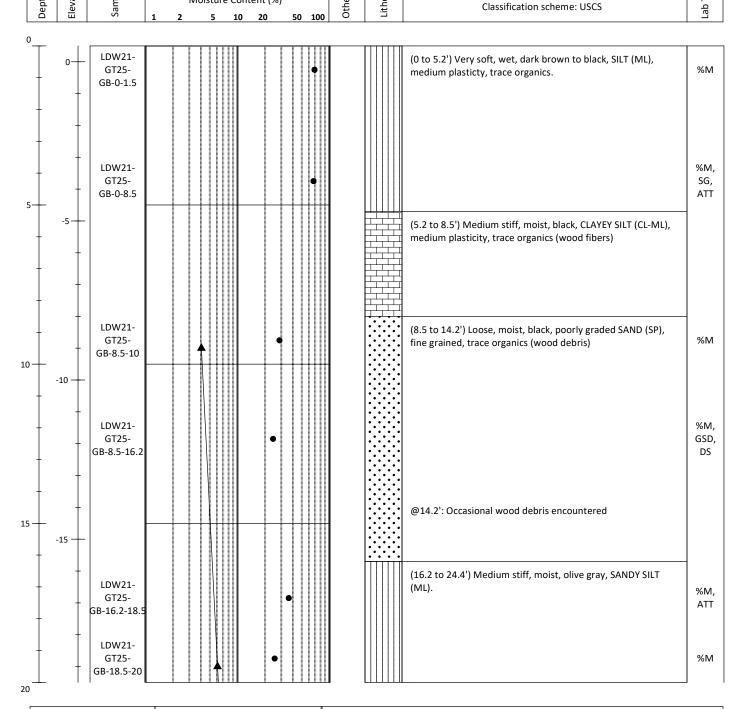




- SPT N-Value
- Moisture Content (%)

# Notes:

#### [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT25-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193902.768 E/LONG: 1276326.832 Total Depth (ft): 30 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.15.21 Mudline Elevation (ft): 0.5 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Resistance (blows per foot) and Lithology Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)



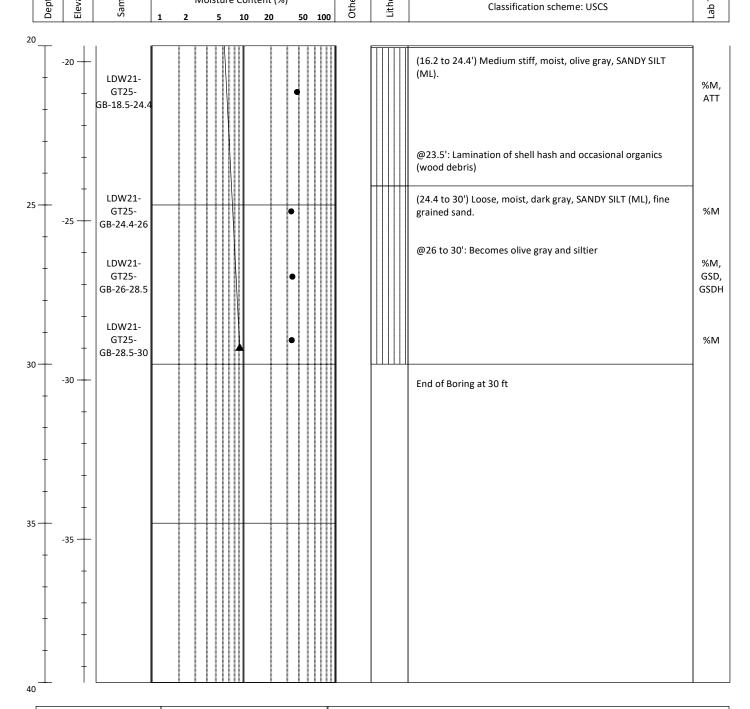


SPT N-Value

Moisture Content (%)

# Notes:

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193902.768 E/LONG: 1276326.832 Total Depth (ft): 30 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 7.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.15.21 Mudline Elevation (ft): 0.5 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)

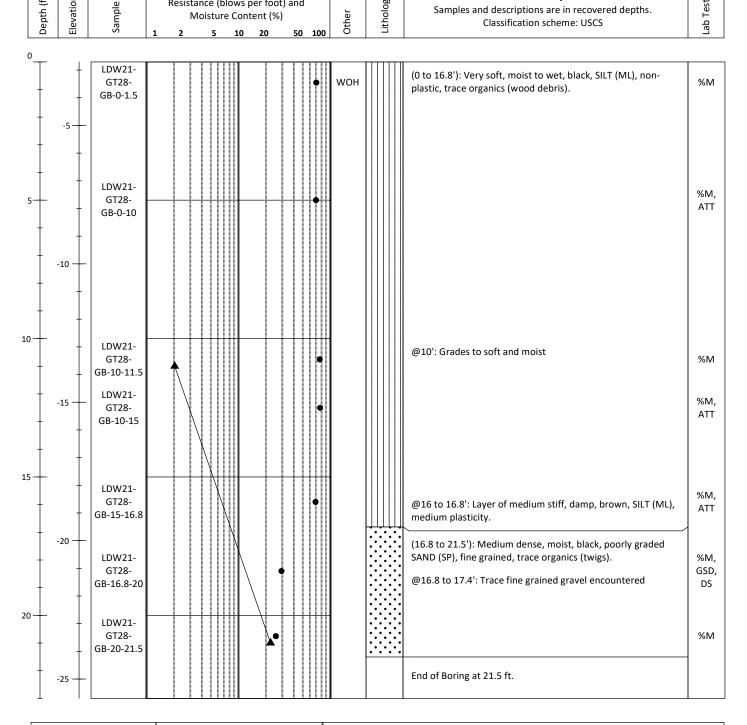




- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

## [DRAFT] Soil Boring Log Sheet 1 of 1 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193703.693 E/LONG: 1275982.714 Total Depth (ft): 21.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.07.21 Mudline Elevation (ft): -2.7 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.



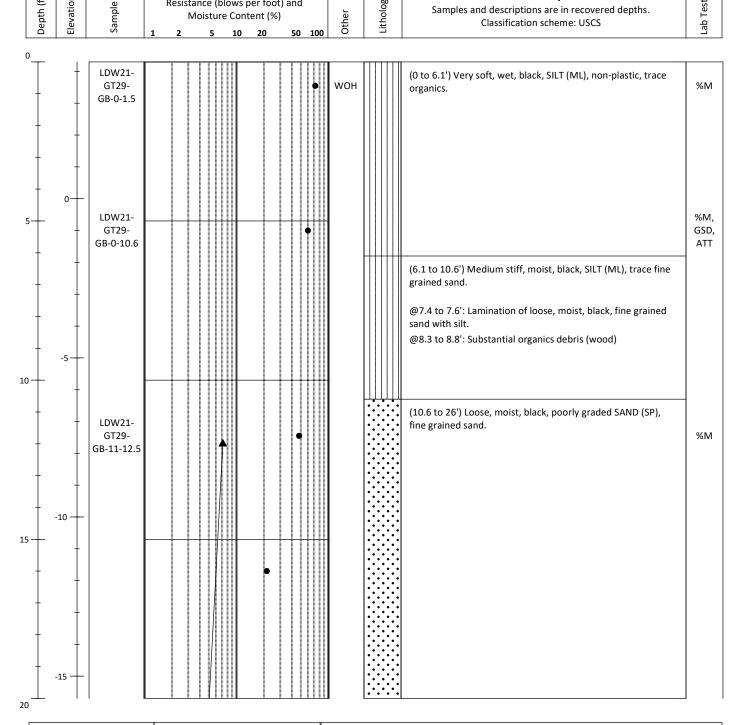


SPT N-Value

Moisture Content (%)

Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193401.625 E/LONG: 1276568.528 Total Depth (ft): 32.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 5.0 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.14.21 Mudline Elevation (ft): 4.3 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.



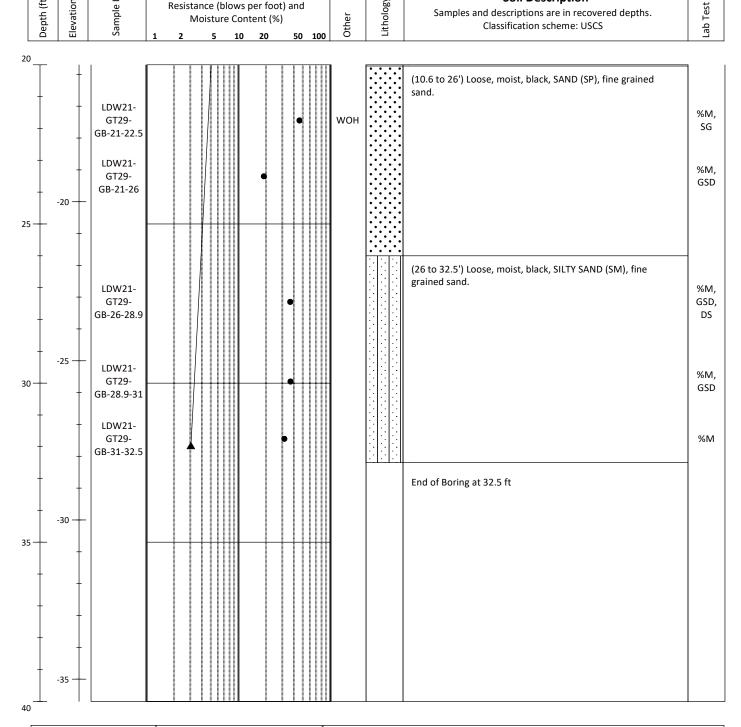


SPT N-Value

Moisture Content (%)

Moisture Content (%)

## [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193401.625 E/LONG: 1276568.528 Total Depth (ft): 32.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 5.0 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.14.21 Mudline Elevation (ft): 4.3 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and





- SPT N-Value
- Moisture Content (%)

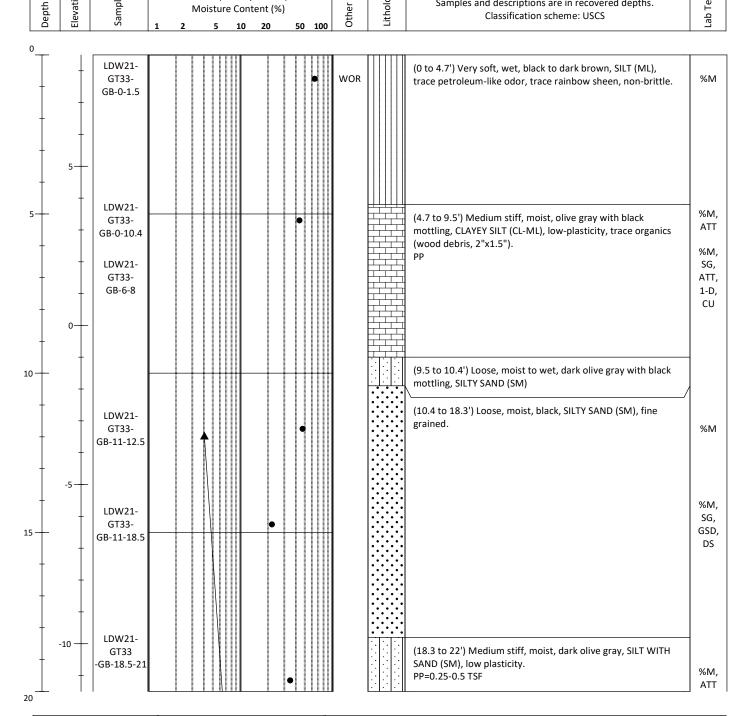
Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

Test

Samples and descriptions are in recovered depths.

#### [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT33-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193093.668 E/LONG: 1276612.259 Total Depth (ft): 32.5 Client: Lower Duwamish Waterway Group Horiz. Datum: Washington State Plane Coordinate North Observed Depth to Mudline (ft): 0.1 North American Datum of 1983, U.S. Feet Collection Date: 07.15.21 Mudline Elevation (ft): 8.5 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)



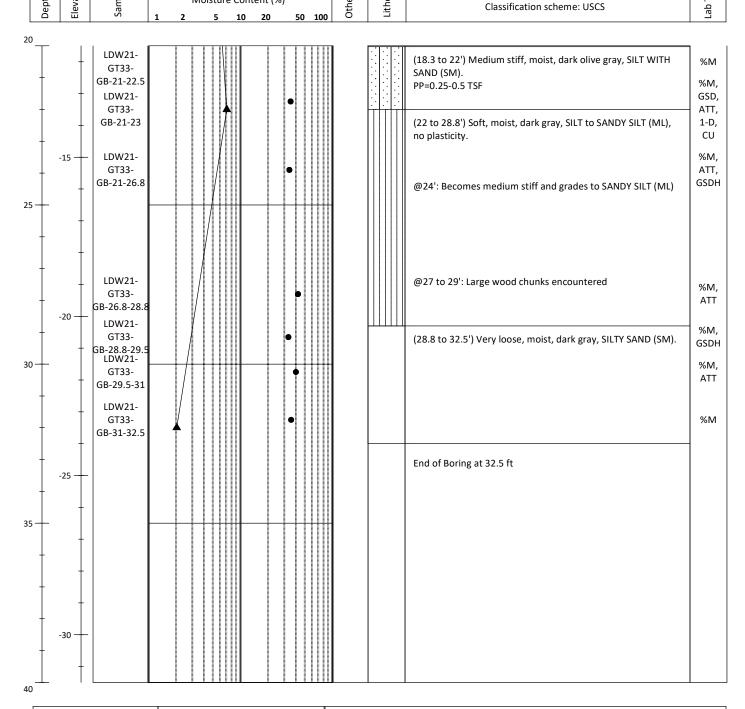


SPT N-Value

Moisture Content (%)

# Notes:

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 193093.668 E/LONG: 1276612.259 Total Depth (ft): 32.5 Client: Lower Duwamish Waterway Group Horiz. Datum: Washington State Plane Coordinate North Observed Depth to Mudline (ft): 0.1 North American Datum of 1983, U.S. Feet Collection Date: 07.15.21 Mudline Elevation (ft): 8.5 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)



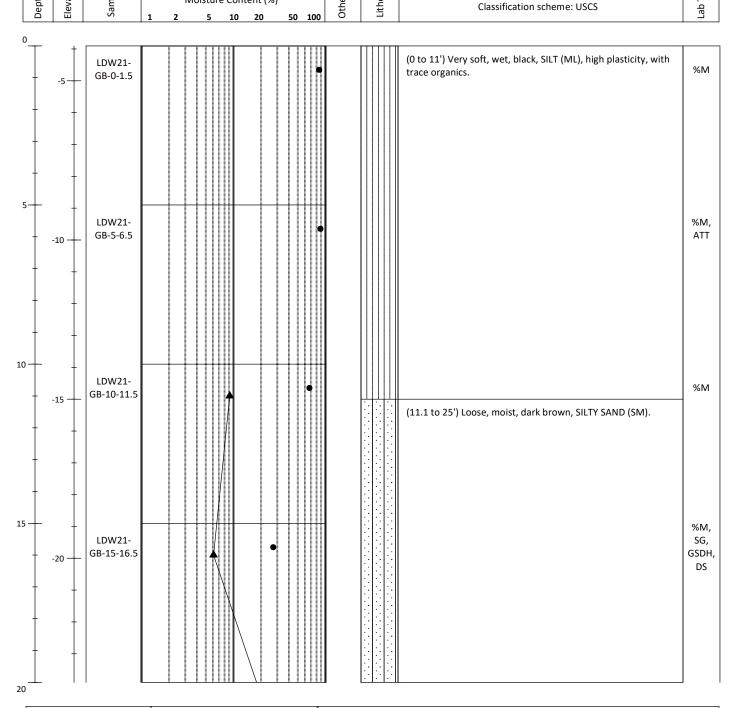


SPT N-Value

Moisture Content (%)

# Notes:

### [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 192818.4 E/LONG: 1277387 Total Depth (ft): 31.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 11.3 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.20.21 Mudline Elevation (ft): -3.9 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)

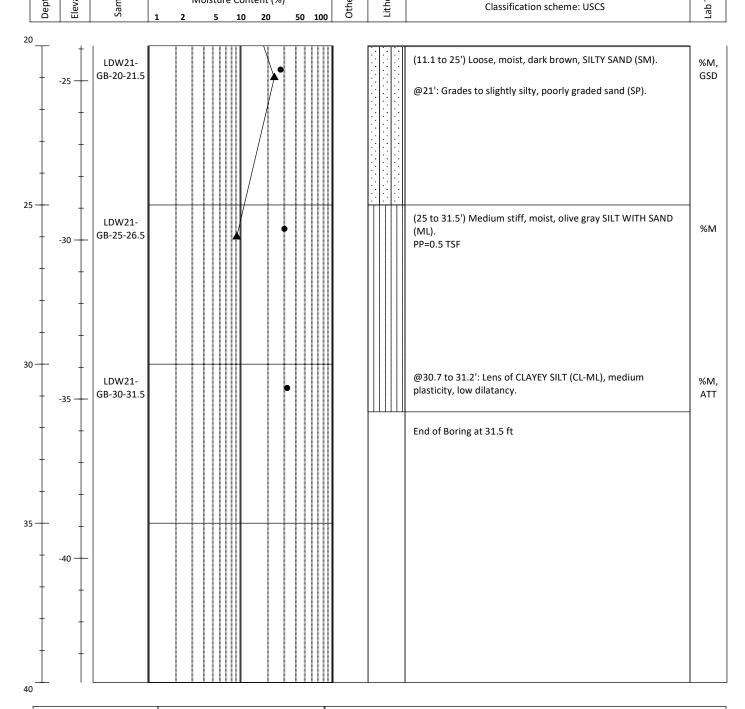




- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 192818.4 E/LONG: 1277387 Total Depth (ft): 31.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 11.3 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.20.21 Mudline Elevation (ft): -3.9 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)

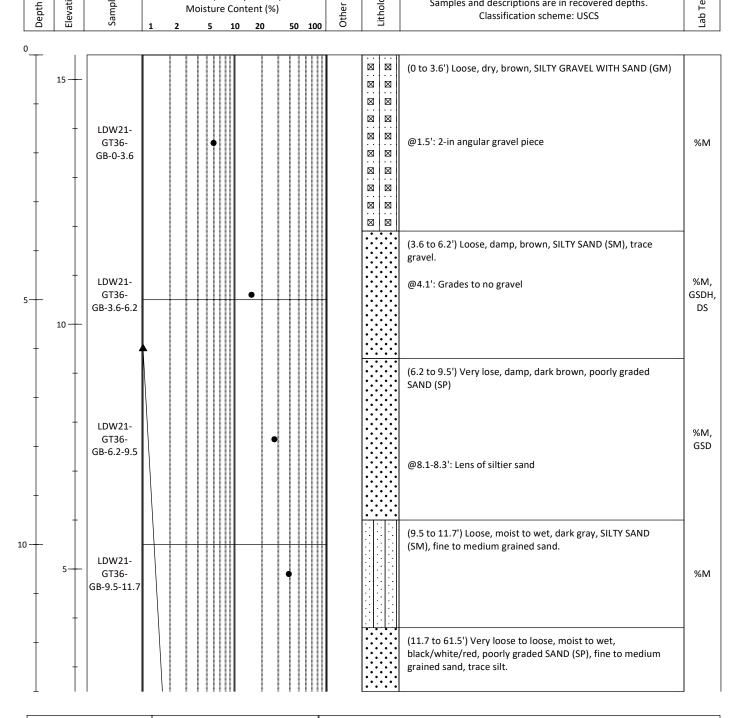




- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

### [DRAFT] Soil Boring Log Sheet 1 of 5 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1277403.821 Total Depth (ft): 61.5 N/LAT: 192741.238 Client: Lower Duwamish Waterway Group Horiz. Datum: Washington State Plane Coordinate North Observed Depth to Mudline (NE North American Datum of 1983, U.S. Feet Collection Date: 07.27.21 Surface Elevation (ft): Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Sam Giannakos Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Lithology Elevation Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

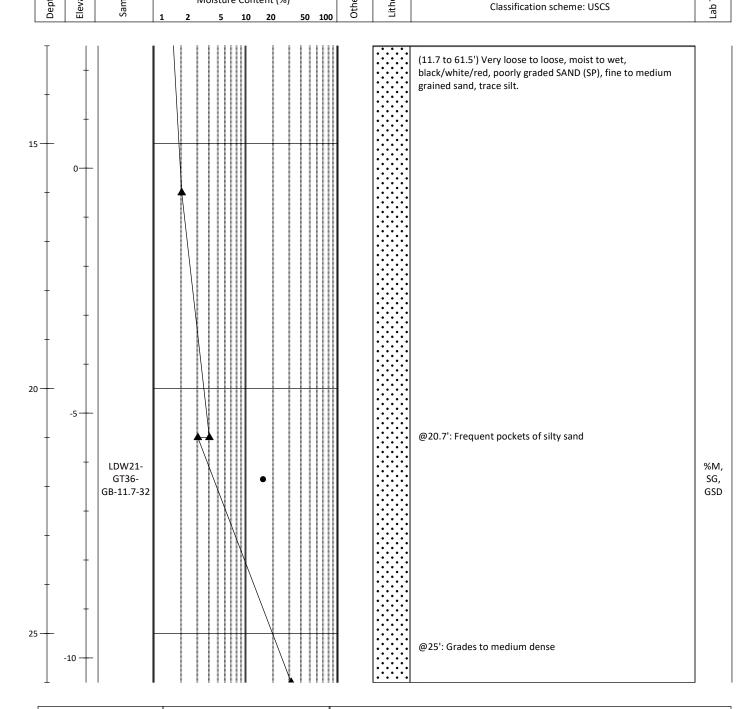




- SPT N-Value
- Moisture Content (%)

# lotes:

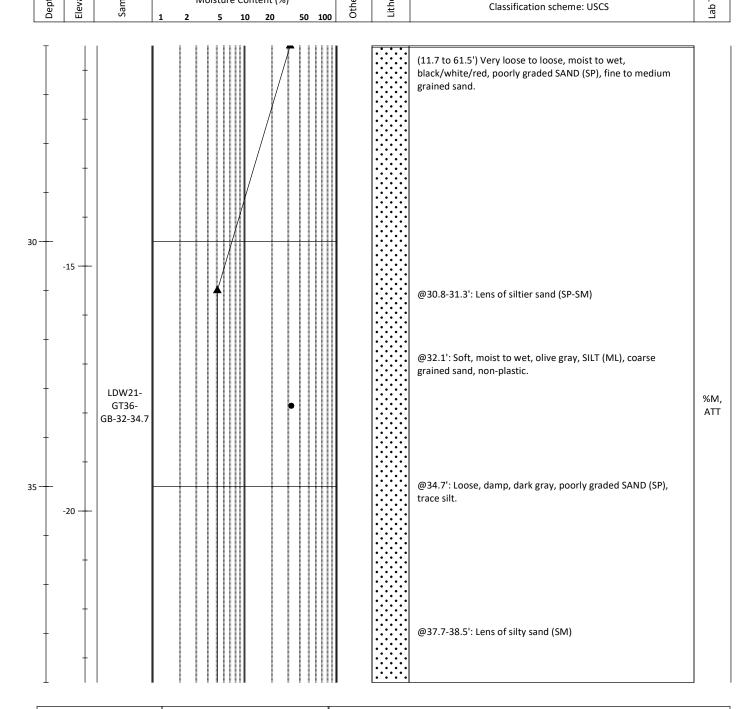
				[DRAFT	_	il Вс -GT36	Sheet 2 of 5			
Project #: 180067-02.03				Project: LDW Upper Reach Phase 2 Investigation				Method: Rotary Sonic	Method: Rotary Sonic	
Locat	tion: S	eattle, WA		N/LAT: 192741.2	238	E,	LONG: <b>1277403.821</b>	Total Depth (ft): 61.5		
Clien	t: Low	er Duwamish	Waterway Group	Horiz. Datum: Washington State Plane Coordinate North			Observed Depth to Mudline (NE			
Colle	Collection Date: 07.27.21			North American Datum of 1983, U.S. Feet			Surface Elevation (ft): 15.5			
Cont	ractor:	Holocene Di	rilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)			Hammer: 140-lb, 30-in drop, Auto			
Logg	ed By:	Sam Giannak	os	Sampler(s): Spl	it Spoon	& Shelb	/ Tube Sampler	Hammer Efficiency (%): 99		
epth (ft)	levation (ft)	ample ID	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and	)ther	ithology	Samples and descrip	Description  Itions are in recovered depths.  Ition scheme: USCS	ab Test	





- SPT N-Value
- Moisture Content (%)

				_	_	il Вс -GT36	oring Log	Sheet 3 of 5	
Project #: 180067-02.03				Project: LDW U	pper Rea	ch Phas	Method: Rotary Sonic	Method: Rotary Sonic	
Locat	tion: S	eattle, WA		N/LAT: 192741.2	N/LAT: 192741.238 E/LONG: 1277403.821 Total Depth (ft): 61.5			Total Depth (ft): 61.5	
Clien	t: Low	er Duwamish	Waterway Group	Horiz. Datum: Washington State Plane Coordinate North			Observed Depth to Mudline (NE		
Colle	Collection Date: 07.27.21			North American Datum of 1983, U.S. Feet			Surface Elevation (ft): 15.5		
Cont	ractor:	Holocene D	rilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)			Hammer: 140-lb, 30-in drop, Auto		
Logg	ed By:	Sam Giannak	os	Sampler(s): Spl	it Spoon	& Shelb	/ Tube Sampler	Hammer Efficiency (%): 99	
epth (ft)	levation (ft)	iample ID	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and	)ther	ithology	Samples and descrip	Description  Itions are in recovered depths.  Ition scheme: USCS	ab Test

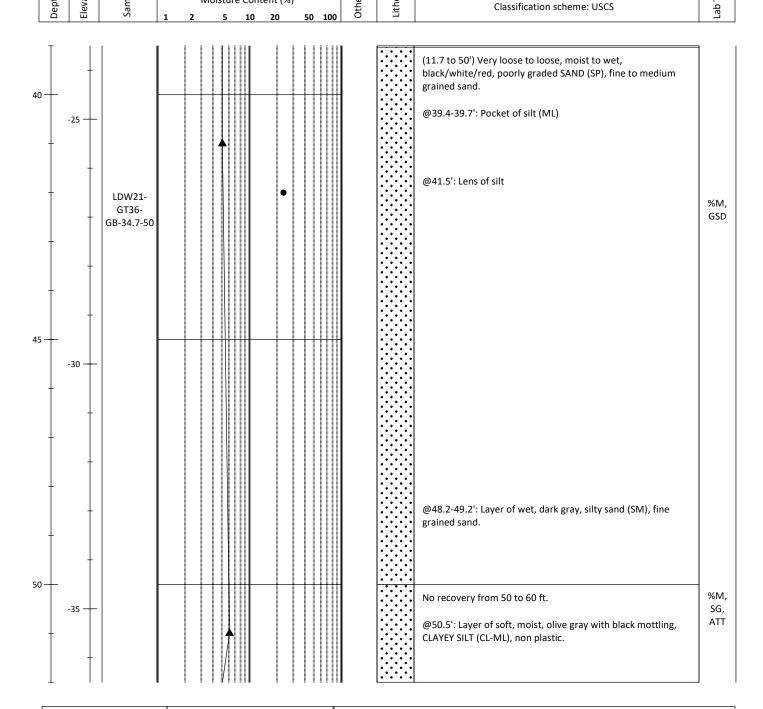




- SPT N-Value
- Moisture Content (%)

# lotes:

				[DRAFT]	_	il Вс -GT36	Sheet 4 of	Sheet 4 of 5	
Proje	ect #: 18	80067-02.03		Project: LDW Upper Reach Phase 2 Investigation				Method: Rotary Sonic	
Locat	tion: S	eattle, WA		N/LAT: 192741.2	38	E/	LONG: <b>1277403.821</b>	Total Depth (ft): 61.5	
Clien	t: Low	er Duwamish	Waterway Group	Horiz. Datum: W	/ashingte	on State	Observed Depth to Mudline (NE		
Colle	ction D	ate: <b>07.27.21</b>		N	orth Am	erican Da	Surface Elevation (ft): 15.5		
Cont	ractor:	Holocene D	rilling, Inc	Vert. Datum: Me	an Lowe	r Low W	ater (MLLW)	Hammer: 140-lb, 30-in drop, Auto	
Logg	ed By:	Sam Giannak	os	Sampler(s): Spl	it Spoon	& Shelb	Tube Sampler	Hammer Efficiency (%): 99	
oth (ft)	ation (ft)	nple ID	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and	ier	ygolou	Samples and descrip	I Description	Test



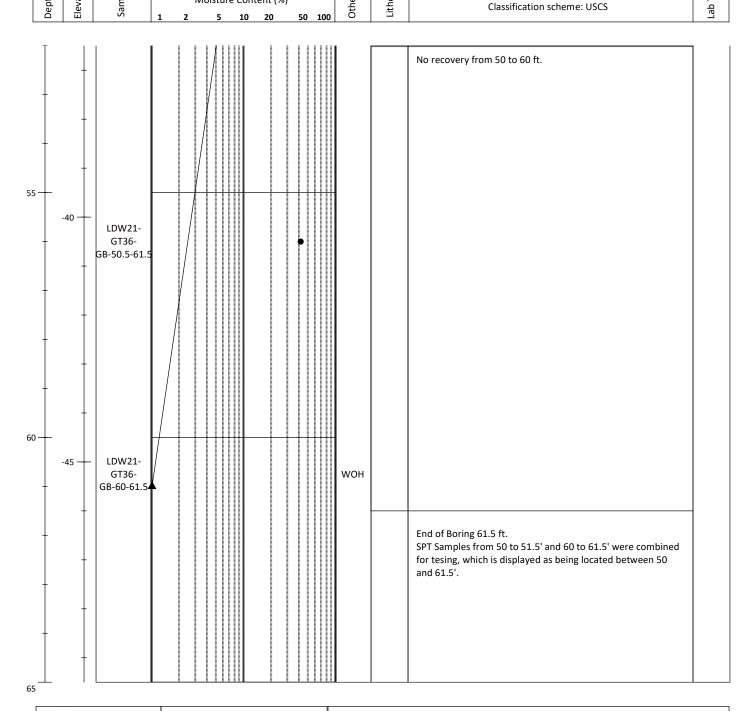


SPT N-Value

Moisture Content (%)

Notes:

				[DRAFT	_	il Вс -GT36	Sheet 5 of 5		
Project #: 180067-02.03				Project: LDW U	pper Rea	ch Phas	Method: Rotary Sonic	Method: Rotary Sonic	
Locat	tion: S	eattle, WA		N/LAT: 192741.2	N/LAT: 192741.238 E/LONG: 1277403.821 Total Depth (ft): 61.5			Total Depth (ft): 61.5	
Clien	t: Low	er Duwamish	Waterway Group	Horiz. Datum: Washington State Plane Coordinate North			Observed Depth to Mudline (NE		
Colle	Collection Date: 07.27.21			North American Datum of 1983, U.S. Feet			Surface Elevation (ft): 15.5		
Cont	ractor:	Holocene D	rilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)			Hammer: 140-lb, 30-in drop, Auto		
Logg	ed By:	Sam Giannak	os	Sampler(s): Spl	it Spoon	& Shelb	y Tube Sampler	Hammer Efficiency (%): 99	
epth (ft)	levation (ft)	ample ID	Uncorrected Standa Resistance (blows Moisture Cor	per foot) and	)ther	ithology	Samples and descrip	Description  Itions are in recovered depths.  Ition scheme: USCS	ab Test

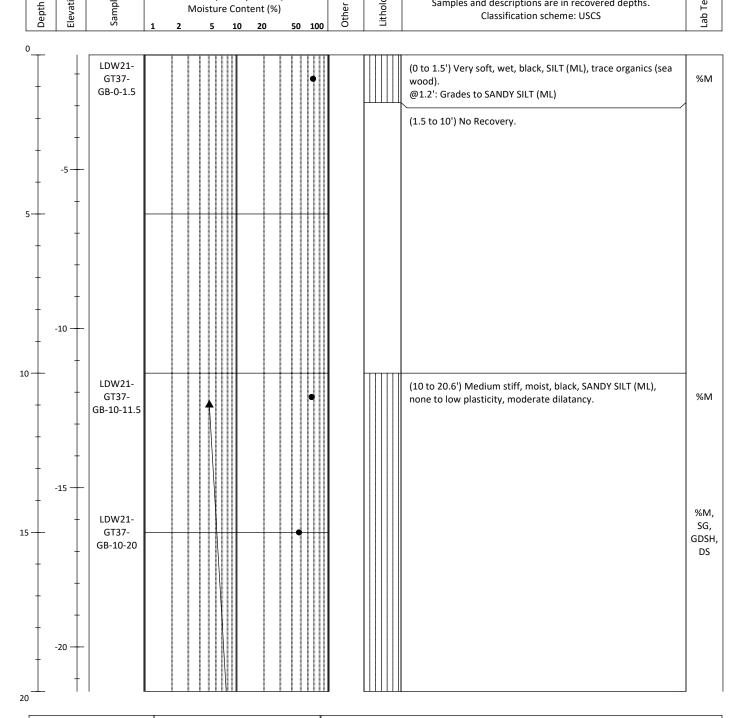




- SPT N-Value
- Moisture Content (%)

# lotes:

#### [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT37-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 192182.064 E/LONG: 1276436.379 Total Depth (ft): 31.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 6.0 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.14.21 Mudline Elevation (ft): -1.4 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)

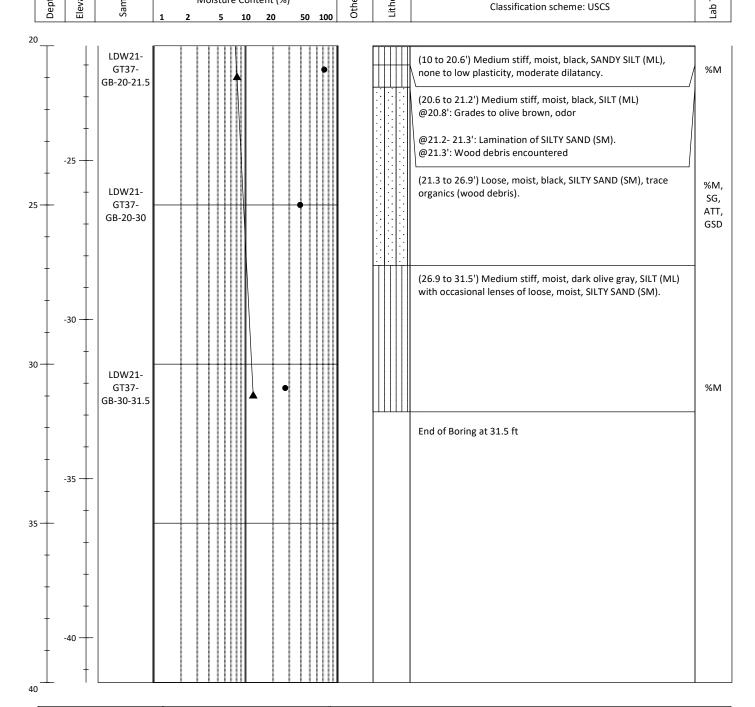




- SPT N-Value
- Moisture Content (%)

# Notes:

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1276436.379 Total Depth (ft): 31.5 N/LAT: 192182.064 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 6.0 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.14.21 Mudline Elevation (ft): -1.4 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Resistance (blows per foot) and Lithology Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

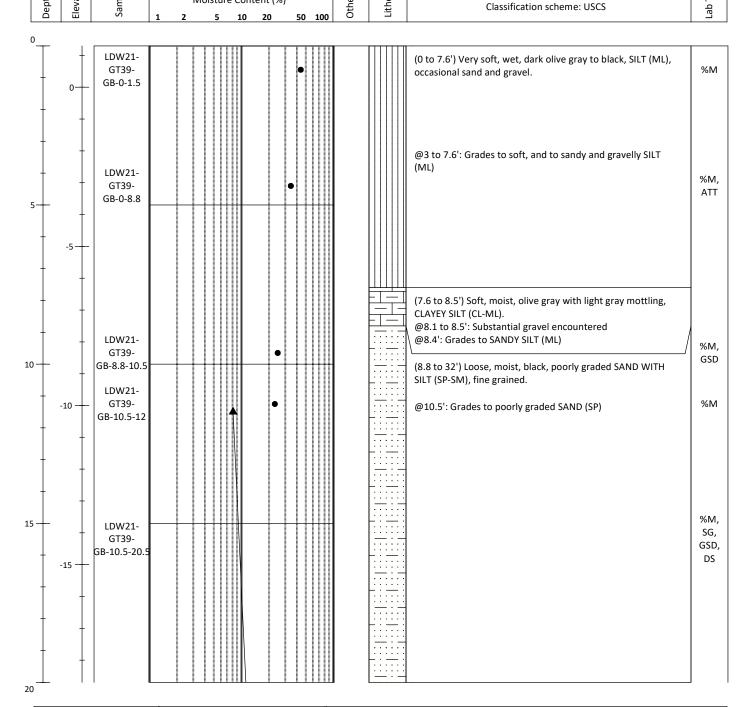




- SPT N-Value
- Moisture Content (%)

# lotes:

#### [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT39-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190600.557 E/LONG: 1277362.3 Total Depth (ft): 32 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 5.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.16.21 Mudline Elevation (ft): 1.3 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

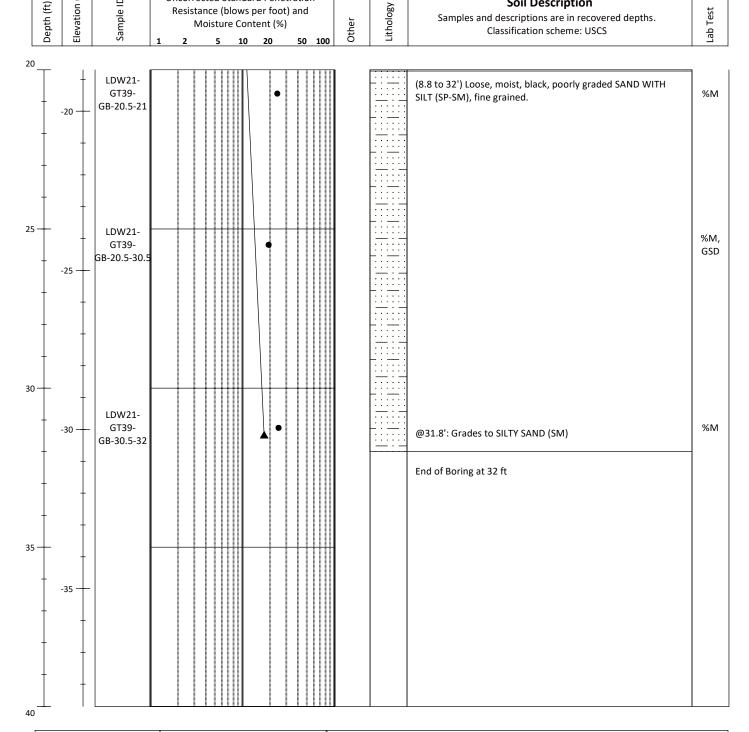




- SPT N-Value
- Moisture Content (%)

# lotes:

## [DRAFT] Soil Boring Log Sheet 2 of 2 LDW21-GT39-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190600.557 E/LONG: 1277362.3 Total Depth (ft): 32 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 5.5 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 07.16.21 Mudline Elevation (ft): 1.3 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Casey Janisch Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration**





 $\Box$ 

Resistance (blows per foot) and

Moisture Content (%)

SPT N-Value

Moisture Content (%)

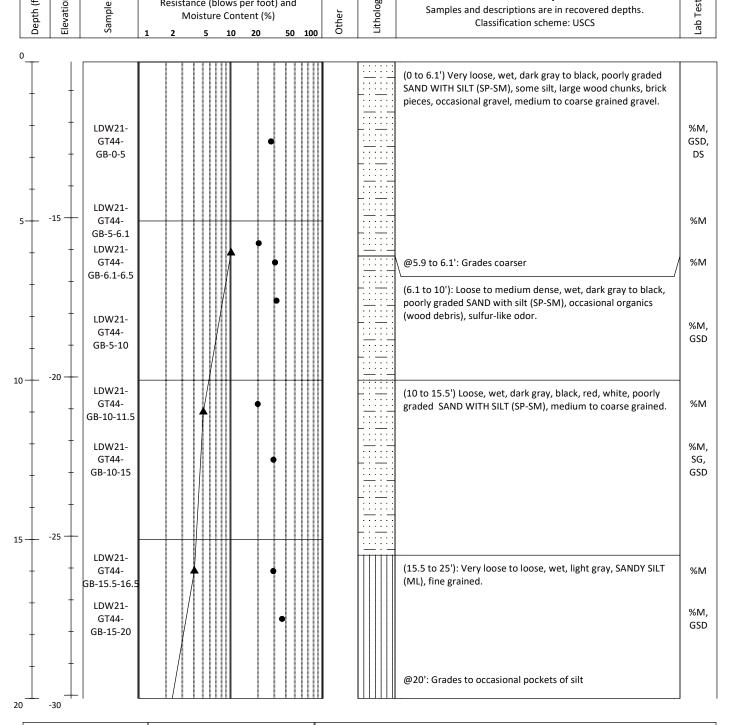
%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

**Soil Description** 

Samples and descriptions are in recovered depths.

Test

## [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT44-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1278233.2 Total Depth (ft): 31.5 N/LAT: 190379.661 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.04.21 Mudline Elevation (ft): -10.1 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test





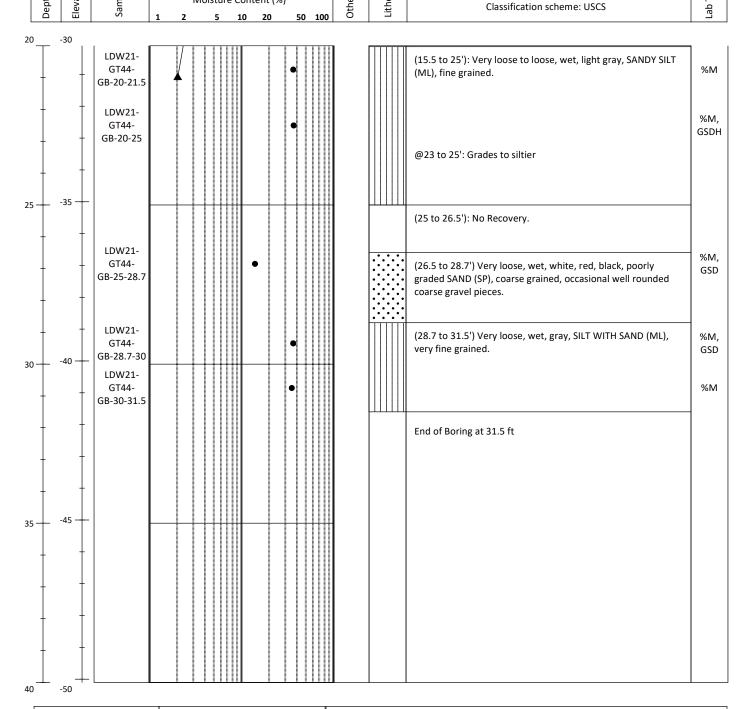
- SPT N-Value
- Moisture Content (%)

Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp. Mudline elevations determined from leadline measurements and Site tide gage levels

Samples and descriptions are in recovered depths.

#### [DRAFT] Soil Boring Log Sheet 2 of 2 LDW21-GT44-GB Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190379.661 E/LONG: 1278233.2 Total Depth (ft): 31.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.04.21 Mudline Elevation (ft): -10.1 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)

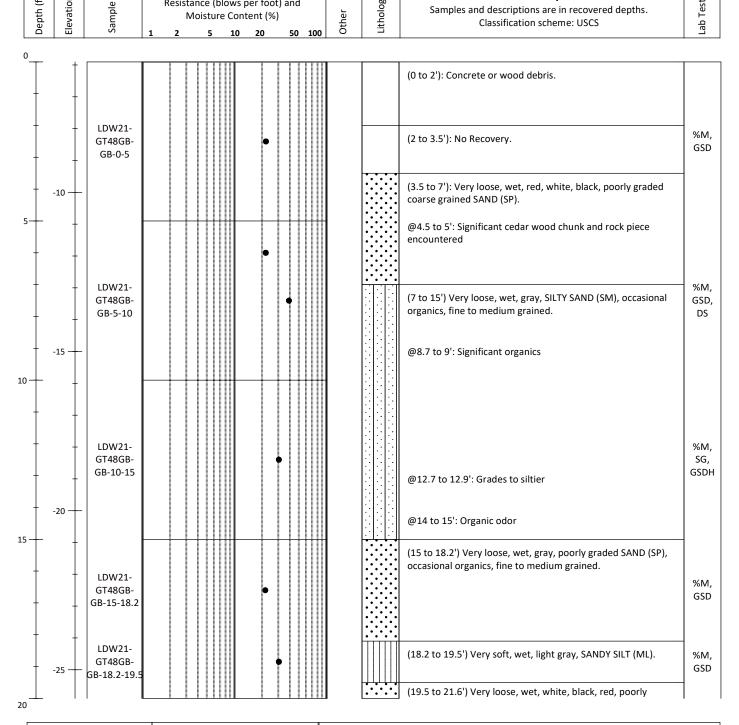




- SPT N-Value
- Moisture Content (%)

# Notes:

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1278379.433 Total Depth (ft): 35 N/LAT: 190317.6 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): -5.9 Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.

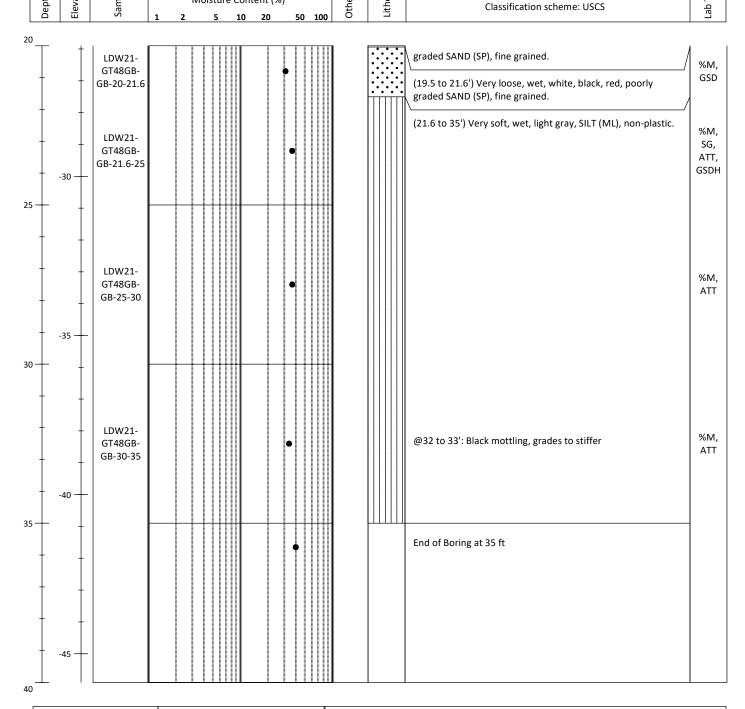




- SPT N-Value
- Moisture Content (%)

Moisture Content (%)

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190317.6 E/LONG: 1278379.433 Total Depth (ft): 35 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): -5.9 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%)



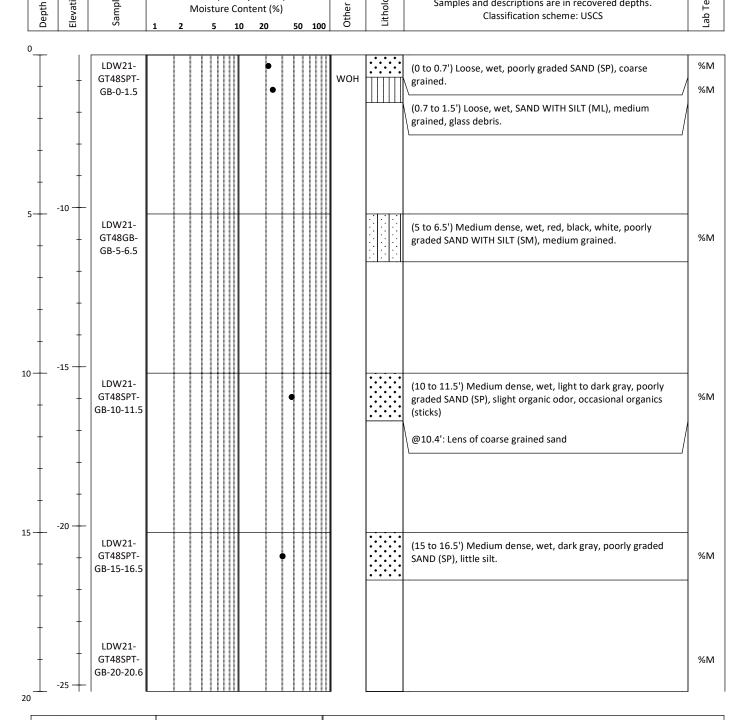


SPT N-Value

• Moisture Content (%)

# Notes:

#### [DRAFT] Soil Boring Log Sheet 1 of 2 LDW21-GT48-SPT Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190313.244 E/LONG: 1278382.172 Total Depth (ft): 36.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): -5.2 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Resistance (blows per foot) and Lithology Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)



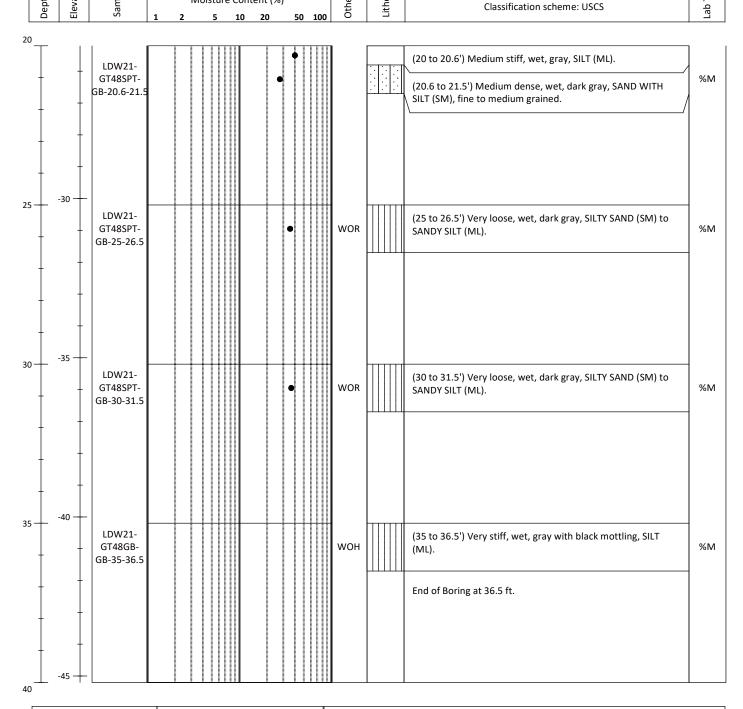


SPT N-Value

Moisture Content (%)

# Notes:

#### [DRAFT] Soil Boring Log Sheet 2 of 2 LDW21-GT48-SPT Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190313.244 E/LONG: 1278382.172 Total Depth (ft): 36.5 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): -5.2 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Sample I Test Samples and descriptions are in recovered depths. Moisture Content (%) Classification scheme: USCS



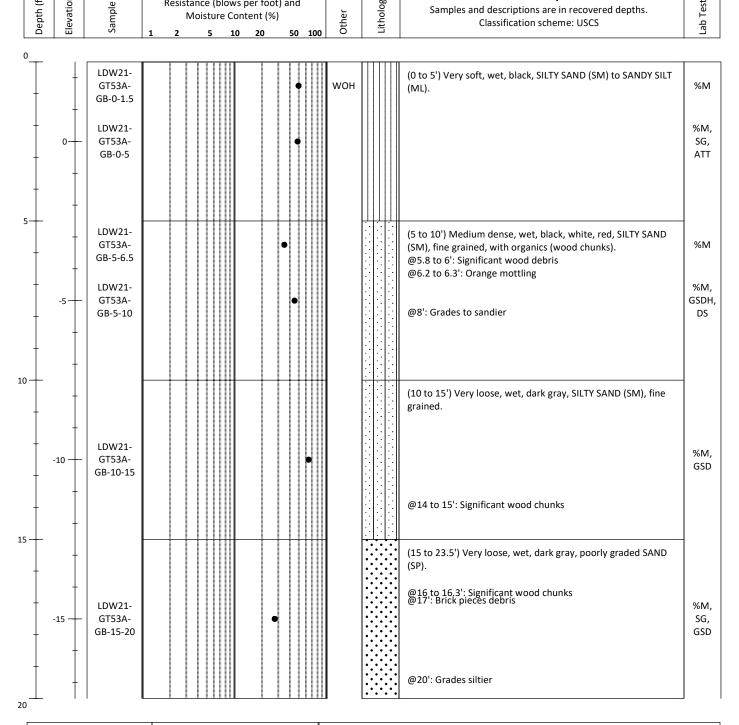


SPT N-Value

Moisture Content (%)

# Notes:

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA E/LONG: 1278593.074 Total Depth (ft): 30 N/LAT: 190178.63 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft.) Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Surface Elevation (ft): 2.5 Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** Δ **Soil Description** $\equiv$ Lithology Elevation Resistance (blows per foot) and Test Samples and descriptions are in recovered depths.





- SPT N-Value
- Moisture Content (%)

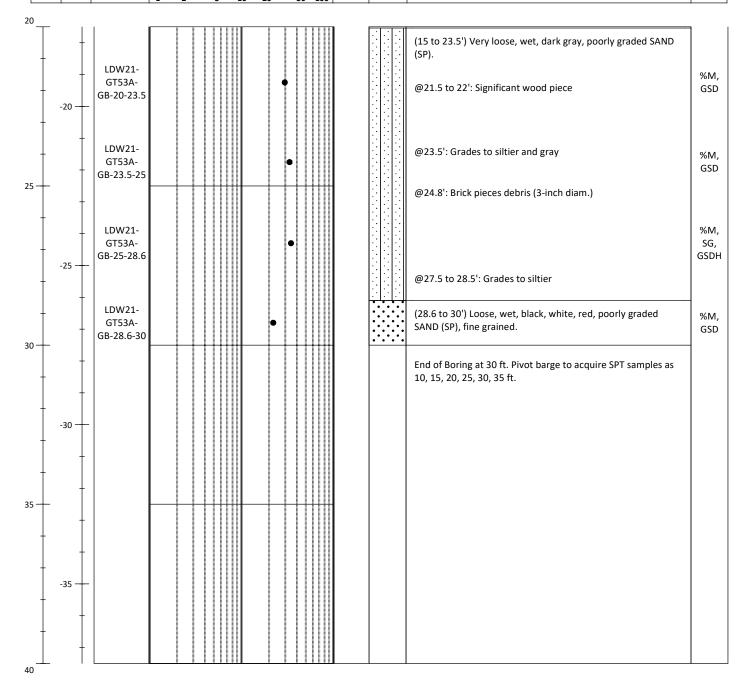
Moisture Content (%)

# [DRAFT] Soil Boring Log

Sheet 2 of 2

Project #: 180067-02.03	Project: LDW Upper Reach Phase 2 Investigation	Method: Rotary Sonic
Location: Seattle, WA	N/LAT: <b>190178.63</b> E/LONG: <b>1278593.074</b>	Total Depth (ft): 30
Client: Lower Duwamish Waterway Group	Horiz. Datum: Washington State Plane Coordinate North	Observed Depth to Mudline (能)
Collection Date: 08.05.21	North American Datum of 1983, U.S. Feet	Surface Elevation (ft): 2.5
Contractor: Holocene Drilling, Inc	Vert. Datum: Mean Lower Low Water (MLLW)	Hammer: 140-lb, 30-in drop, Auto
Logged By: Garrett Timm	Sampler(s): Split Spoon & Shelby Tube Sampler	Hammer Efficiency (%): 99

oth (ft)	ation (ft)	nple ID	Uncorrected Standard Penetration Resistance (blows per foot) and Moisture Content (%)	er	ology	Soil Description Samples and descriptions are in recovered depths.	Test
Depth	Elevai	Samp	Moisture Content (%)	Other	Litho	Classification scheme: USCS	Lab T



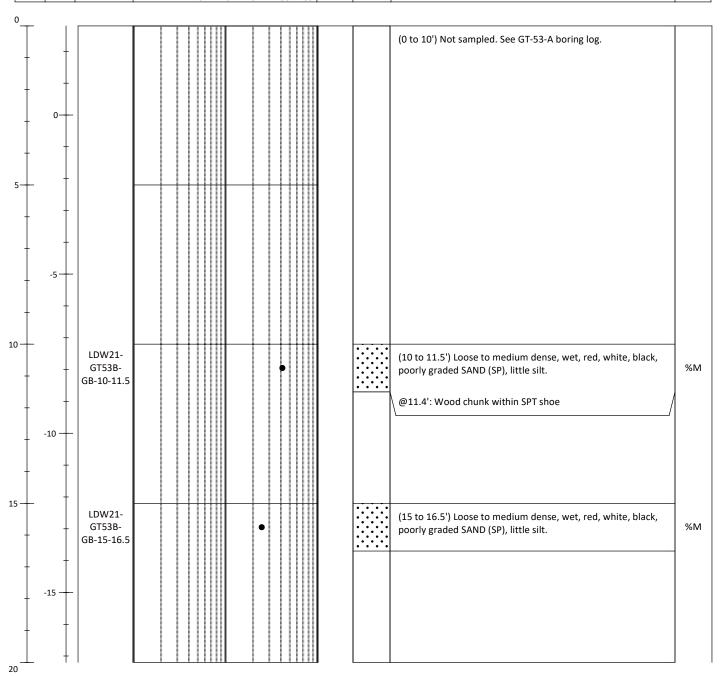


- SPT N-Value
- Moisture Content (%)

# lotes:

## [DRAFT] Soil Boring Log Sheet 1 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190175.401 E/LONG: 1278593.916 Total Depth (ft): 32 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 9.2 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): 2.8 Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Vert. Datum: Mean Lower Low Water (MLLW) Logged By: Garrett Timm Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99

oth (ft)	ation (ft)	nple ID	Uncorrected Standard Penetration Resistance (blows per foot) and Moisture Content (%)	ner nology	Soil Description Samples and descriptions are in recovered depths.	Test
Deptl	Eleva	Samp	Moisture Content (%)  1 2 5 10 20 50 100	Othe	Classification scheme: USCS	Lab T



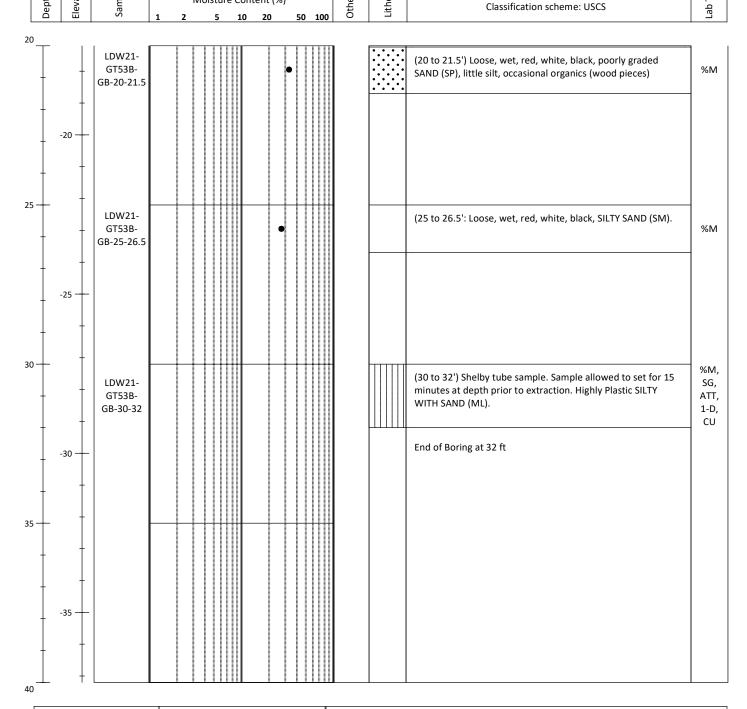


- SPT N-Value
- Moisture Content (%)

# Notes:

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution,
GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp
Mudline elevations determined from leadline measurements and Site tide gage levels
Depth to mudline at this location determined using reading at LDW21-GT53-A & tide stage difference

### [DRAFT] Soil Boring Log Sheet 2 of 2 Project #: 180067-02.03 Project: LDW Upper Reach Phase 2 Investigation Method: Rotary Sonic Location: Seattle, WA N/LAT: 190175.401 E/LONG: 1278593.916 Total Depth (ft): 32 Client: Lower Duwamish Waterway Group Observed Depth to Mudline (ft): 9.2 Horiz. Datum: Washington State Plane Coordinate North North American Datum of 1983, U.S. Feet Collection Date: 08.05.21 Mudline Elevation (ft): 2.8 Vert. Datum: Mean Lower Low Water (MLLW) Hammer: 140-lb, 30-in drop, Auto Contractor: Holocene Drilling, Inc Logged By: Garrett Timm Sampler(s): Split Spoon & Shelby Tube Sampler Hammer Efficiency (%): 99 $\equiv$ **Uncorrected Standard Penetration** $\Box$ **Soil Description** Depth (ft) Elevation Lithology Resistance (blows per foot) and Test Sample Samples and descriptions are in recovered depths. Moisture Content (%)





- SPT N-Value
- Moisture Content (%)

%M=Percent Moisture Content,SG=Specific Gravity,ATT=Atterberg Limits,GSD=Grainsize Distribution, GSDH=Grainsize Distribution+Hydrometer,1-D: One-densional Consolidation,CU=Unconsolidated Comp Mudline elevations determined from leadline measurements and Site tide gage levels Depth to mudline at this location determined using reading at LDW21-GT53-A & tide stage difference

# PRESENTATION OF SITE INVESTIGATION RESULTS

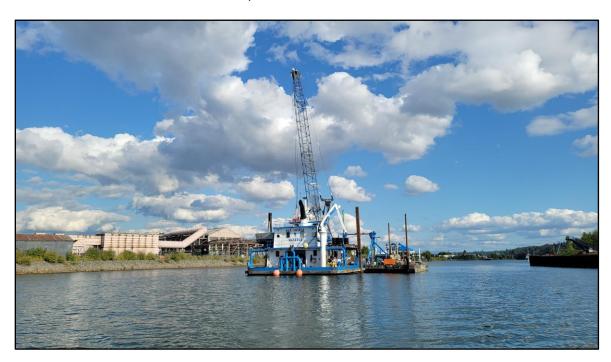
# LDW Phase 3

Prepared for:

Anchor QEA

ConeTec Job No: 21-59-22445

Project Start Date: 06-JUL-2021 Project End Date: 29-JUL-2021 Report Date: 9-AUG-2021



# Prepared by:

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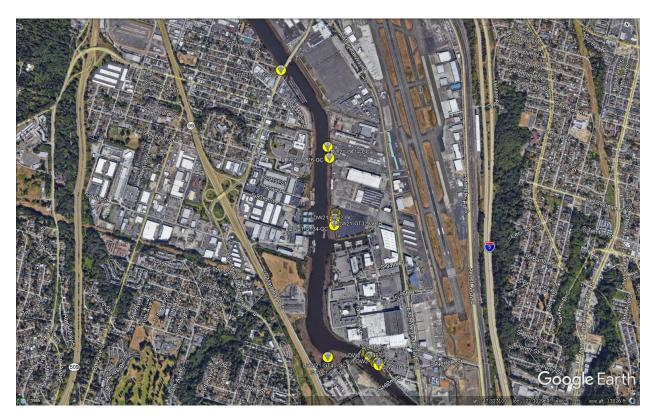
### Introduction

The enclosed report presents the results of the site investigation program conducted by ConeTec Inc. for Anchor QEA along mile 3-5 of the Duwamish River located in Seattle WA. The program consisted of cone penetration tests, full flow penetration tests & electronic vane testing

## **Project Information**

Project				
Client	Anchor QEA			
Project	LDW Phase 3			
ConeTec project number	21-59-22445			

An aerial overview from Google Earth including the CPTu test locations is presented below.



Rig Description	Deployment System	Test Type
C05-023 Track Rig	Integrated Push System	CPT, BCPT, VST
A07-018 Amphibious Rig	Integrated Push System	СРТ
Barge Support	Auxiliary Push Boat	CPT, BCPT, VST



Coordinates					
Test Type	Collection Method	EPSG Number	Comments		
CPT, BCPT, VST	Client provided	4326	Coordinates converted from State Plane		

Cone Penetrometers Used for this Project							
Cone Description	Cone Number	Cross Sectional Area (cm²)	Sleeve Area (cm²)	Tip Capacity (bar)	Sleeve Capacity (bar)	Pore Pressure Capacity (bar)	
681:T375F10U35	681	15	225	375	10	35	
Cone 681 was used for all CPTu soundings.							

Cone Penetration Test (CPTu)					
Depth reference	Depths are referenced to the existing mudline at the time of each test.				
Tip and sleeve data offset	0.1 meter				
Tip and sieeve data onset	This has been accounted for in the CPT data files.				
Additional plats	Advanced plots with Ic, Su, phi and N1(60)				
Additional plots	<ul> <li>Soil Behaviour Type (SBT) scatter plots</li> </ul>				
Additional comments	A negative water table has been applied to all soundings completed from				
Additional comments	barge deck. All CPT data files begin at mudline (mudline = 0.0ft)				

Calculated Geotechnical Parameter Tables					
Additional information	The Normalized Soil Behaviour Type Chart based on Qtn (SBT Qtn) (Robertson, 2009) was used to classify the soil for this project. A detailed set of calculated CPTu parameters have been generated and are provided in Excel format files in the release folder. The CPTu parameter calculations are based on values of corrected tip resistance (qt) sleeve friction (fs) and pore pressure (u2).  Effective stresses are calculated based on unit weights that have been assigned to the individual soil behaviour type zones and the assumed equilibrium pore pressure profile.				

Full-Flow Cone Penetration Test (BCPTu)					
Donth reference	All soundings were started slightly above the mudline in the water column.				
Depth reference	Mudline is clearly indicated on all plots and clearly visible within the data set.				
Unit weight profiles	A unit weight of 62.43pcf was applied to data collected within the water				
	column above mudline				
	A unit weight of 111.37pcf was applied to data collected below mudline				
	The unit weight is clearly indicated in the data set.				



Electric Field Vane Shear Test (VST)					
Depth reference	ence Depths are referenced to depth below mudline at the time of each test				
Load cell capacity	100 N·m				
Load cell location	Uphole				
Additional comments	All vane tests were completed from the floating barge platform. The vane test results were affected by barge movement from local waves, local vessel traffic and river flow. Additionally, the vane results were susceptible to elevation charge from either rising or falling tide. Over the course of a vane test the barge would gain/lose approximately 2"-4" of elevation due to tidal effects.				

### Limitations

This report has been prepared for the exclusive use of Anchor QEA (Client) for the project titled "LDW Phase 3". The report's contents may not be relied upon by any other party without the express written permission of ConeTec Inc. (ConeTec). ConeTec has provided site investigation services, prepared the factual data reporting and provided geotechnical parameter calculations consistent with current best practices. No other warranty, expressed or implied, is made.

The information presented in the report document and the accompanying data set pertain to the specific project, site conditions and objectives described to ConeTec by the Client. In order to properly understand the factual data, assumptions and calculations, reference must be made to the documents provided and their accompanying data sets, in their entirety.



Cone penetration tests (CPTu) are conducted using an integrated electronic piezocone penetrometer and data acquisition system manufactured by Adara Systems Ltd., a subsidiary of ConeTec.

ConeTec's piezocone penetrometers are compression type designs in which the tip and friction sleeve load cells are independent and have separate load capacities. The piezocones use strain gauged load cells for tip and sleeve friction and a strain gauged diaphragm type transducer for recording pore pressure. The piezocones also have a platinum resistive temperature device (RTD) for monitoring the temperature of the sensors, an accelerometer type dual axis inclinometer and two geophone sensors for recording seismic signals. All signals are amplified and measured with minimum sixteen-bit resolution down hole within the cone body, and the signals are sent to the surface using a high bandwidth, error corrected digital interface through a shielded cable.

ConeTec penetrometers are manufactured with various tip, friction and pore pressure capacities in both 10 cm² and 15 cm² tip base area configurations in order to maximize signal resolution for various soil conditions. The specific piezocone used for each test is described in the CPT summary table presented in the first appendix. The 15 cm² penetrometers do not require friction reducers as they have a diameter larger than the deployment rods. The 10 cm² piezocones use a friction reducer consisting of a rod adapter extension behind the main cone body with an enlarged cross sectional area (typically 44 millimeters diameter over a length of 32 millimeters with tapered leading and trailing edges) located at a distance of 585 millimeters above the cone tip.

The penetrometers are designed with equal end area friction sleeves, a net end area ratio of 0.8 and cone tips with a 60 degree apex angle.

All ConeTec piezocones can record pore pressure at various locations. Unless otherwise noted, the pore pressure filter is located directly behind the cone tip in the " $u_2$ " position (ASTM Type 2). The filter is six millimeters thick, made of porous plastic (polyethylene) having an average pore size of 125 microns (90-160 microns). The function of the filter is to allow rapid movements of extremely small volumes of water needed to activate the pressure transducer while preventing soil ingress or blockage.

The piezocone penetrometers are manufactured with dimensions, tolerances and sensor characteristics that are in general accordance with the current ASTM D5778 standard. ConeTec's calibration criteria also meets or exceeds those of the current ASTM D5778 standard. An illustration of the piezocone penetrometer is presented in Figure CPTu.



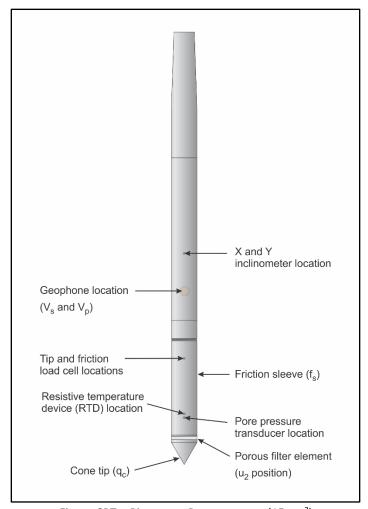


Figure CPTu. Piezocone Penetrometer (15 cm<sup>2</sup>)

The ConeTec data acquisition systems consist of a Windows based computer and a signal interface box and power supply. The signal interface combines depth increment signals, seismic trigger signals and the downhole digital data. This combined data is then sent to the Windows based computer for collection and presentation. The data is recorded at fixed depth increments using a depth wheel attached to the push cylinders or by using a spring loaded rubber depth wheel that is held against the cone rods. The typical recording interval is 2.5 centimeters; custom recording intervals are possible.

The system displays the CPTu data in real time and records the following parameters to a storage media during penetration:

- Depth
- Uncorrected tip resistance (q<sub>c</sub>)
- Sleeve friction (f<sub>s</sub>)
- Dynamic pore pressure (u)
- Additional sensors such as resistivity, passive gamma, ultra violet induced fluorescence, if applicable



All testing is performed in accordance to ConeTec's CPTu operating procedures which are in general accordance with the current ASTM D5778 standard.

Prior to the start of a CPTu sounding a suitable cone is selected, the cone and data acquisition system are powered on, the pore pressure system is saturated with silicone oil and the baseline readings are recorded with the cone hanging freely in a vertical position.

The CPTu is conducted at a steady rate of two centimeters per second, within acceptable tolerances. Typically one meter length rods with an outer diameter of 1.5 inches (38.1 millimeters) are added to advance the cone to the sounding termination depth. After cone retraction final baselines are recorded.

Additional information pertaining to ConeTec's cone penetration testing procedures:

- Each filter is saturated in silicone oil under vacuum pressure prior to use
- Baseline readings are compared to previous readings
- Soundings are terminated at the client's target depth or at a depth where an obstruction is encountered, excessive rod flex occurs, excessive inclination occurs, equipment damage is likely to take place, or a dangerous working environment arises
- Differences between initial and final baselines are calculated to ensure zero load offsets have not occurred and to ensure compliance with ASTM standards

The interpretation of piezocone data for this report is based on the corrected tip resistance ( $q_t$ ), sleeve friction ( $f_s$ ) and pore water pressure (u). The interpretation of soil type is based on the correlations developed by Robertson et al. (1986) and Robertson (1990, 2009). It should be noted that it is not always possible to accurately identify a soil behavior type based on these parameters. In these situations, experience, judgment and an assessment of other parameters may be used to infer soil behavior type.

The recorded tip resistance  $(q_c)$  is the total force acting on the piezocone tip divided by its base area. The tip resistance is corrected for pore pressure effects and termed corrected tip resistance  $(q_t)$  according to the following expression presented in Robertson et al. (1986):

$$q_t = q_c + (1-a) \cdot u_2$$

where: qt is the corrected tip resistance

q<sub>c</sub> is the recorded tip resistance

 $u_2$  is the recorded dynamic pore pressure behind the tip ( $u_2$  position)

a is the Net Area Ratio for the piezocone (0.8 for ConeTec probes)

The sleeve friction ( $f_s$ ) is the frictional force on the sleeve divided by its surface area. As all ConeTec piezocones have equal end area friction sleeves, pore pressure corrections to the sleeve data are not required.

The dynamic pore pressure (u) is a measure of the pore pressures generated during cone penetration. To record equilibrium pore pressure, the penetration must be stopped to allow the dynamic pore pressures to stabilize. The rate at which this occurs is predominantly a function of the permeability of the soil and the diameter of the cone.



The friction ratio  $(R_f)$  is a calculated parameter. It is defined as the ratio of sleeve friction to the tip resistance expressed as a percentage. Generally, saturated cohesive soils have low tip resistance, high friction ratios and generate large excess pore water pressures. Cohesionless soils have higher tip resistances, lower friction ratios and do not generate significant excess pore water pressure.

A summary of the CPTu soundings along with test details and individual plots are provided in the appendices. A set of files with calculated geotechnical parameters were generated for each sounding based on published correlations and are provided in Excel format in the data release folder. Information regarding the methods used is also included in the data release folder.

For additional information on CPTu interpretations and calculated geotechnical parameters, refer to Robertson et al. (1986), Lunne et al. (1997), Robertson (2009), Mayne (2013, 2014) and Mayne and Peuchen (2012).



The cone penetration test is halted at specific depths to carry out pore pressure dissipation (PPD) tests, shown in Figure PPD-1. For each dissipation test the cone and rods are decoupled from the rig and the data acquisition system measures and records the variation of the pore pressure (u) with time (t).

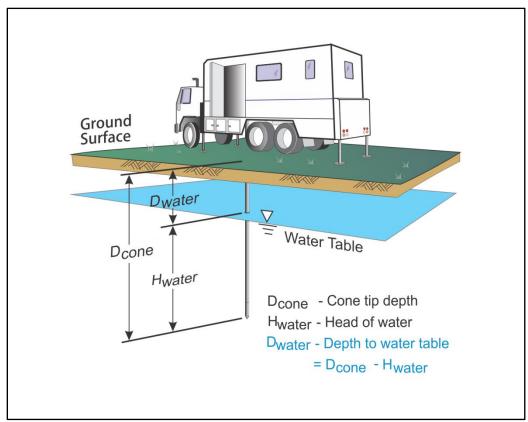


Figure PPD-1. Pore pressure dissipation test setup

Pore pressure dissipation data can be interpreted to provide estimates of ground water conditions, permeability, consolidation characteristics and soil behavior.

The typical shapes of dissipation curves shown in Figure PPD-2 are very useful in assessing soil type, drainage, in situ pore pressure and soil properties. A flat curve that stabilizes quickly is typical of a freely draining sand. Undrained soils such as clays will typically show positive excess pore pressure and have long dissipation times. Dilative soils will often exhibit dynamic pore pressures below equilibrium that then rise over time. Overconsolidated fine-grained soils will often exhibit an initial dilatory response where there is an initial rise in pore pressure before reaching a peak and dissipating.

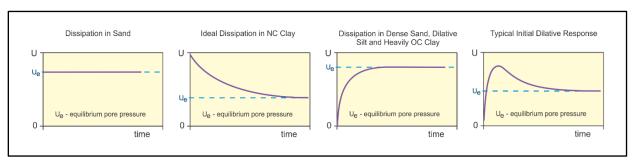


Figure PPD-2. Pore pressure dissipation curve examples



In order to interpret the equilibrium pore pressure ( $u_{eq}$ ) and the apparent phreatic surface, the pore pressure should be monitored until such time as there is no variation in pore pressure with time as shown for each curve in Figure PPD-2.

In fine grained deposits the point at which 100% of the excess pore pressure has dissipated is known as  $t_{100}$ . In some cases this can take an excessive amount of time and it may be impractical to take the dissipation to  $t_{100}$ . A theoretical analysis of pore pressure dissipations by Teh and Houlsby (1991) showed that a single curve relating degree of dissipation versus theoretical time factor (T\*) may be used to calculate the coefficient of consolidation ( $c_h$ ) at various degrees of dissipation resulting in the expression for  $c_h$  shown below.

$$c_h = \frac{T^* \cdot a^2 \cdot \sqrt{I_r}}{t}$$

Where:

T\* is the dimensionless time factor (Table Time Factor)

a is the radius of the cone

I<sub>r</sub> is the rigidity index

t is the time at the degree of consolidation

Table Time Factor. T\* versus degree of dissipation (Teh and Houlsby (1991))

		3 G 66. C C	0.000.6	7	011 01101	100.00)	
Degree of Dissipation (%)	20	30	40	50	60	70	80
T* (u <sub>2</sub> )	0.038	0.078	0.142	0.245	0.439	0.804	1.60

The coefficient of consolidation is typically analyzed using the time ( $t_{50}$ ) corresponding to a degree of dissipation of 50% ( $u_{50}$ ). In order to determine  $t_{50}$ , dissipation tests must be taken to a pressure less than  $u_{50}$ . The  $u_{50}$  value is half way between the initial maximum pore pressure and the equilibrium pore pressure value, known as  $u_{100}$ . To estimate  $u_{50}$ , both the initial maximum pore pressure and  $u_{100}$  must be known or estimated. Other degrees of dissipations may be considered, particularly for extremely long dissipations.

At any specific degree of dissipation the equilibrium pore pressure (u at  $t_{100}$ ) must be estimated at the depth of interest. The equilibrium value may be determined from one or more sources such as measuring the value directly ( $u_{100}$ ), estimating it from other dissipations in the same profile, estimating the phreatic surface and assuming hydrostatic conditions, from nearby soundings, from client provided information, from site observations and/or past experience, or from other site instrumentation.

For calculations of  $c_h$  (Teh and Houlsby (1991)),  $t_{50}$  values are estimated from the corresponding pore pressure dissipation curve and a rigidity index ( $I_r$ ) is assumed. For curves having an initial dilatory response in which an initial rise in pore pressure occurs before reaching a peak, the relative time from the peak value is used in determining  $t_{50}$ . In cases where the time to peak is excessive,  $t_{50}$  values are not calculated.

Due to possible inherent uncertainties in estimating  $I_r$ , the equilibrium pore pressure and the effect of an initial dilatory response on calculating  $t_{50}$ , other methods should be applied to confirm the results for  $c_h$ .



Additional published methods for estimating the coefficient of consolidation from a piezocone test are described in Burns and Mayne (1998, 2002), Jones and Van Zyl (1981), Robertson et al. (1992) and Sully et al. (1999).

A summary of the pore pressure dissipation tests and dissipation plots are presented in the relevant appendix.



ASTM D5778-12, 2012, "Standard Test Method for Performing Electronic Friction Cone and Piezocone Penetration Testing of Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D5778-12.

Burns, S.E. and Mayne, P.W., 1998, "Monotonic and dilatory pore pressure decay during piezocone tests", Canadian Geotechnical Journal 26 (4): 1063-1073. DOI: 1063-1073/T98-062.

Burns, S.E. and Mayne, P.W., 2002, "Analytical cavity expansion-critical state model cone dissipation in fine-grained soils", Soils & Foundations, Vol. 42(2): 131-137.

Jones, G.A. and Van Zyl, D.J.A., 1981, "The piezometer probe: a useful investigation tool", Proceedings, 10<sup>th</sup> International Conference on Soil Mechanics and Foundation Engineering, Vol. 3, Stockholm: 489-495.

Lunne, T., Robertson, P.K. and Powell, J. J. M., 1997, "Cone Penetration Testing in Geotechnical Practice", Blackie Academic and Professional.

Mayne, P.W., 2013, "Evaluating yield stress of soils from laboratory consolidation and in-situ cone penetration tests", Sound Geotechnical Research to Practice (Holtz Volume) GSP 230, ASCE, Reston/VA: 406-420. DOI: 10.1061/9780784412770.027.

Mayne, P.W. and Peuchen, J., 2012, "Unit weight trends with cone resistance in soft to firm clays", Geotechnical and Geophysical Site Characterization 4, Vol. 1 (Proc. ISC-4, Pernambuco), CRC Press, London: 903-910.

Mayne, P.W., 2014, "Interpretation of geotechnical parameters from seismic piezocone tests", CPT'14 Keynote Address, Las Vegas, NV, May 2014.

Robertson, P.K., Campanella, R.G., Gillespie, D. and Greig, J., 1986, "Use of Piezometer Cone Data", Proceedings of InSitu 86, ASCE Specialty Conference, Blacksburg, Virginia.

Robertson, P.K., 1990, "Soil Classification Using the Cone Penetration Test", Canadian Geotechnical Journal, Volume 27: 151-158. DOI: 10.1139/T90-014.

Robertson, P.K., Sully, J.P., Woeller, D.J., Lunne, T., Powell, J.J.M. and Gillespie, D.G., 1992, "Estimating coefficient of consolidation from piezocone tests", Canadian Geotechnical Journal, 29(4): 539-550. DOI: 10.1139/T92-061.

Robertson, P.K., 2009, "Interpretation of cone penetration tests – a unified approach", Canadian Geotechnical Journal, Volume 46: 1337-1355. DOI: 10.1139/T09-065.

Sully, J.P., Robertson, P.K., Campanella, R.G. and Woeller, D.J., 1999, "An approach to evaluation of field CPTU dissipation data in overconsolidated fine-grained soils", Canadian Geotechnical Journal, 36(2): 369-381. DOI: 10.1139/T98-105.

Teh, C.I., and Houlsby, G.T., 1991, "An analytical study of the cone penetration test in clay", Geotechnique, 41(1): 17-34. DOI: 10.1680/geot.1991.41.1.17.



Full flow penetration testing (BCPTu) is performed in conjunction with a piezocone penetration test using an integrated electronic piezocone with a spherical attachment and a data acquisition system manufactured by Adara Systems Ltd., a subsidiary of ConeTec.

ConeTec's piezocone penetrometers are compression type designs in which the tip and friction sleeve load cells are independent and have separate load capacities. The piezocones use strain gauged load cells for tip and sleeve friction and a strain gauged diaphragm type transducer for recording pore pressure. The piezocones also have a platinum resistive temperature device (RTD) for monitoring the temperature of the sensors, an accelerometer type dual axis inclinometer and a geophone sensor for recording seismic signals. All signals are amplified downhole within the cone body and the analog signals are sent to the surface through a shielded cable.

ConeTec penetrometers are manufactured with various tip, friction and pore pressure capacities in 5 cm², 10 cm² and 15 cm² tip base area configurations in order to maximize signal resolution for various soil conditions. The 15 cm² penetrometers do not require friction reducers as they have a diameter larger than the deployment rods. The 5 cm² and 10 cm² piezocones use a friction reducer consisting of a rod adapter extension behind the main cone body with an enlarged cross-sectional area (typically forty-four millimeter diameter over a length of thirty-two millimeters with tapered leading and trailing edges) located at a distance of 585 millimeters above the cone tip.

The penetrometers are designed with equal end area friction sleeves, a net end area ratio of 0.8 and cone tips with a sixty-degree apex angle.

The piezocone penetrometers are manufactured with dimensions, tolerances and sensor characteristics that are in general accordance with the current ASTM D5778 standard. ConeTec's calibration criteria also meet or exceed those of the current ASTM D5778 standard.

For ball full flow penetration tests, the cone tip is replaced with a spherical attachment that can have projected plan areas of 40 cm<sup>2</sup>, 60 cm<sup>2</sup>, 100 cm<sup>2</sup> or 150 cm<sup>2</sup>. The selection of the size is based on soil strength and deployment limitations. An illustration of the piezocone with a spherical attachment is presented in Figure BCPTu.

The specific piezocone and ball area used for each test is described in the ball full flow penetration test summary presented in the relevant appendix.



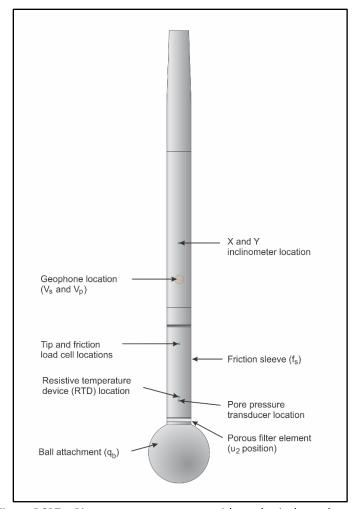


Figure BCPTu. Piezocone penetrometer with a spherical attachment

The ConeTec data acquisition systems consist of a Windows based computer and a signal conditioner and power supply interface box with a sixteen-bit (or greater) analog to digital (A/D) converter. The data is recorded in fixed depth increments using a depth wheel attached to the push cylinders or by using a spring loaded rubber depth wheel that is held against the cone rods. The typical recording interval is 2.5 centimeters; custom recording intervals are possible.

The system displays the data in real time and records the following parameters to a storage media during penetration:

- Depth
- Uncorrected ball tip resistance (q<sub>b</sub>)
- Sleeve friction (f<sub>s</sub>)
- Dynamic pore pressure (u) at the shoulder (u<sub>2</sub>) or at the equator of the ball
- Additional sensors such as resistivity, passive gamma, ultra violet induced fluorescence, if applicable



Prior to the start of a BCPTu sounding a suitable cone and spherical attachment are selected, the cone and data acquisition system are powered on, the pore pressure system is saturated with silicone oil and the baseline readings are recorded with the ball hanging freely in a vertical position.

The BCPTu is conducted at a steady rate of two centimeters per second, within acceptable tolerances. Typically, one-meter length rods with an outer diameter of 38.1 millimeters are added to advance the ball to the sounding termination depth. The test may be interrupted at selected depths to cycle the probe up and down in order to achieve a completely remolded soil state. Cycling is typically conducted during retraction of the ball and the number of conducted cycles is dependent on reaching a consistent tip value. After ball retraction the final baselines are recorded.

The full flow penetration test can be halted at specific depths to carry out pore pressure dissipation (PPD) tests. For each dissipation test the data acquisition system measures and records the variation of the pore pressure (u) with time (t). Pore pressure dissipation data can be interpreted to provide estimates of equilibrium pore pressures ( $u_{eq}$ ).

Additional information pertaining to ConeTec's full flow penetration testing procedures:

- Each filter is saturated in silicone oil under vacuum pressure prior to use
- Recorded baselines are checked with an independent multi-meter
- Baseline readings are compared to previous readings verifying compliance with ASTM standards
- Soundings are terminated at the client's target depth or at a depth where an obstruction is encountered, excessive rod flex occurs or excessive inclination occurs, equipment damage is likely to take place or a dangerous working environment arises
- Differences between initial and final baselines are calculated to ensure zero load offsets have not occurred and to ensure compliance with ASTM standards

Full flow penetration tests are conducted to assess the undrained shear strength (Su) of low to medium strength soils. During penetration, the soil flows around the penetrometer significantly reducing the influence of overburden stress as compared to the cone penetration test (CPTu). For the test to be valid, the soil must flow around the penetrometer. Cycling is conducted in order to achieve a completely remolded soil state to provide an indication of sensitivity in soft soils.

The recorded ball tip resistance  $(q_b)$  is the total force acting on the piezocone spherical attachment divided by its base area. The ball tip resistance is corrected for pore pressure effects and termed corrected ball tip resistance  $(q_{bt})$  according to the following expression:

$$q_{bt} = q_b + [(1-a)u_2] \frac{A_s}{A_p}$$

where:  $q_{bt}$  is the corrected ball tip resistance  $q_{bt}$  is the recorded ball tip resistance  $u_{2t}$  is the recorded dynamic pore pressure behind the tip ( $u_{2t}$  position) a is the Net Area Ratio for the piezocone (0.8 for ConeTec probes)  $A_{st}$  is the shaft area  $A_{pt}$  is the ball plan area



The undrained shear strength (Su) derived from the full flow penetration test is related to the net ball tip resistance (q<sub>btnet</sub>) and ball factor (N<sub>ball</sub>) using the following relationship:

$$Su = \frac{q_{btnet}}{N_{ball}}$$

Due to different geometry and the subdued sleeve and pore pressure response, full flow penetration test results are not used for the interpretation of other geotechnical parameters or for soil classification.

A summary of the BCPTu soundings along with test details and individual plots are provided in the appendices. Tabular results generated for each sounding are provided in Excel format in the data release folder. Information regarding the calculated parameters is also included in the data release folder.

For additional information on full flow penetrometer testing, refer to Weemees et al. (2006).

### References

ASTM D5778-12, 2012, "Standard Test Method for Performing Electronic Friction Cone and Piezocone Penetration Testing of Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D5778-12.

Weemees, I., Howie, J., Woeller, D.J., Sharp, J.T., Cargill, E., Greig, J., 2006, "Improved Techniques for the In-Situ Determination of Undrained Shear Strength in Soft Clays," Sea to Sky Geotechnics, Proceedings of the 59th Canadian Geotechnical Conference, Vancouver, B.C., 1–4 October. BiTech Publishers Ltd., Richmond, B.C. pp. 89–95.



The electric field vane system is manufactured by Adara Systems Ltd., a subsidiary of ConeTec. An illustration of the uphole vane system configuration is presented in Figure eVST.

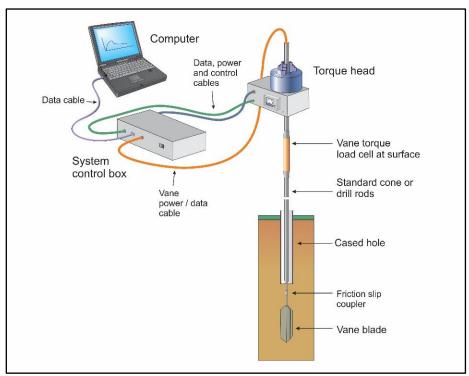


Figure eVST. Illustration of the uphole electric field vane system configuration

The vane system is designed with an array of strain gauges in a load cell that measure the applied torque. The torque signal is amplified and converted to digital data within the tool and transmitted to the data acquisition system through a shielded cable. The system uses a friction slip coupler to permit the free slip or play of approximately fifteen degrees between the rods and the vane blade in order to isolate and record rod friction from the soil before rotation of the vane blade starts. The system is designed to use vane blades of various sizes and configurations that connect to the friction slip coupler. The vane blades manufactured by Adara have dimensions and tolerances that are in general accordance with the current ASTM D2573 standards. In very soft soil conditions and at the request of the client, ConeTec may use a large diameter vane blade that exceeds the ASTM D2573 maximum size specifications in order to maximize torque resolution. In very stiff soil conditions and at the request of the client, ConeTec may use a smaller diameter vane blade than the minimum size specified in ASTM D2573 in order to obtain a peak torque below the capacity of the load cell.

The electric motor (capable of 100 Newton-meters of torque) is designed to clamp onto and rotate the rods and vane blade at a constant rate.

ConeTec's calibration criteria of the load cells are in accordance with the current ASTM D2573 standard.



The data acquisition system consists of a computer that records the vane data every 0.2 degrees of rotation. The system records the following parameters and saves them to a file as the test is conducted:

- Torque in Newton-meters
- Rotation in degrees
- Elapsed time in seconds (from the start of the test)

All testing is performed in accordance to ConeTec's field vane testing operating procedures and in general accordance with the current ASTM D2573 standard. For additional information on vane shear testing refer to Greig et al. (1987).

Prior to the start of a vane shear test profile, a suitable sized vane blade is selected, the vane system is powered on and the vane load cell baseline reading is recorded with the load cell hanging freely in a vertical position.

The vane blade, slip coupler and rods are advanced to the desired test depth through a cased hole, typically using AWJ drill rods or one-meter length rods with an outer diameter of 1.5 inches (38.1 millimeters). Test depths are referenced to the middle of the rectangular portion of the vane blade. The motor rotates the rods at a near constant rate up to and beyond the yield stress (peak) until the load remains near constant (post peak). Following post peak readings, the vane blade is then rapidly rotated clockwise ten times to completely remold the soil. The test procedure is repeated in order to record the remolded strength of the soil. The vane blade is then advanced to the next depth and the procedure is repeated or the vane blade is retracted to allow for drilling and vane blade size changes. Once the vane profile is complete, the final baseline of the load cell is recorded and compared to previous reading as a QA/QC check.

Undrained shear strength from the field vane,  $(S_u)_{fv}$ , is calculated from torque measurements using the following general equation (ASTM D2573) taking into consideration the case of rectangular or tapered ends at the top and/or bottom of the vane blade.

$$(S_u)_{fv} = \frac{12 \cdot T_{max}}{\pi D^2 \left(\frac{D}{\cos(i_T)} + \frac{D}{\cos(i_B)} + 6H\right)}$$



where:

 $(S_u)_{fv}$  = undrained shear strength from the field vane

 $T_{max}$  = maximum value of torque

D = vane diameter

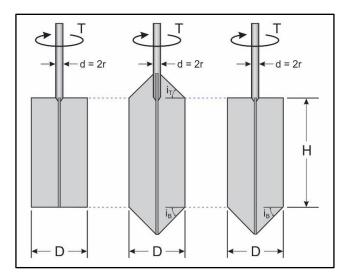
H = height of the rectangular portion of the vane

i<sub>T</sub> = angle of taper at vane top (with respect to horizontal)

 $i_B$  = angle of taper at vane

bottom (with respect to

horizontal)



For rectangular vane blades where H/D = 2, the above equation simplifies to:

$$(S_u)_{\text{fv}} = \frac{6 \cdot T_{\text{max}}}{7\pi D^3}$$

The recorded rod friction is subtracted from the peak and remolded torque. No correction factors are applied to the vane results to derive the mobilized shear strength ( $\tau_{mobilized}$ ).

A summary of the vane shear tests, a table of results and individual VST plots are provided in the relevant appendices. Tabular data in Excel format is provided in the data release folder.

### References

ASTM D2573 / D2573M-18, 2018, "Standard Test Method for Field Vane Shear Test in Saturated Fine-Grained Soils", ASTM International, West Conshohocken, PA. DOI: 10.1520/D2573\_D2573M-18.

Greig, J.W., R.G. Campanella and P.K. Robertson, 1987, "Comparison of Field Vane Results With Other In-Situ Test Results", International Symposium on Laboratory and Field Vane Shear Strength Testing, ASTM, Tampa, FL, Proceedings.



The appendices listed below are included in the report:

- Cone Penetration Test Summary and Standard Cone Penetration Test Plots
- Advanced Cone Penetration Test Plots with Ic, Su(Nkt), Phi and N(60)Ic/N1(60)Ic
- Soil Behavior Type (SBT) Scatter Plots
- Ball Cone Penetration Test Summary and Plots
- Electronic Vane Test Summary and Results
- Electronic Vane Test Plots



Cone Penetration Test Summary and Standard Cone Penetration Test Plots





Job No: 21-59-22445
Client: Anchor QEA
Project: LDW Phase 3
Start Date: 06-Jul-2021
End Date: 29-Jul-2021

### CONE PENETRATION TEST SUMMARY Assumed Final Refer to Phreatic Longitude<sup>3</sup> Latitude<sup>3</sup> Sounding ID Cone File Name Date Depth Notation Surface<sup>1</sup> (deg) (deg) (ft) Number (ft) LDW21-GT06-GC 21-59-22445 CP06 22-Jul-2021 681:T375F10U35 -5.0 31.1 47.52892 -122.31483 IDW21-GT14-GC 08-Jul-2021 681:T375F10U35 47.52477 -122.30819 21-59-22445\_CP14 -5.6 28.7 LDW21-GT16-GC 21-59-22445 CP16 08-Jul-2021 681:T375F10U35 -8.4 29.8 47.52409 -122.30770 -6.6 30.3 LDW21-GT17-GC 21-59-22445 CP17 12-Jul-2021 681:T375F10U35 4 LDW21-GT20-GC 21-59-22445 CP20 16-Jul-2021 681:T375F10U35 -6.6 23.0 4 LDW21-GT22-GC 21-59-22445 CP22 13-Jul-2021 681:T375F10U35 -7.7 28.8 4 16-Jul-2021 LDW21-GT27-GC 21-59-22445\_CP27 681:T375F10U35 -3.0 30.4 4 LDW21-GT30-GC 21-59-22445 CP30 21-Jul-2021 681:T375F10U35 -7.0 30.1 47.52066 -122.30558 LDW21-GT31-GC 21-59-22445 CP31 09-Jul-2021 681:T375F10U35 2.0 11.4 4,2 LDW21-GT31-GC-B 21-59-22445 CP31B 13-Jul-2021 681:T375F10U35 -5.0 27.3 4 LDW21-GT32-GC 09-Jul-2021 681:T375F10U35 2.0 47.52028 -122.30553 21-59-22445 CP32 5.8 2 LDW21-GT32-GC-B 21-Jul-2021 681:T375F10U35 47.52030 -122.30555 21-59-22445 CP32B -2.0 30.8 LDW21-GT34-GC 21-59-22445 CP34 21-Jul-2021 681:T375F10U35 -2.8 47.51986 -122.30540 30.3 LDW21-GT40-GC 21-59-22445 CP40 19-Jul-2021 681:T375F10U35 -4.9 31.7 47.51155 -122.30247 LDW21-GT45-GC 28-Jul-2021 -7.2 47.51254 -122.29899 21-59-22445 CP45 681:T375F10U35 31.6 LDW21-GT46-GC 21-59-22445 CP46 26-Jul-2021 681:T375F10U35 -13.2 9.8 47.51233 -122.29862 LDW21-GT47-GC 27-Jul-2021 681:T375F10U35 47.51242 -122.29865 21-59-22445 CP47 -12.5 31.2 LDW21-GT49-GC 21-59-22445 CP49 28-Jul-2021 681:T375F10U35 -6.5 32.5 47.51235 -122.29820 23-Jul-2021 LDW21-GT50-GC 21-59-22445 CP50 681:T375F10U35 -11.6 5.5 47.51207 -122.29793



Job No: 21-59-22445
Client: Anchor QEA
Project: LDW Phase 3
Start Date: 06-Jul-2021
End Date: 29-Jul-2021

CONE PENETRATION TEST SUMMARY								
Sounding ID	File Name	Date	Cone	Assumed Phreatic Surface <sup>1</sup> (ft)	Final Depth (ft)	Latitude <sup>3</sup> (deg)	Longitude <sup>3</sup> (deg)	Refer to Notation Number
LDW21-GT51-GC	21-59-22445_CP51	26-Jul-2021	681:T375F10U35	-6.4	6.6	47.51218	-122.29794	
LDW21-GT52-GC	21-59-22445_CP52	27-Jul-2021	681:T375F10U35	-6.9	30.4	47.51211	-122.29774	
LDW21-GT54-GC	21-59-22445_CP54	27-Jul-2021	681:T375F10U35	-6.0	30.8	47.51197	-122.29758	
Totals	22 soundings				547.89			

- 1. Phreatic surface measured from barge deck with weighted tip tape at each location. Hydrostatic profile applied to interpretation tables
- 2. CPT sounding completed from land based machine all other locations completed from floating barge platform.
- 3. Coordinates were provided by client
- 4. Coordinates currently not available. Coordinates will be provided by client at a later date



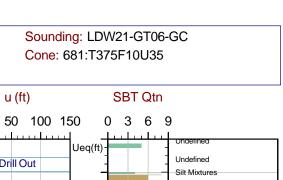
qt (tsf)

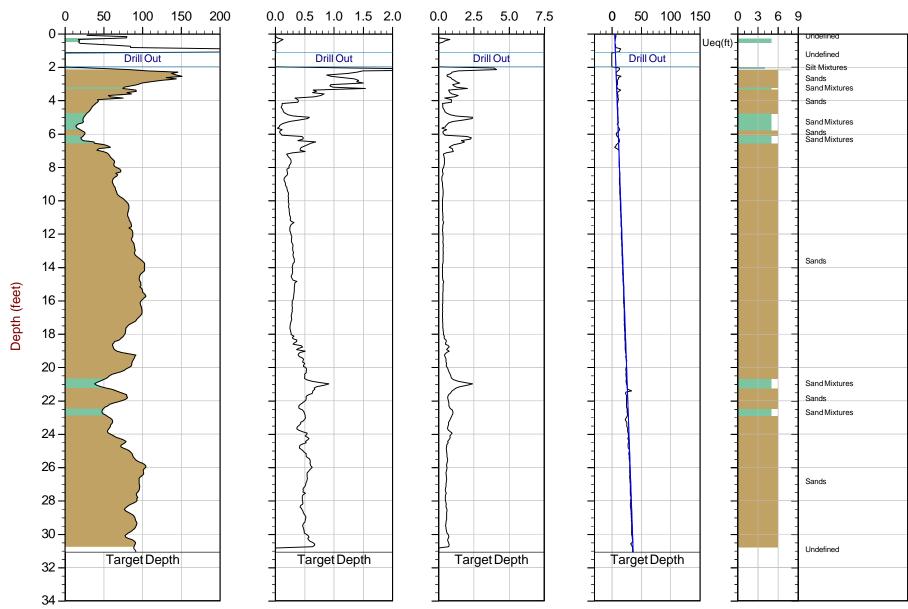
Job No: 21-59-22445 Date: 2021-07-22 17:30

Rf (%)

Site: LDW Phase 3

fs (tsf)





Max Depth: 9.475 m / 31.09 ftDepth Inc: 0.025 m / 0.082 ftAvg Int: Every Point

File: 21-59-22445\_CP06.COR Unit Wt: SBTQtn (PKR2009)

SBT: Robertson, 2009 and 2010

Coords: Lat: 47.52892 Long: -122.31483



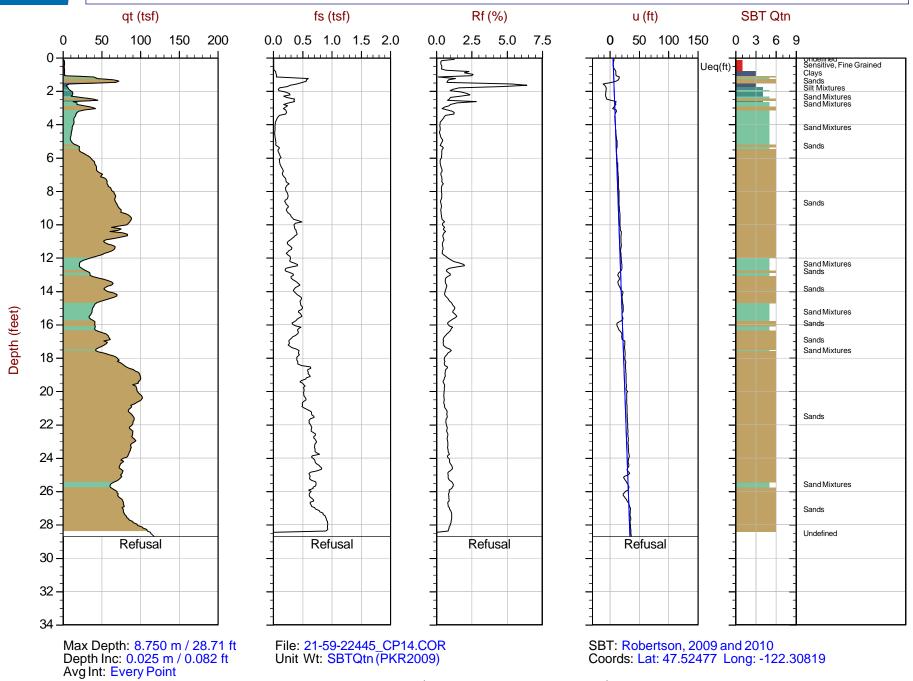
Job No: 21-59-22445 Date: 2021-07-08 14:11

Site: LDW Phase 3

Sounding: LDW21-GT14-GC Cone: 681:T375F10U35

Coords: Lat: 47.52477 Long: -122.30819

Hydrostatic Line



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

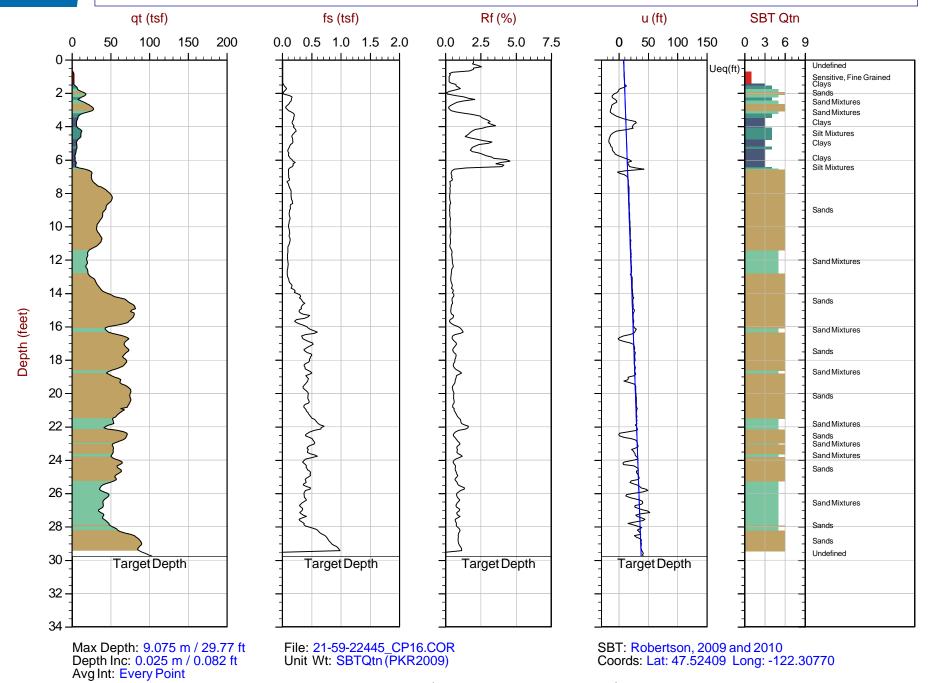
The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Job No: 21-59-22445 Date: 2021-07-08 16:24 Sounding: LDW21-GT16-GC Cone: 681:T375F10U35

Hydrostatic Line

Site: LDW Phase 3



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

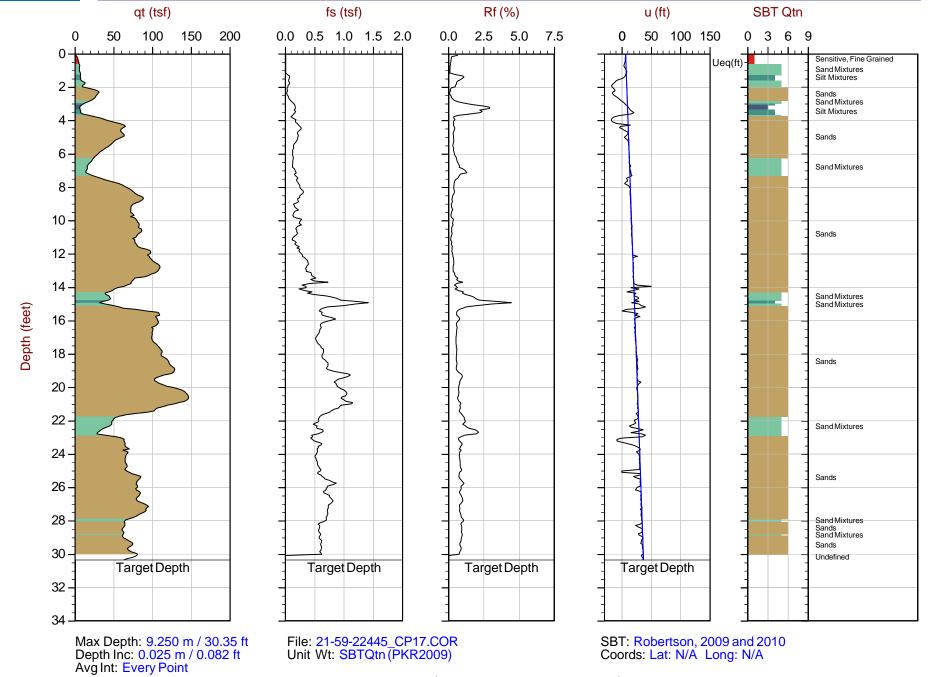
The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Job No: 21-59-22445 Date: 2021-07-12 19:15

Site: LDW Phase 3







6

8

10 -

12 -

14 -

16 -

18 -

20

22

24

26

28

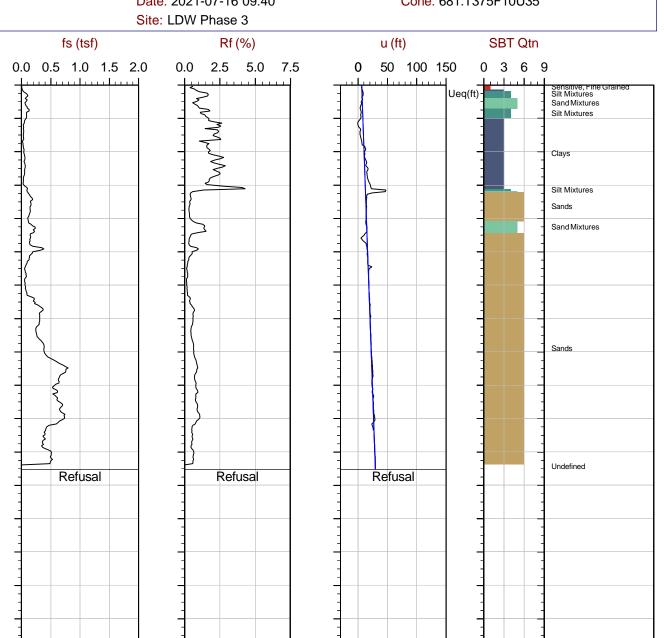
30

32

100 150 200

qt (tsf)

Job No: 21-59-22445 Date: 2021-07-16 09:40 Sounding: LDW21-GT20-GC Cone: 681:T375F10U35



Max Depth: 7.025 m / 23.05 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

Refusal

File: 21-59-22445\_CP20.COR Unit Wt: SBTQtn (PKR2009)

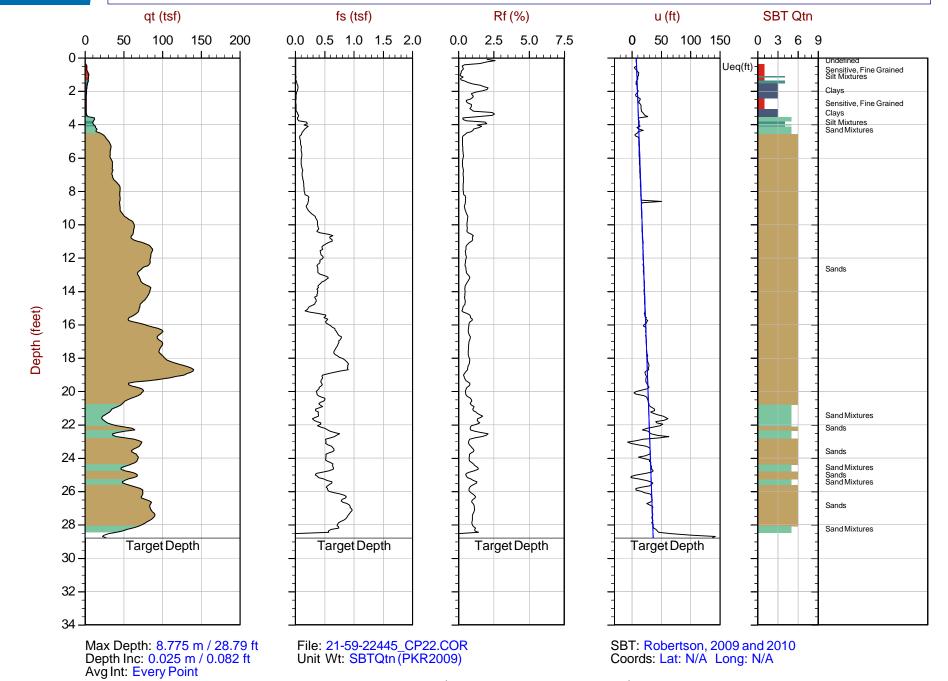
SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A



Job No: 21-59-22445 Date: 2021-07-13 19:06

Site: LDW Phase 3

Sounding: LDW21-GT22-GC Cone: 681:T375F10U35





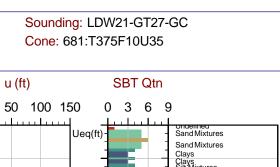
qt (tsf)

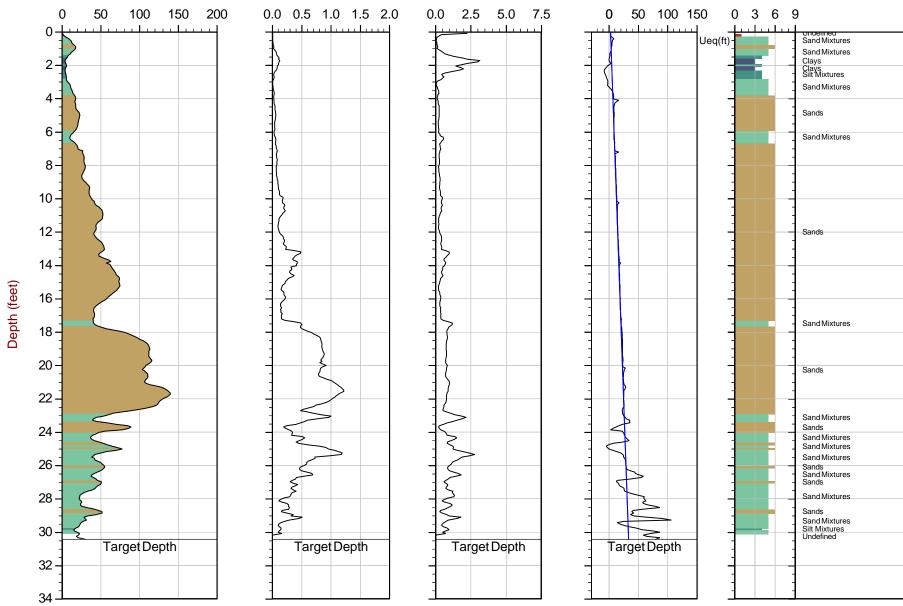
Job No: 21-59-22445 Date: 2021-07-16 08:30

Rf (%)

Site: LDW Phase 3

fs (tsf)





Max Depth: 9.275 m / 30.43 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP27.COR Unit Wt: SBTQtn (PKR2009)

SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

Hydrostatic Line

Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

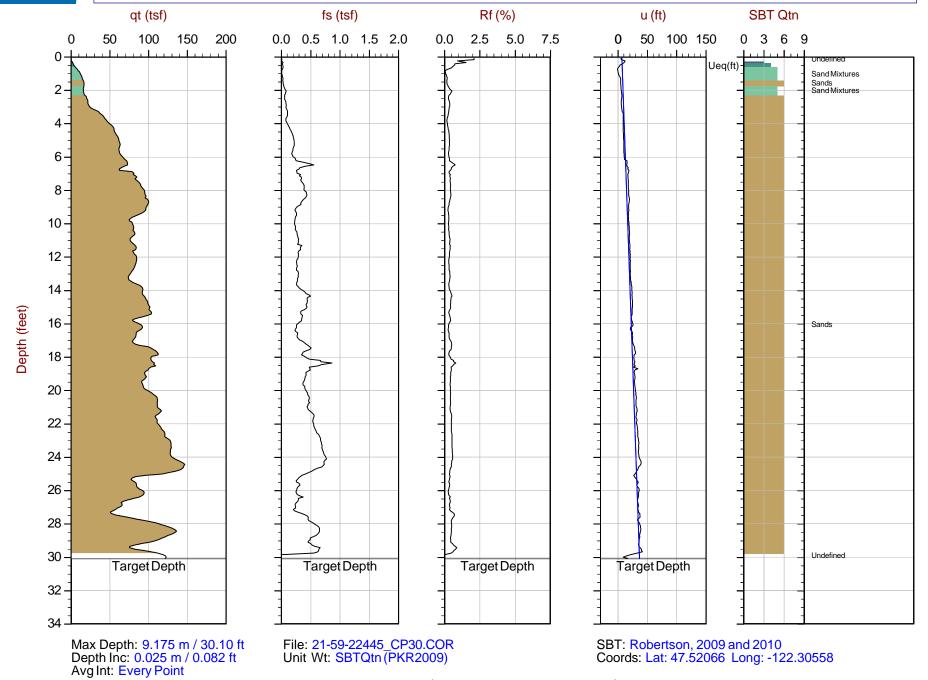


# Anchor QEA

Job No: 21-59-22445 Date: 2021-07-21 15:09

Site: LDW Phase 3

Sounding: LDW21-GT30-GC Cone: 681:T375F10U35

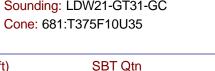


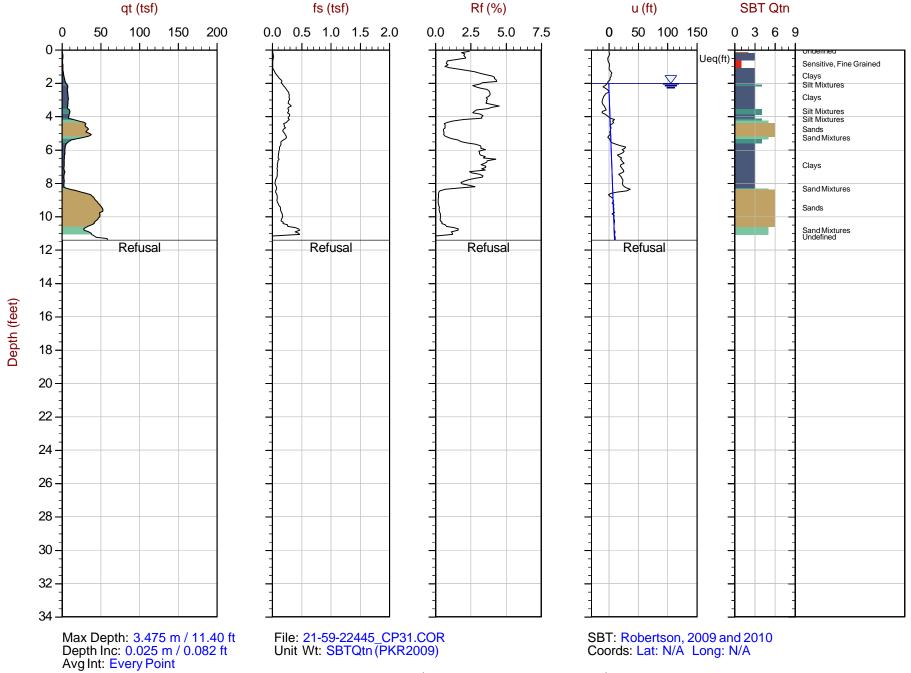


Job No: 21-59-22445 Date: 2021-07-09 10:35

Site: LDW Phase 3

Sounding: LDW21-GT31-GC





Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



# Anchor QEA

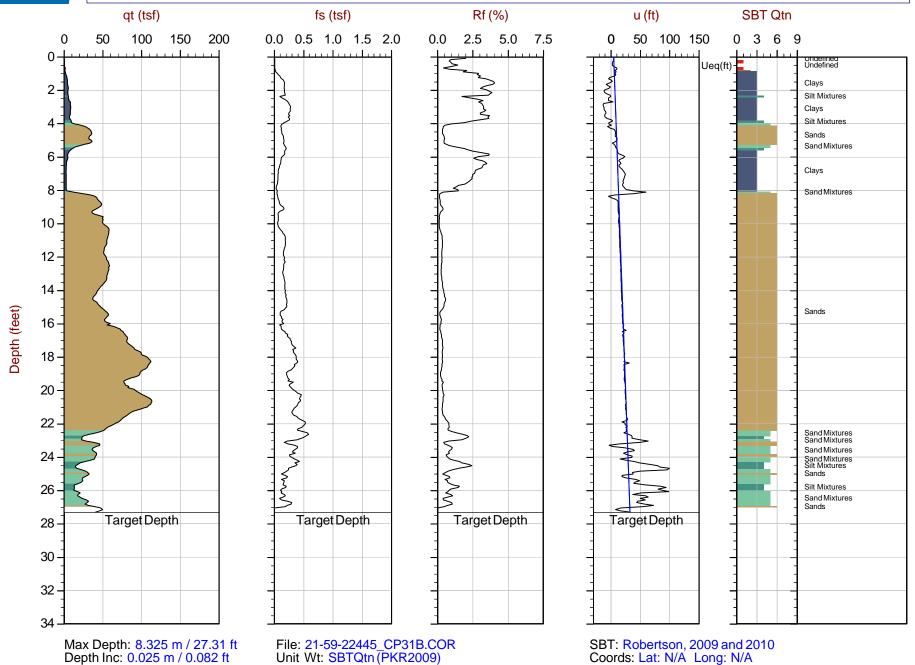
Job No: 21-59-22445 Date: 2021-07-13 17:56

Site: LDW Phase 3

Sounding: LDW21-GT31-GC-B

Hydrostatic Line

Cone: 681:T375F10U35



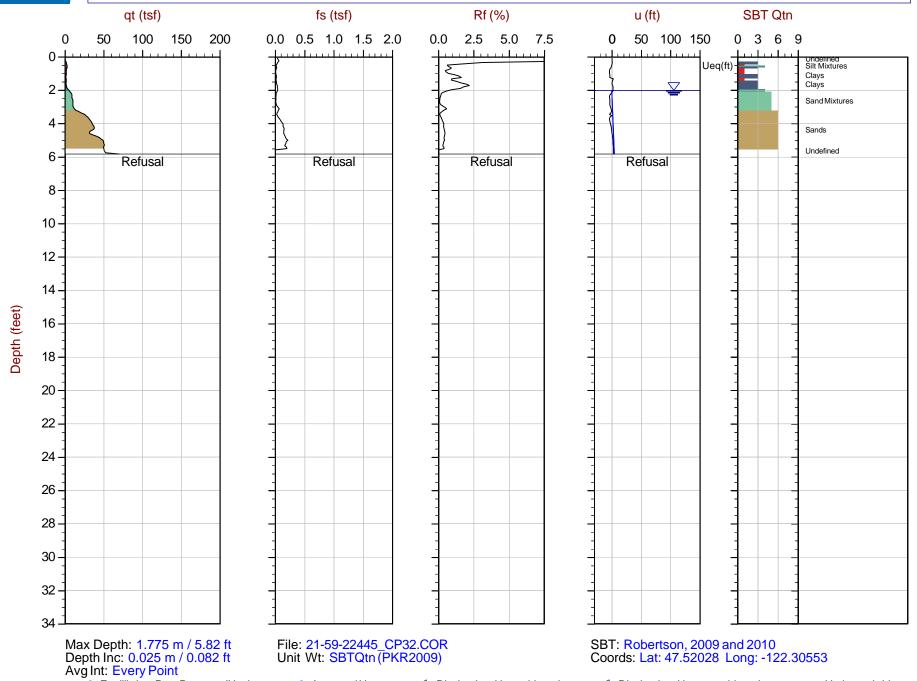


Job No: 21-59-22445 Date: 2021-07-09 11:18

Site: LDW Phase 3

Sounding: LDW21-GT32-GC

Cone: 681:T375F10U35



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Coords: Lat: 47.52028 Long: -122.30553



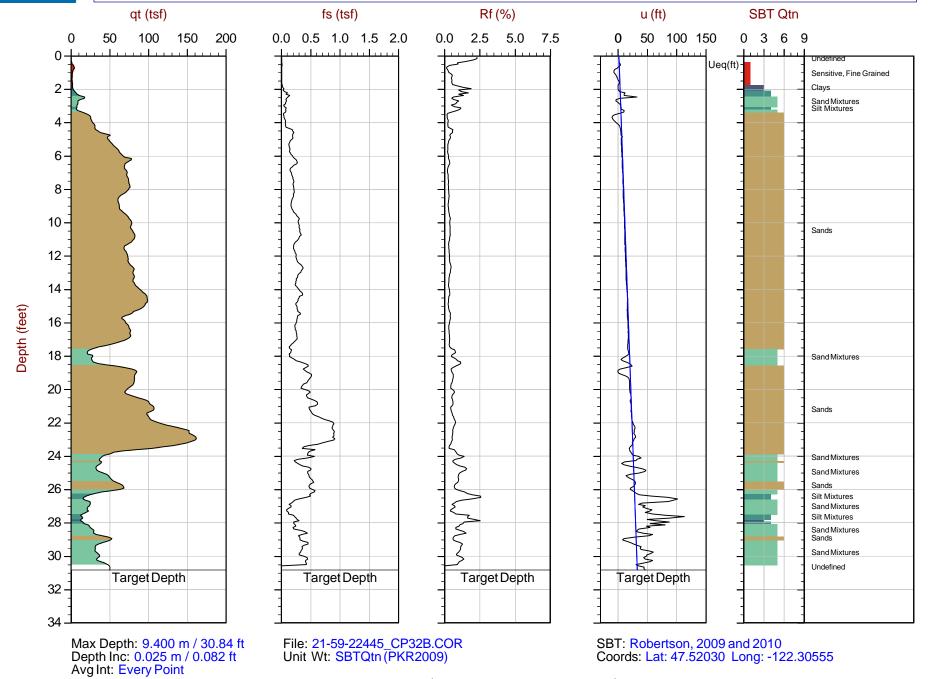
Job No: 21-59-22445 Date: 2021-07-21 13:24

Site: LDW Phase 3

Sounding: LDW21-GT32-GC-B

Cone: 681:T375F10U35

Coords: Lat: 47.52030 Long: -122.30555





qt (tsf)

Job No: 21-59-22445 Date: 2021-07-21 14:17

Rf (%)

Site: LDW Phase 3

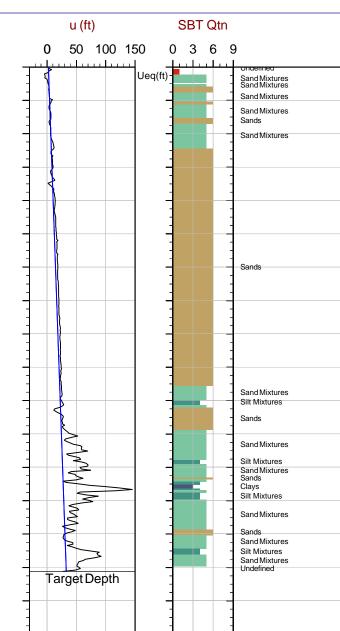
fs (tsf)

File: 21-59-22445\_CP34.COR Unit Wt: SBTQtn (PKR2009)

Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

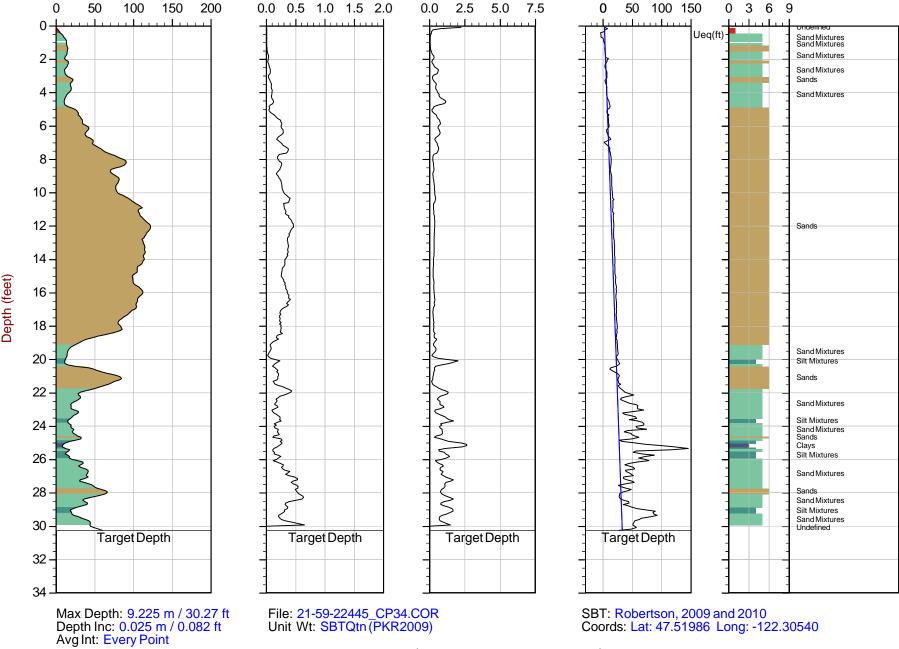
The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Sounding: LDW21-GT34-GC Cone: 681:T375F10U35



SBT: Robertson, 2009 and 2010

Coords: Lat: 47.51986 Long: -122.30540





Job No: 21-59-22445 Date: 2021-07-19 13:58

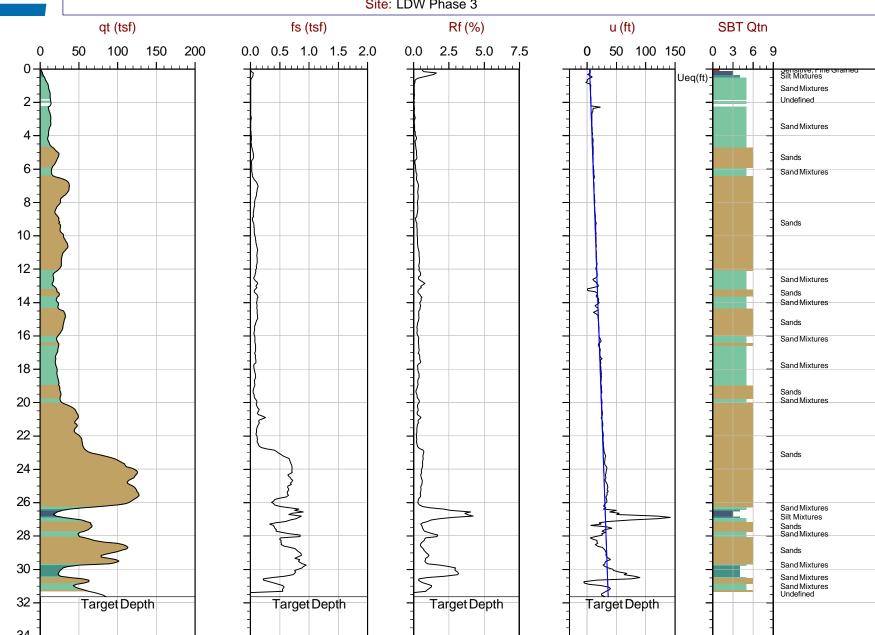
Site: LDW Phase 3

Sounding: LDW21-GT40-GC Cone: 681:T375F10U35

SBT: Robertson, 2009 and 2010

Coords: Lat: 47.51155 Long: -122.30247

Hydrostatic Line



Max Depth: 9.650 m / 31.66 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

File: 21-59-22445\_CP40.COR Unit Wt: SBTQtn (PKR2009)



0

# Anchor QEA

100 150 200

qt (tsf)

Job No: 21-59-22445 Date: 2021-07-28 18:24

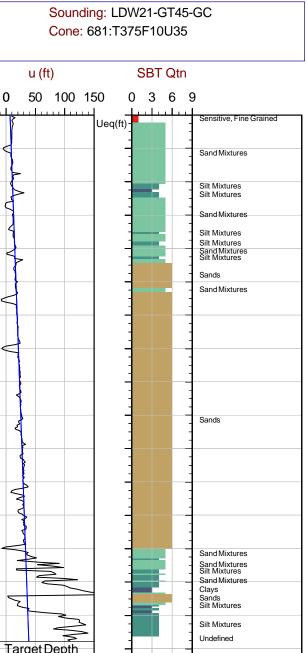
Rf (%)

0.0 2.5 5.0 7.5

Site: LDW Phase 3

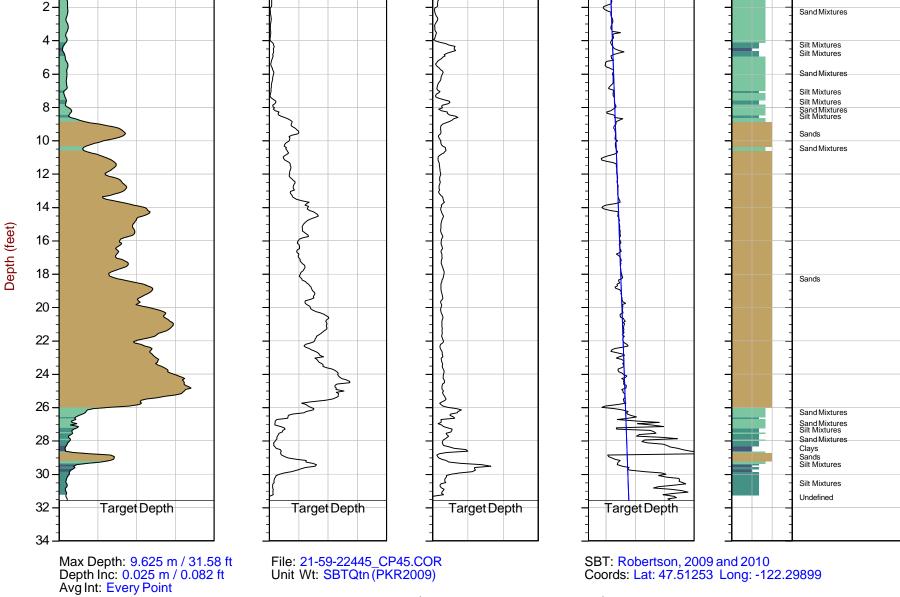
fs (tsf)

0.0 0.5 1.0 1.5 2.0



Coords: Lat: 47.51253 Long: -122.29899

Hydrostatic Line



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



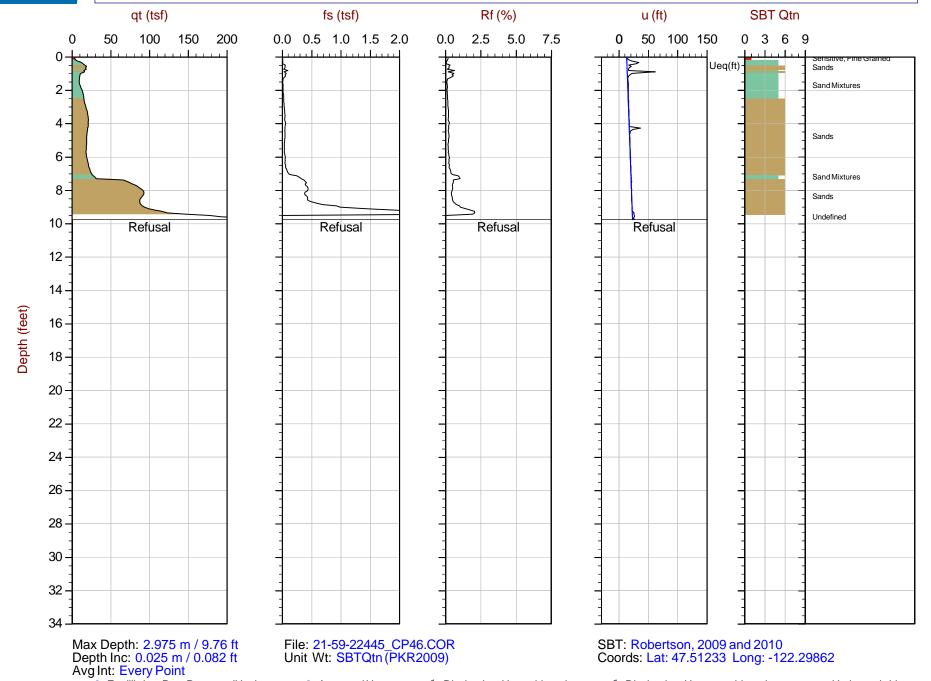
Job No: 21-59-22445 Date: 2021-07-26 09:49

Site: LDW Phase 3

Sounding: LDW21-GT46-GC

Hydrostatic Line

Cone: 681:T375F10U35





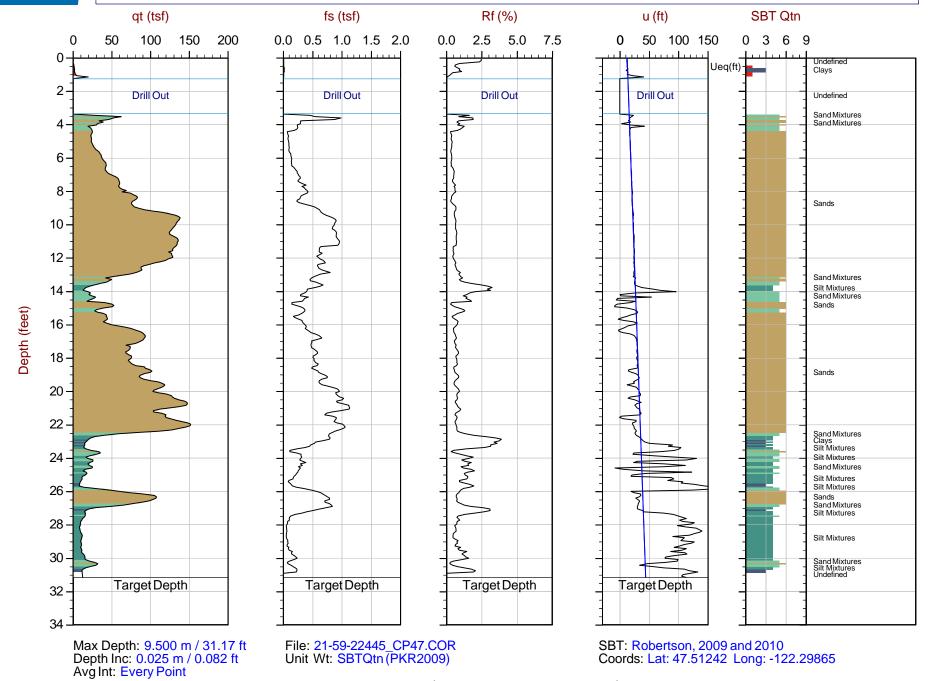
Job No: 21-59-22445 Date: 2021-07-27 20:39

Cone: 681:T375F10U35

Sounding: LDW21-GT47-GC

Hydrostatic Line

Site: LDW Phase 3



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



0

# Anchor QEA

100 150 200

qt (tsf)

Job No: 21-59-22445 Date: 2021-07-28 19:27

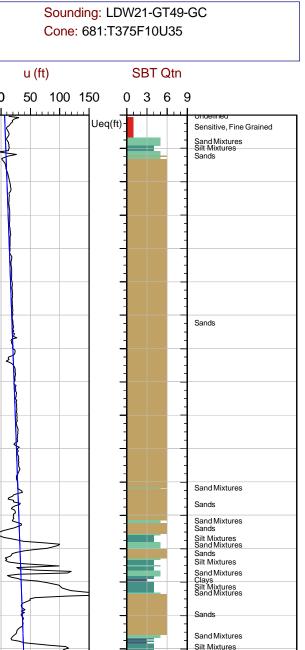
Rf (%)

0.0 2.5 5.0 7.5

Site: LDW Phase 3

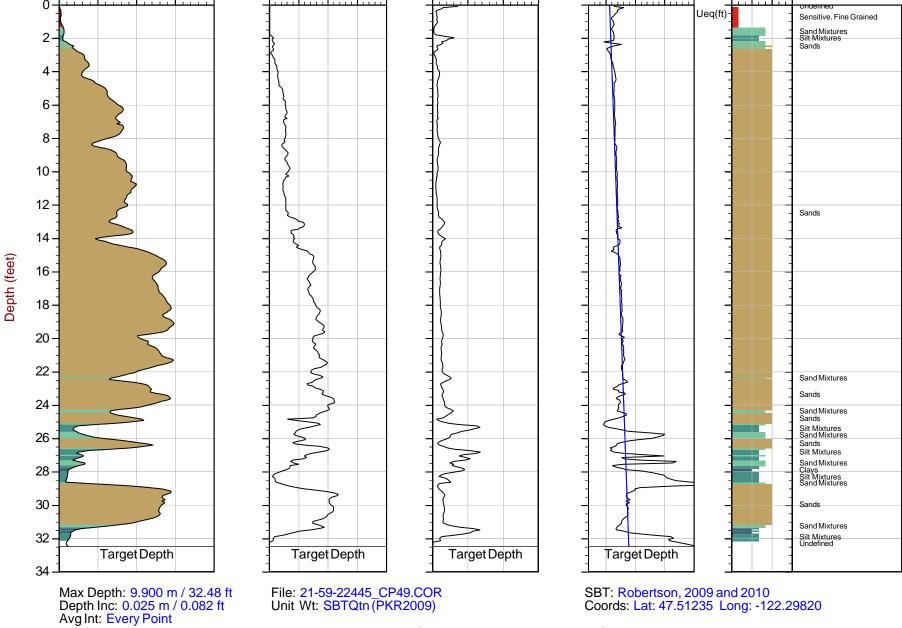
fs (tsf)

0.0 0.5 1.0 1.5 2.0



Coords: Lat: 47.51235 Long: -122.29820

Hydrostatic Line



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

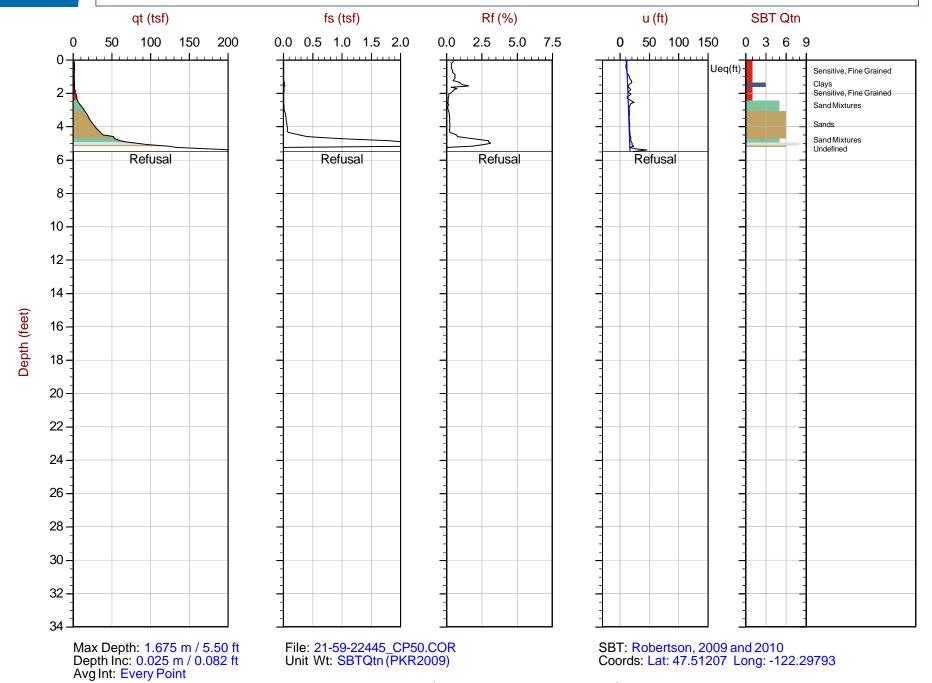


Job No: 21-59-22445 Date: 2021-07-23 15:21

Site: LDW Phase 3

Sounding: LDW21-GT50-GC

Cone: 681:T375F10U35



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Coords: Lat: 47.51207 Long: -122.29793



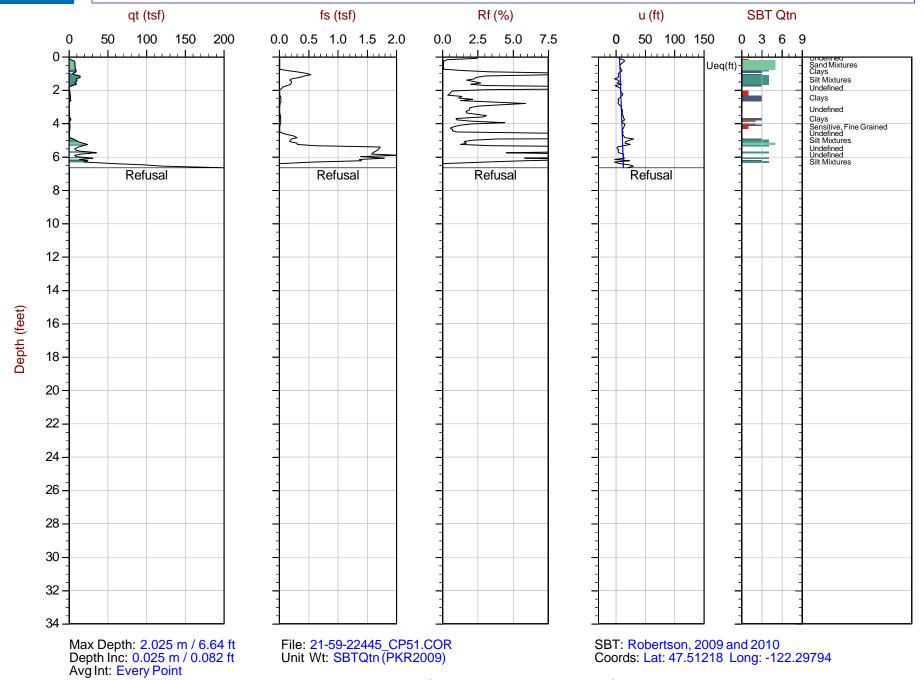
Job No: 21-59-22445 Date: 2021-07-26 19:23

Site: LDW Phase 3

Sounding: LDW21-GT51-GC

Cone: 681:T375F10U35

Coords: Lat: 47.51218 Long: -122.29794



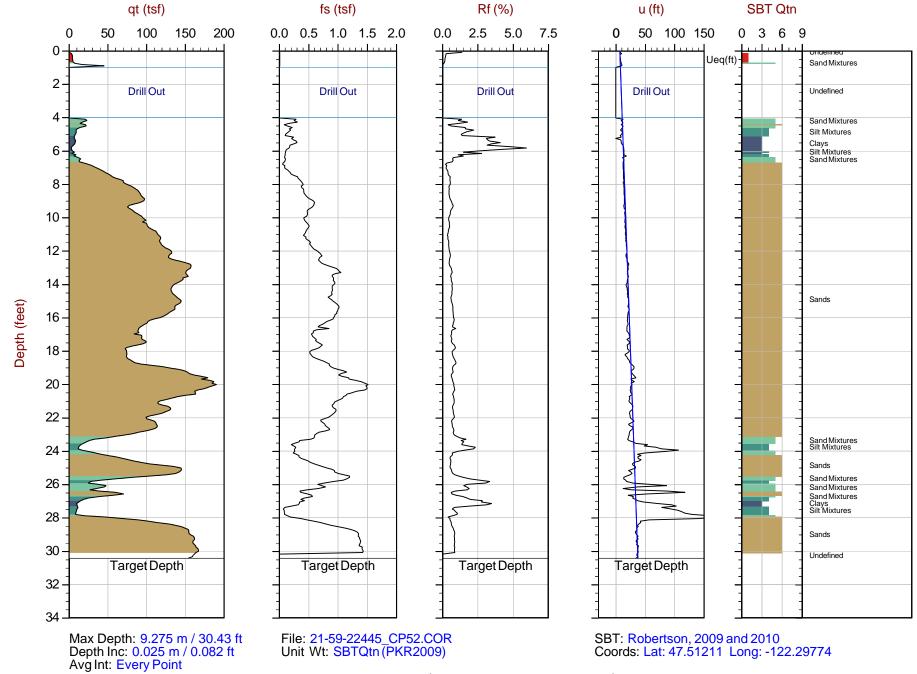


Job No: 21-59-22445 Date: 2021-07-27 19:40

Site: LDW Phase 3



Hydrostatic Line

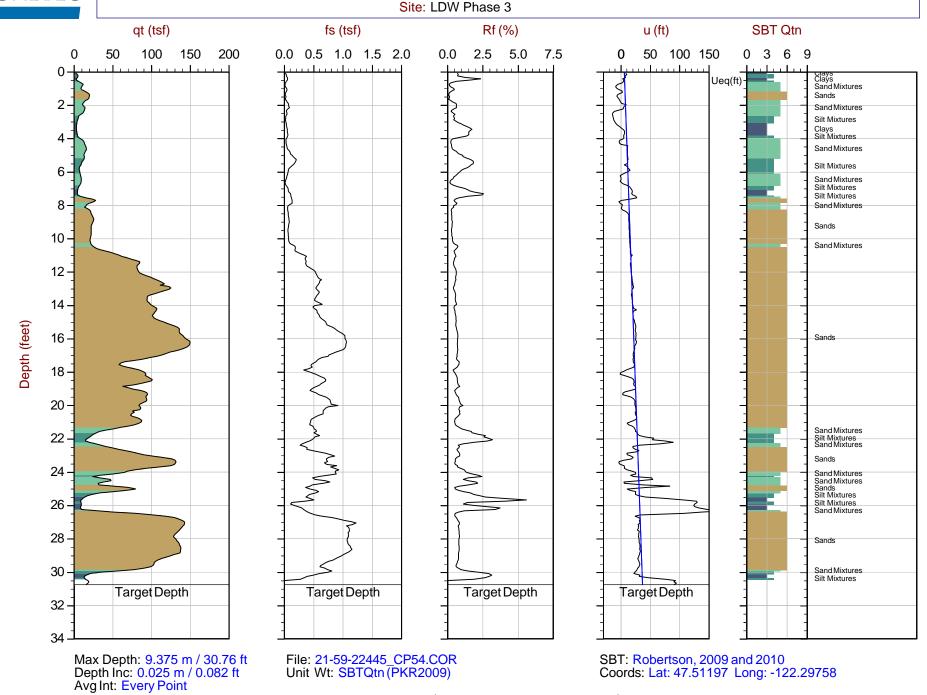


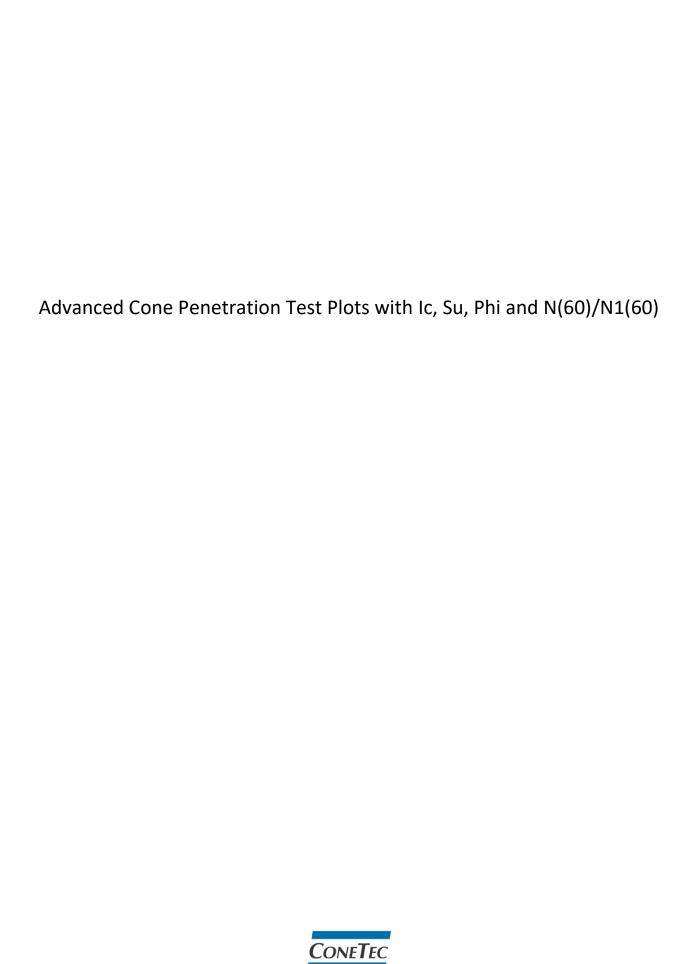
Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Job No: 21-59-22445 Date: 2021-07-27 18:31 Sounding: LDW21-GT54-GC Cone: 681:T375F10U35





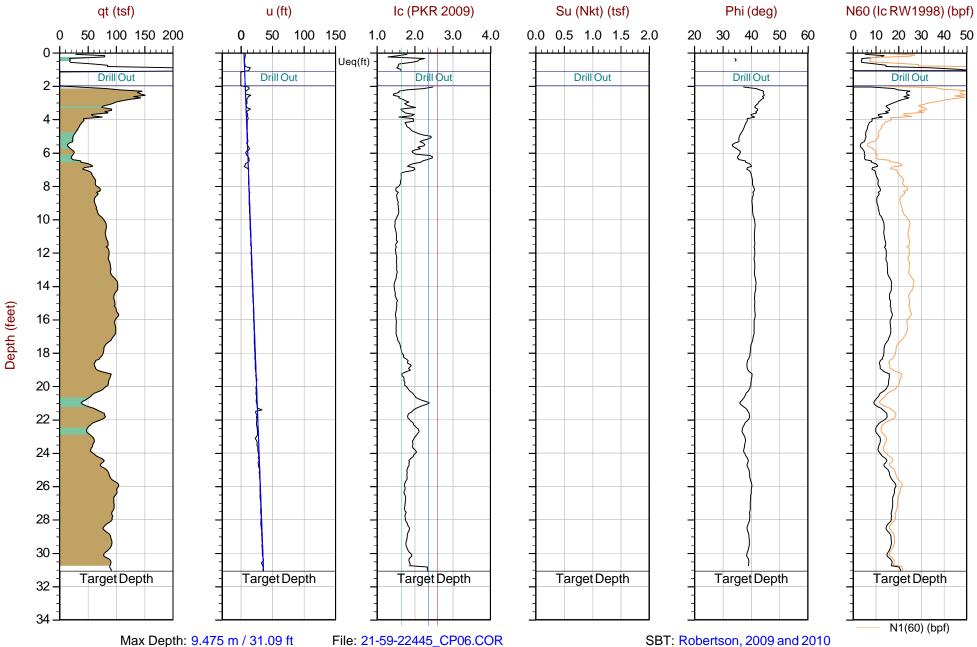


Job No: 21-59-22445 Date: 2021-07-22 17:30

Site: LDW Phase 3

Sounding: LDW21-GT06-GC

Cone: 681:T375F10U35



Max Depth: 9.475 m / 31.09 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP06.COR Unit Wt: SBTQtn(PKR2009) Su Nkt: 15.0

Coords: Lat: 47.52892 Long: -122.31483

Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Job No: 21-59-22445 Date: 2021-07-08 14:11

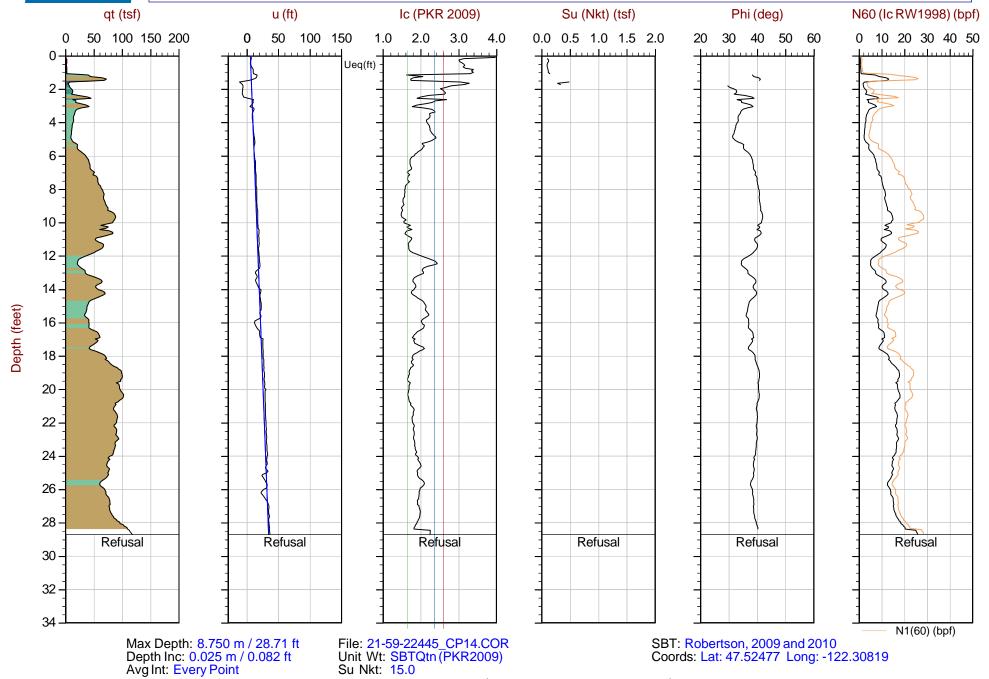
Site: LDW Phase 3

Sounding: LDW21-GT14-GC

Cone: 681:T375F10U35

Coords: Lat: 47.52477 Long: -122.30819

Hydrostatic Line



Su Nkt: 15.0

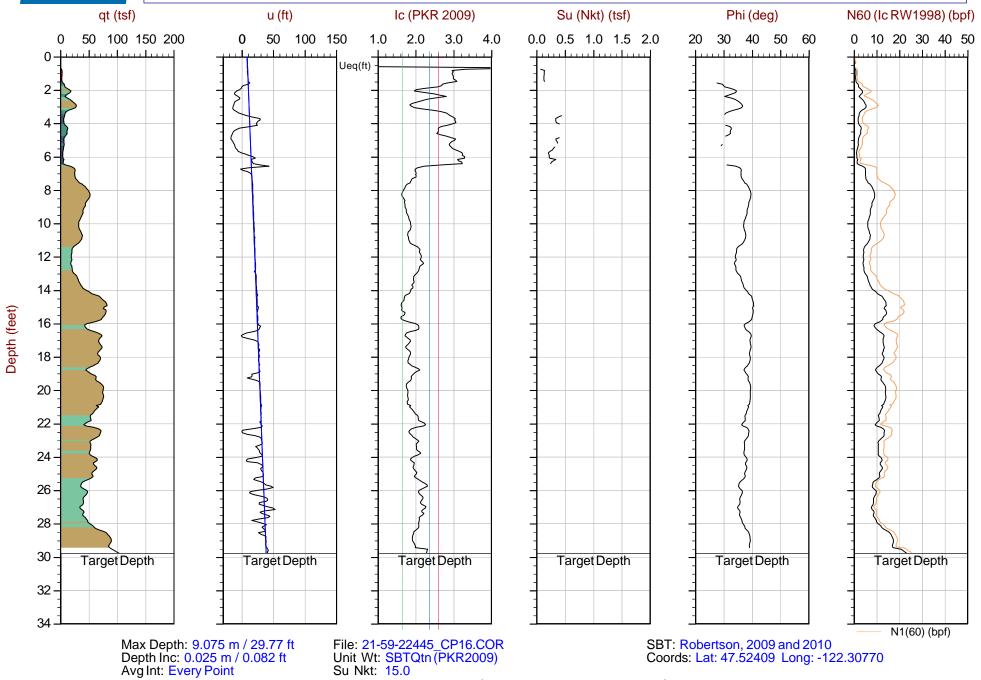


Job No: 21-59-22445 Date: 2021-07-08 16:24

Site: LDW Phase 3

Sounding: LDW21-GT16-GC

Cone: 681:T375F10U35



Su Nkt: 15.0

Coords: Lat: 47.52409 Long: -122.30770



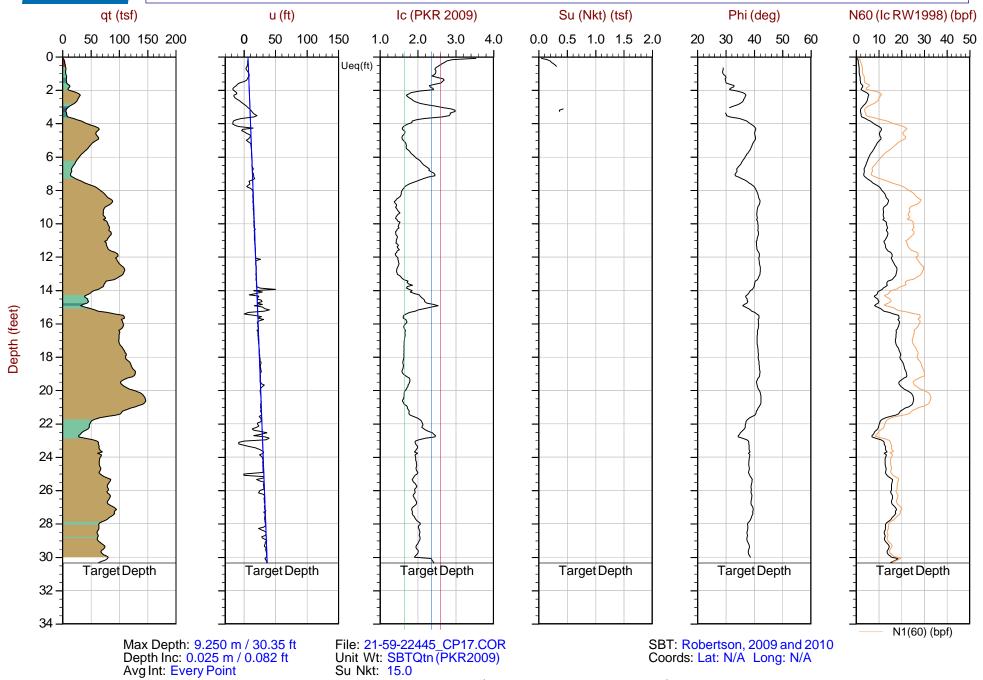
Job No: 21-59-22445 Date: 2021-07-12 19:15

Site: LDW Phase 3

Sounding: LDW21-GT17-GC

Hydrostatic Line

Cone: 681:T375F10U35



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0

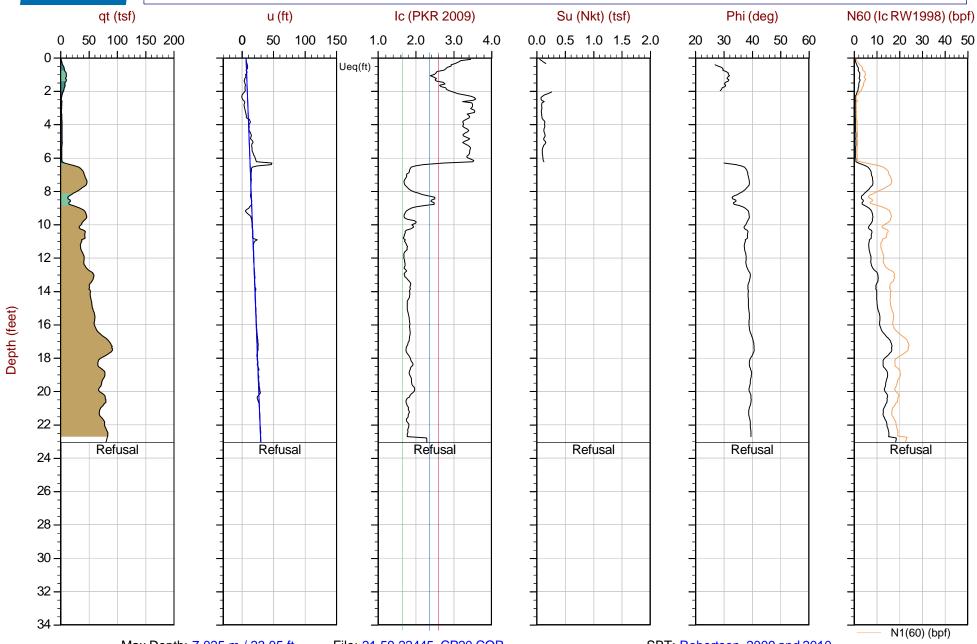


Job No: 21-59-22445 Date: 2021-07-16 09:40

Site: LDW Phase 3

Sounding: LDW21-GT20-GC

Cone: 681:T375F10U35



Max Depth: 7.025 m / 23.05 ftDepth Inc: 0.025 m / 0.082 ftAvg Int: Every Point File: 21-59-22445\_CP20.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0 SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

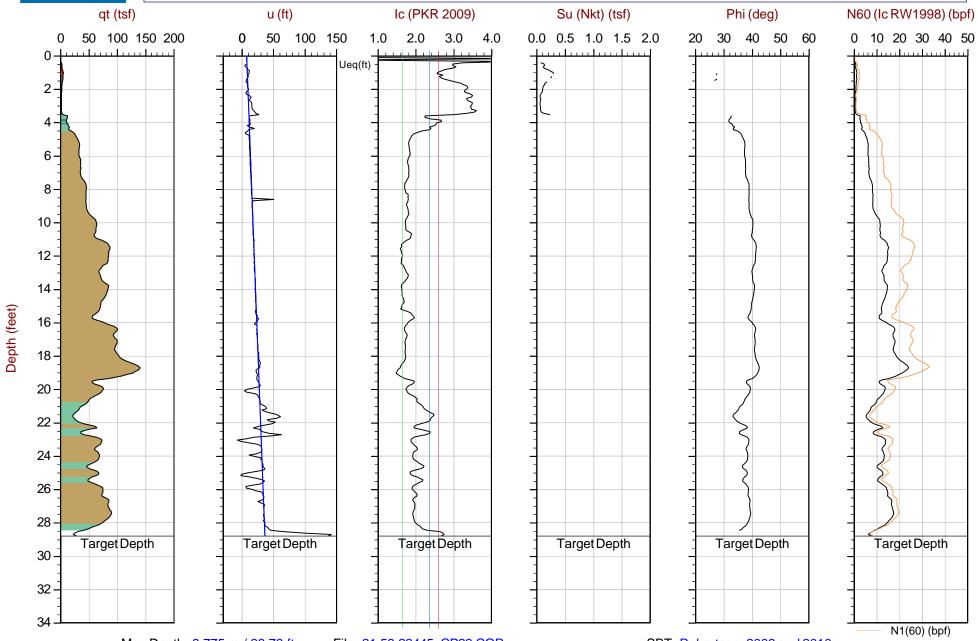


Job No: 21-59-22445 Date: 2021-07-13 19:06

Site: LDW Phase 3

Sounding: LDW21-GT22-GC

Cone: 681:T375F10U35



Max Depth: 8.775 m / 28.79 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP22.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

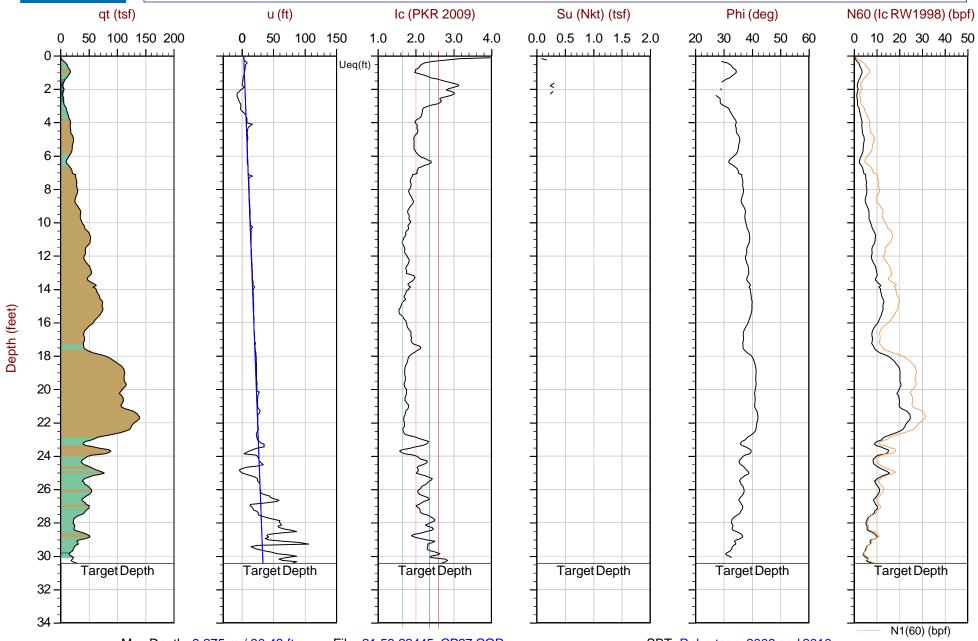


Job No: 21-59-22445 Date: 2021-07-16 08:30

Site: LDW Phase 3

Sounding: LDW21-GT27-GC

Cone: 681:T375F10U35



Max Depth: 9.275 m / 30.43 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP27.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

Hydrostatic Line

Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

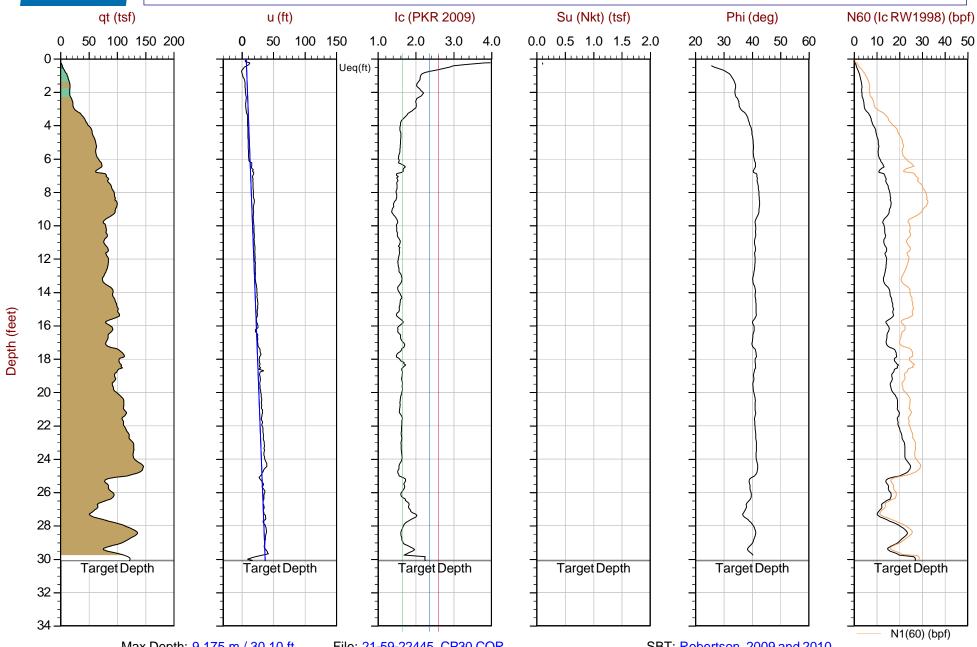


Job No: 21-59-22445 Date: 2021-07-21 15:09

Site: LDW Phase 3

Sounding: LDW21-GT30-GC

Cone: 681:T375F10U35



Max Depth: 9.175 m / 30.10 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP30.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: 47.52066 Long: -122.30558

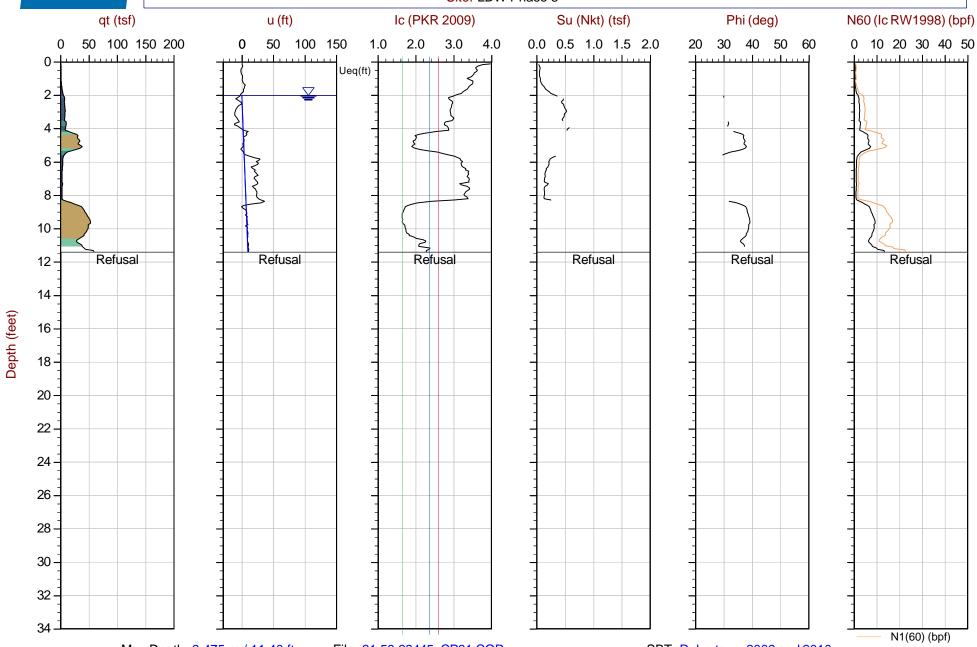


Job No: 21-59-22445 Date: 2021-07-09 10:35

Site: LDW Phase 3

Sounding: LDW21-GT31-GC

Cone: 681:T375F10U35



Max Depth: 3.475 m / 11.40 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP31.COR Unit Wt: SBTQtn(PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

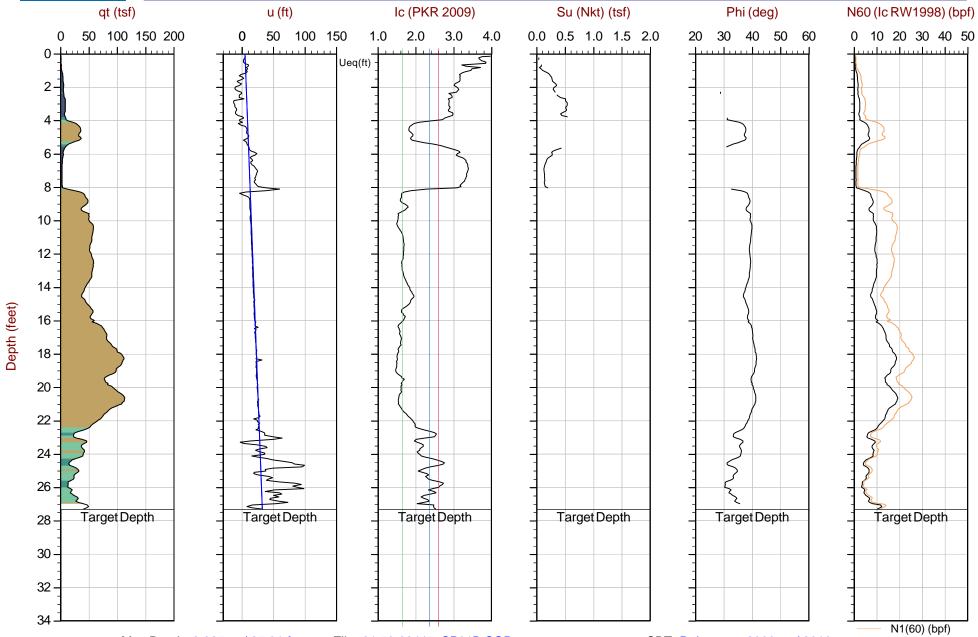


Job No: 21-59-22445 Date: 2021-07-13 17:56

Site: LDW Phase 3

Sounding: LDW21-GT31-GC-B

Cone: 681:T375F10U35



Max Depth: 8.325 m / 27.31 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP31B.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: N/A Long: N/A

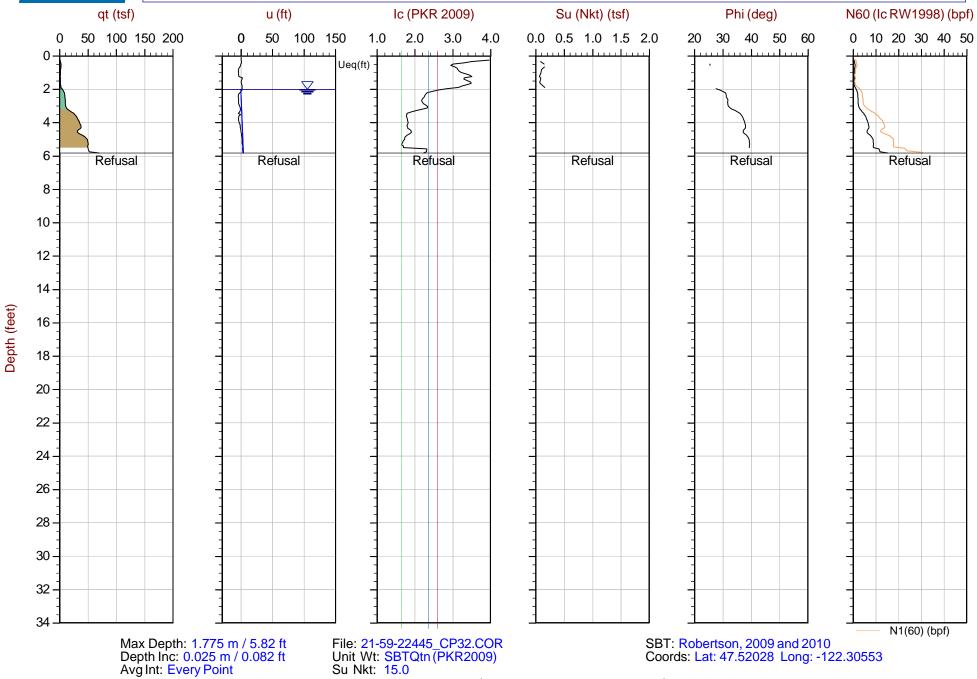


Job No: 21-59-22445 Date: 2021-07-09 11:18

Site: LDW Phase 3

Sounding: LDW21-GT32-GC

Cone: 681:T375F10U35



Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0

Coords: Lat: 47.52028 Long: -122.30553

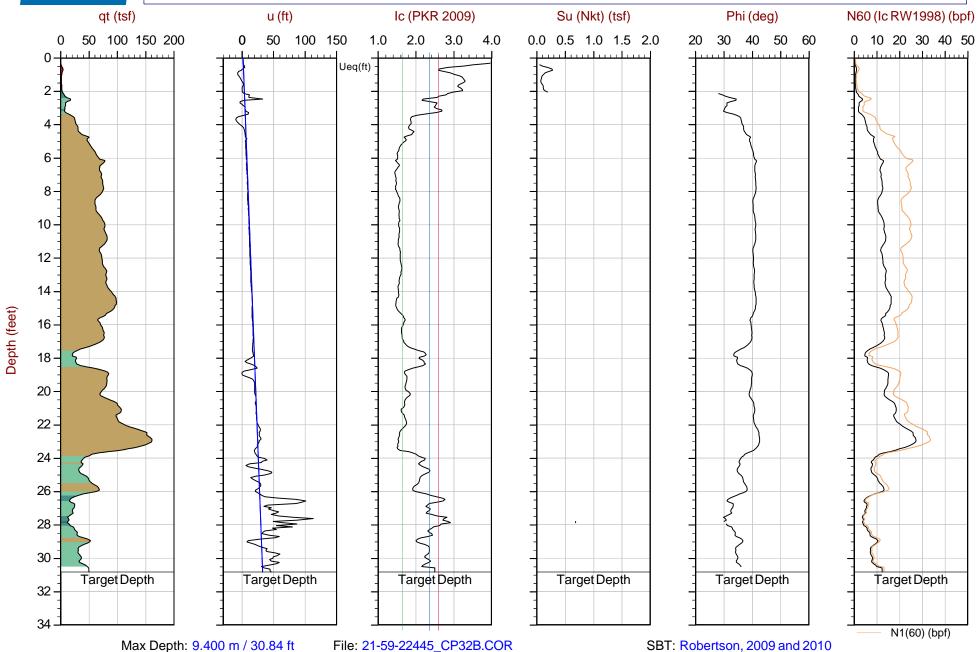


Job No: 21-59-22445 Date: 2021-07-21 13:24

Site: LDW Phase 3

Sounding: LDW21-GT32-GC-B

Cone: 681:T375F10U35



Max Depth: 9.400 m / 30.84 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP32B.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

Coords: Lat: 47.52030 Long: -122.30555

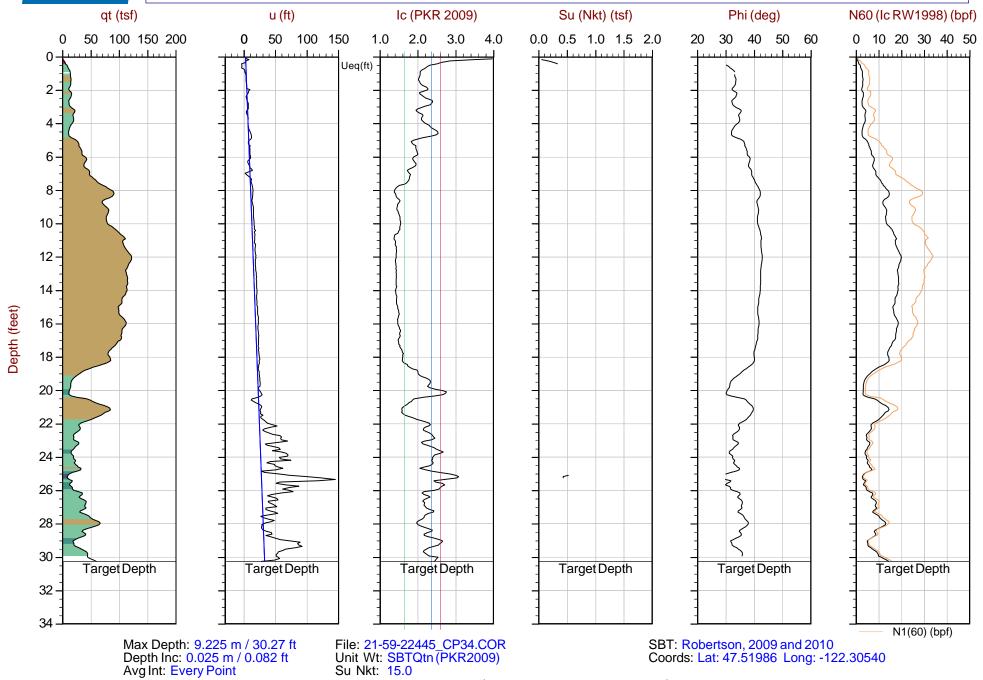


Job No: 21-59-22445 Date: 2021-07-21 14:17

Site: LDW Phase 3

Sounding: LDW21-GT34-GC

Cone: 681:T375F10U35



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0

Coords: Lat: 47.51986 Long: -122.30540

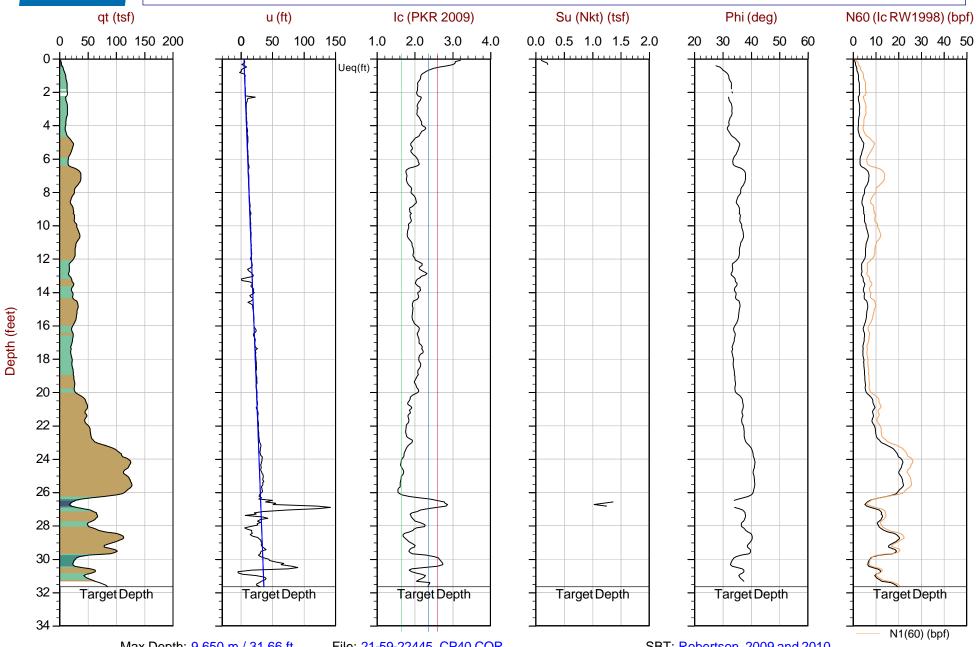


Job No: 21-59-22445 Date: 2021-07-19 13:58

Site: LDW Phase 3

Sounding: LDW21-GT40-GC

Cone: 681:T375F10U35



Max Depth: 9.650 m / 31.66 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP40.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

SBT: Robertson, 2009 and 2010 Coords: Lat: 47.51155 Long: -122.30247

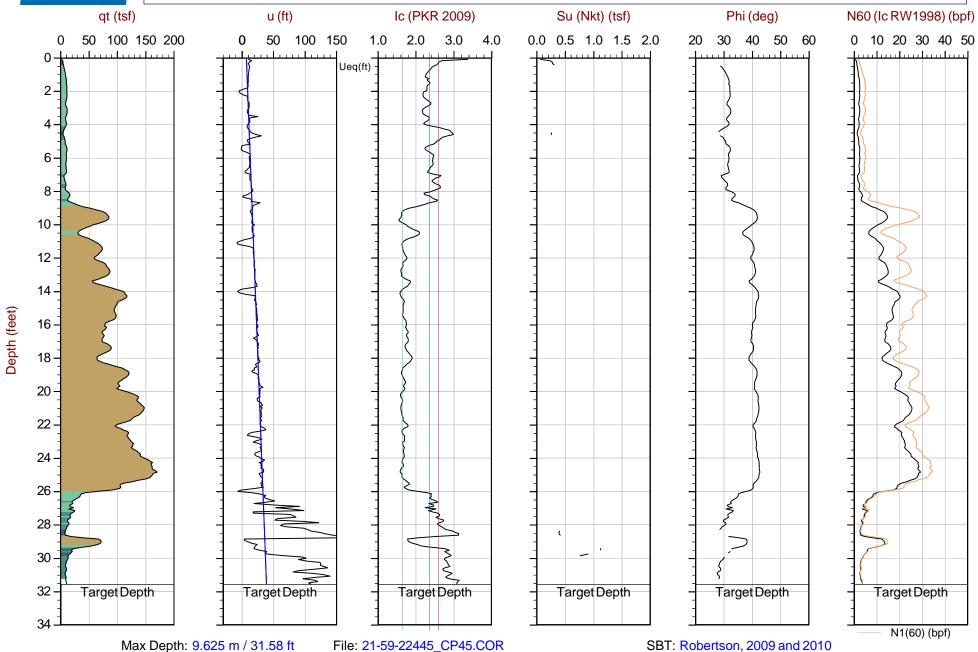


Job No: 21-59-22445 Date: 2021-07-28 18:24

Site: LDW Phase 3

Sounding: LDW21-GT45-GC

Cone: 681:T375F10U35



Max Depth: 9.625 m / 31.58 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP45.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

Coords: Lat: 47.51253 Long: -122.29899

Hydrostatic Line

Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

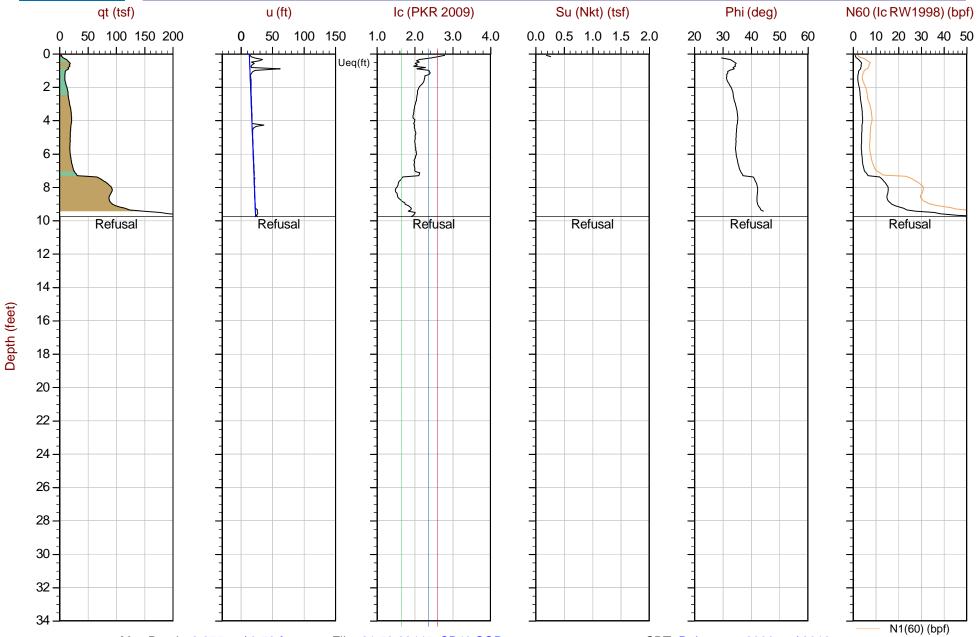


Job No: 21-59-22445 Date: 2021-07-26 09:49

Site: LDW Phase 3

Sounding: LDW21-GT46-GC

Cone: 681:T375F10U35



Max Depth: 2.975 m / 9.76 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP46.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0 SBT: Robertson, 2009 and 2010 Coords: Lat: 47.51233 Long: -122.29862



Job No: 21-59-22445 Date: 2021-07-27 20:39

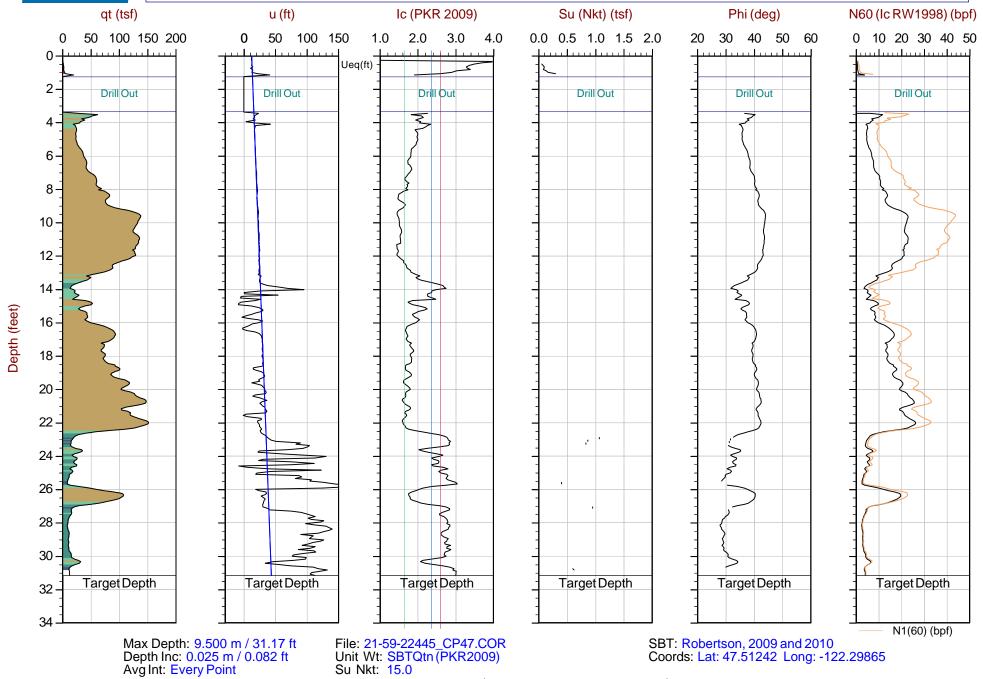
Site: LDW Phase 3

Sounding: LDW21-GT47-GC

Cone: 681:T375F10U35

Coords: Lat: 47.51242 Long: -122.29865

Hydrostatic Line



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0



Job No: 21-59-22445 Date: 2021-07-28 19:27

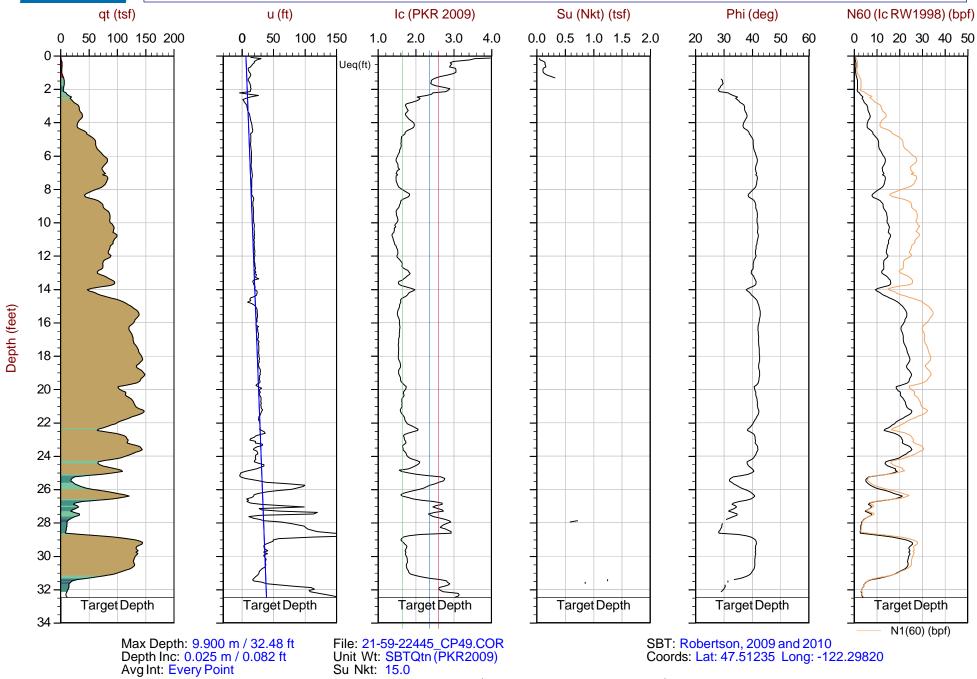
Site: LDW Phase 3

Sounding: LDW21-GT49-GC

Cone: 681:T375F10U35

Coords: Lat: 47.51235 Long: -122.29820

Hydrostatic Line



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0

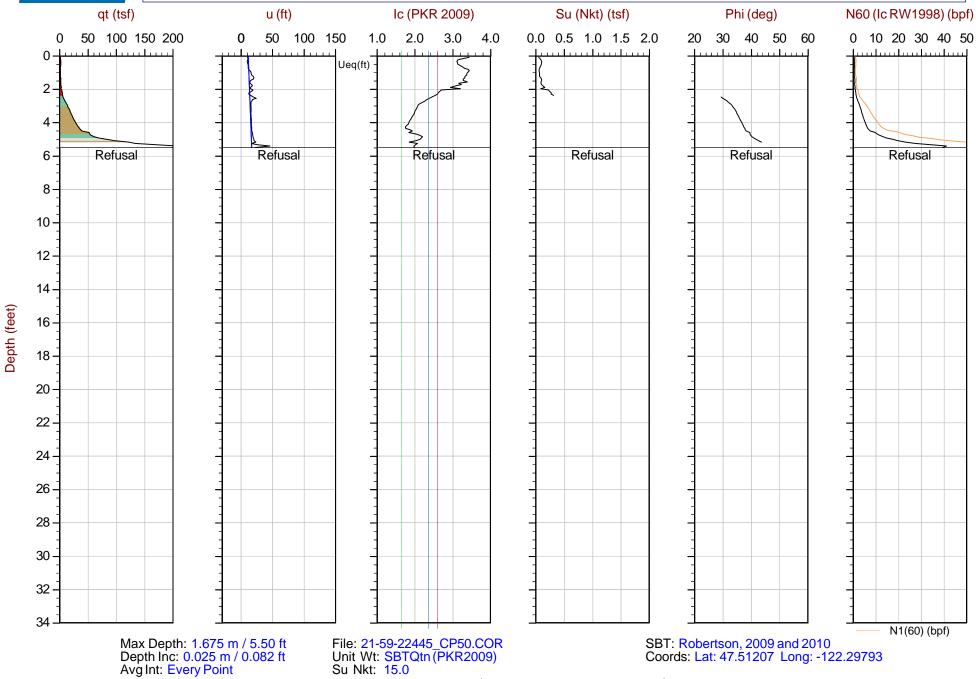


Job No: 21-59-22445 Date: 2021-07-23 15:21

Site: LDW Phase 3

Sounding: LDW21-GT50-GC

Cone: 681:T375F10U35



Su Nkt: 15.0 Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Coords: Lat: 47.51207 Long: -122.29793

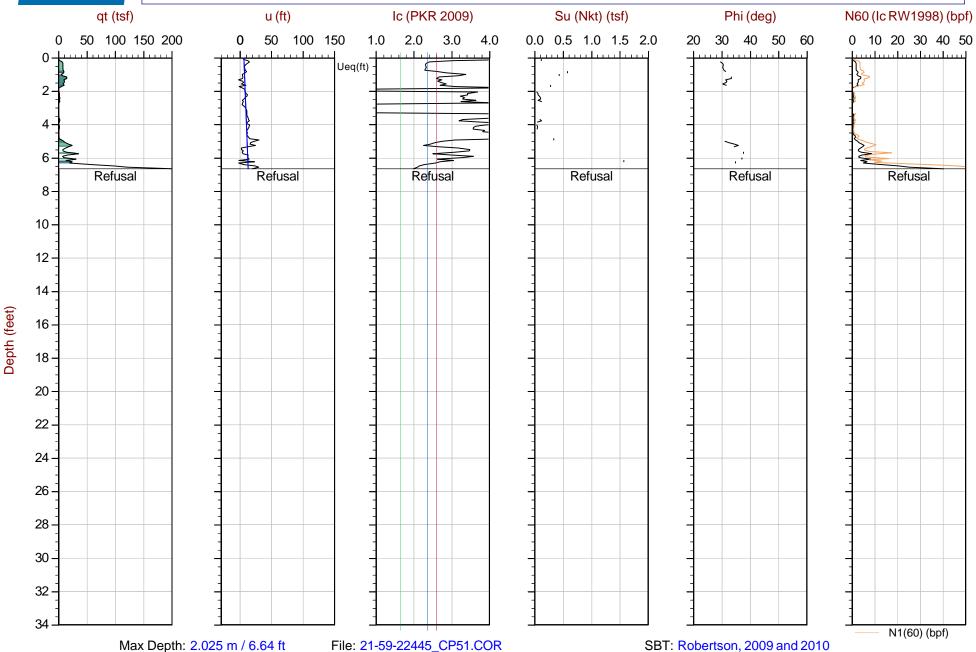


Job No: 21-59-22445 Date: 2021-07-26 19:23

Site: LDW Phase 3

Sounding: LDW21-GT51-GC

Cone: 681:T375F10U35



Max Depth: 2.025 m / 6.64 ft Depth Inc: 0.025 m / 0.082 ft Avg Int: Every Point

File: 21-59-22445\_CP51.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

Coords: Lat: 47.51218 Long: -122.29794

Hydrostatic Line

Equilibrium Pore Pressure (Ueq) Assumed Ueq Dissipation, Ueq achieved Dissipation, Ueq not achieved

The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.



Job No: 21-59-22445 Date: 2021-07-27 19:40

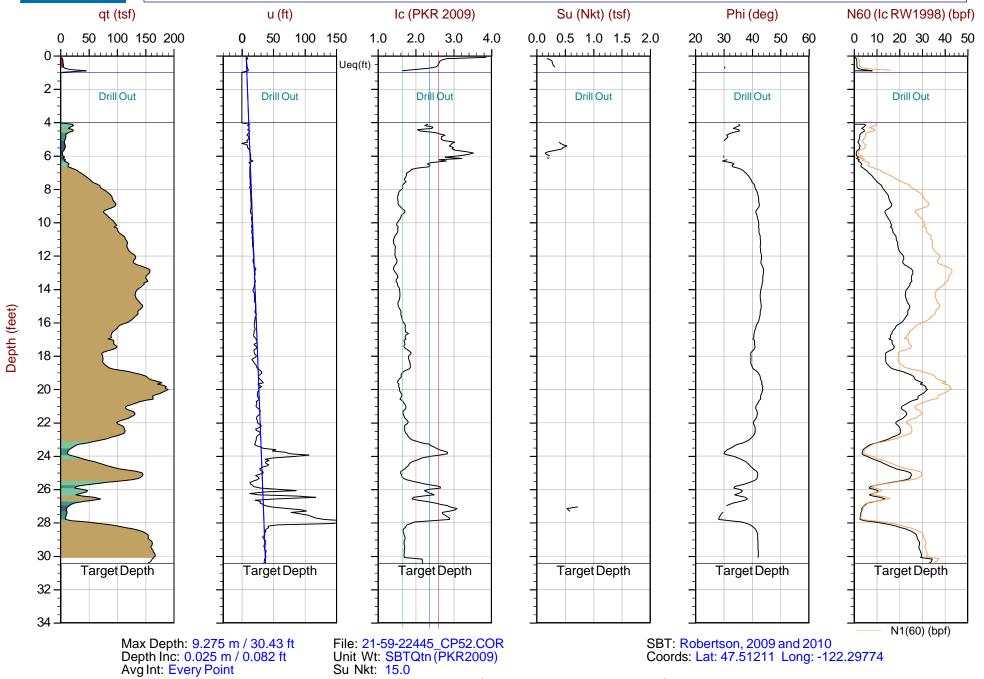
Site: LDW Phase 3

Sounding: LDW21-GT52-GC

Cone: 681:T375F10U35

Coords: Lat: 47.51211 Long: -122.29774

Hydrostatic Line



Equilibrium Pore Pressure (Ueq)
 Assumed Ueq
 Dissipation, Ueq achieved
 Dissipation, Ueq not achieved
 The reported coordinates were acquired from hand-held GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

Su Nkt: 15.0

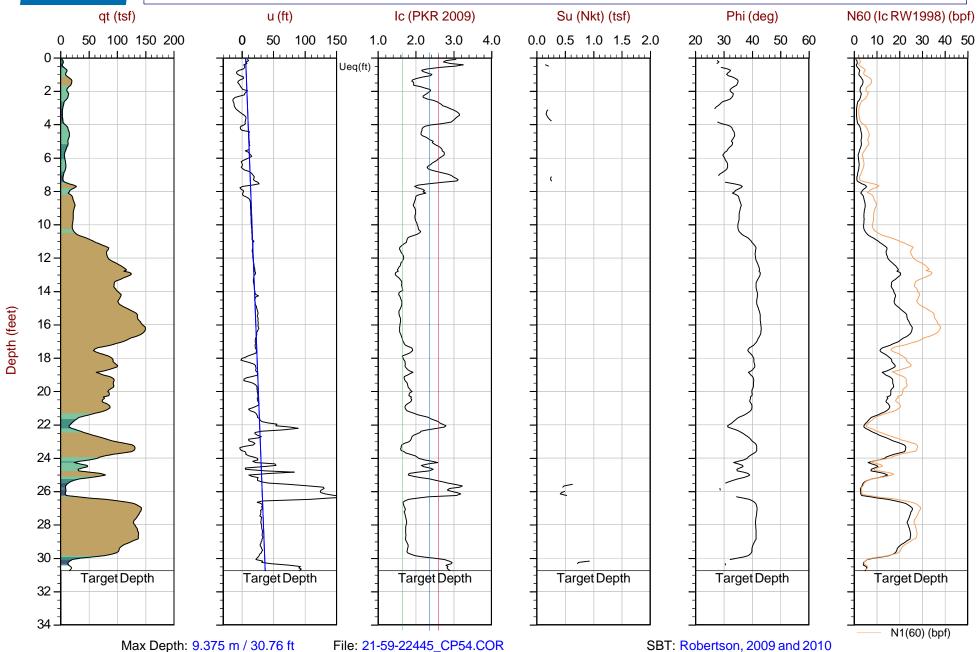


Job No: 21-59-22445 Date: 2021-07-27 18:31

Site: LDW Phase 3

Sounding: LDW21-GT54-GC

Cone: 681:T375F10U35



Max Depth: 9.375 m / 30.76 ftDepth Inc: 0.025 m / 0.082 ftAvg Int: Every Point

File: 21-59-22445\_CP54.COR Unit Wt: SBTQtn (PKR2009) Su Nkt: 15.0

Coords: Lat: 47.51197 Long: -122.29758

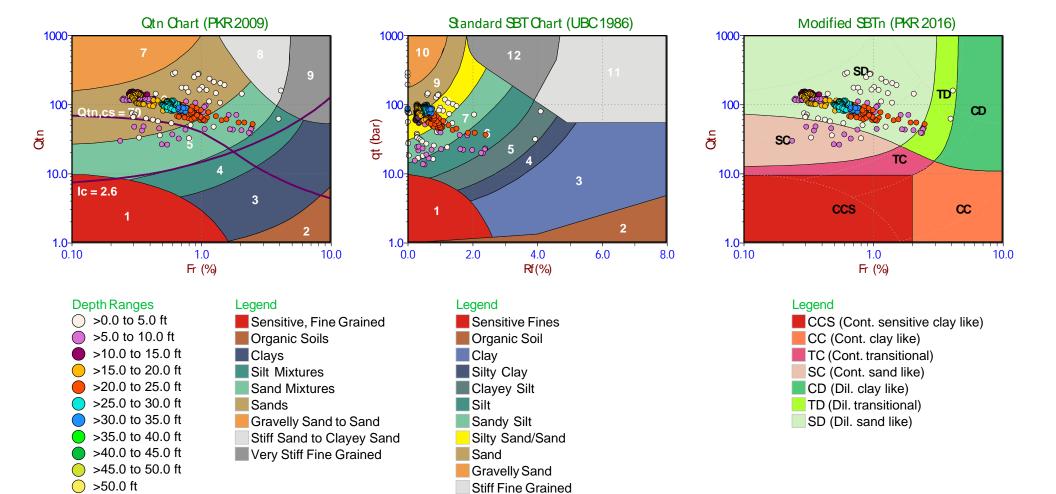
Soil Behavior Type (SBT) Scatter Plots





Job No: 21-59-22445 Date: 2021-07-22 17:30 Sounding: LDW21-GT06-GC Cone: 681:T375F10U35

Site: LDW Phase 3



Cemented Sand

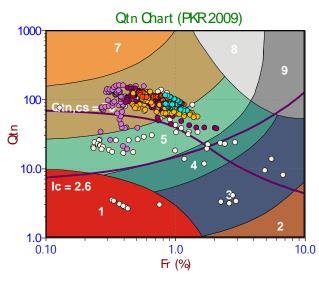


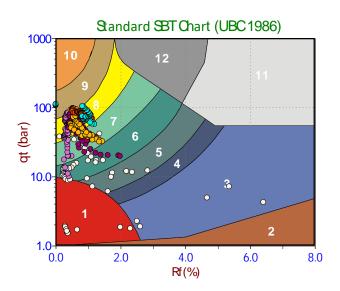
Job No: 21-59-22445

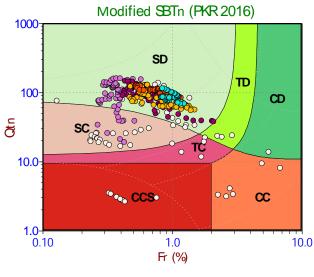
Date: 2021-07-08 14:11

Site: LDW Phase 3

Sounding: LDW21-GT14-GC Cone: 681:T375F10U35







# Depth Ranges >0.0 to 5.0 ft >5.0 to 10.0 ft >10.0 to 15.0 ft >15.0 to 20.0 ft >20.0 to 25.0 ft >25.0 to 30.0 ft >30.0 to 35.0 ft >35.0 to 40.0 ft >40.0 to 45.0 ft >50.0 ft



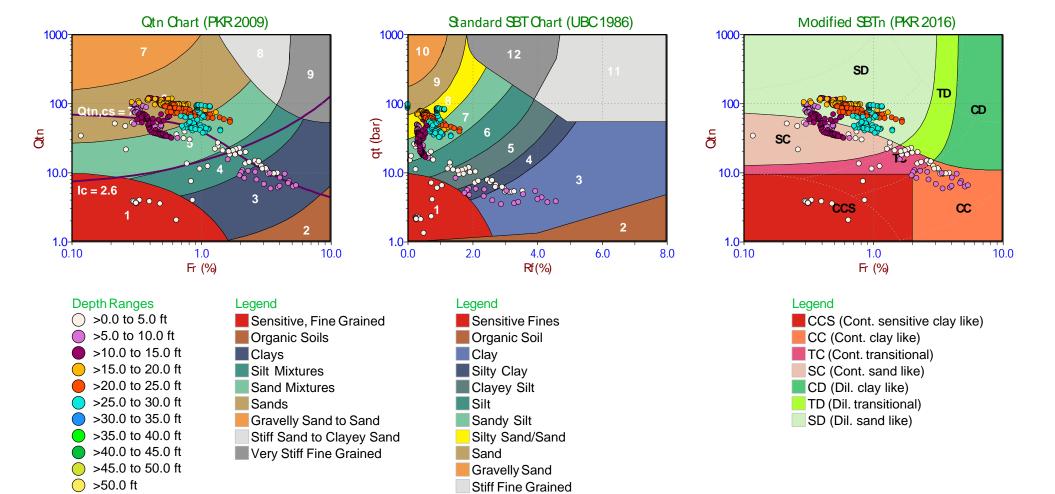






Job No: 21-59-22445 Date: 2021-07-08 16:24 Sounding: LDW21-GT16-GC Cone: 681:T375F10U35

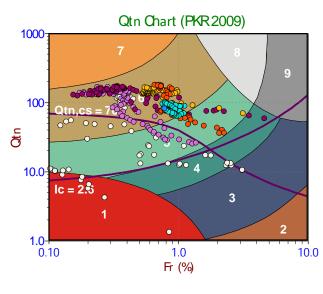
Site: LDW Phase 3

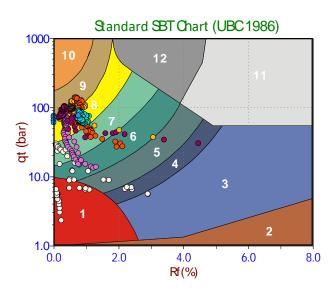


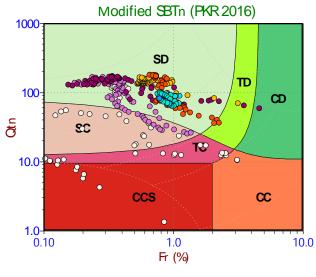
Cemented Sand



Job No: 21-59-22445 Date: 2021-07-12 19:15 Site: LDW Phase 3 Sounding: LDW21-GT17-GC Cone: 681:T375F10U35













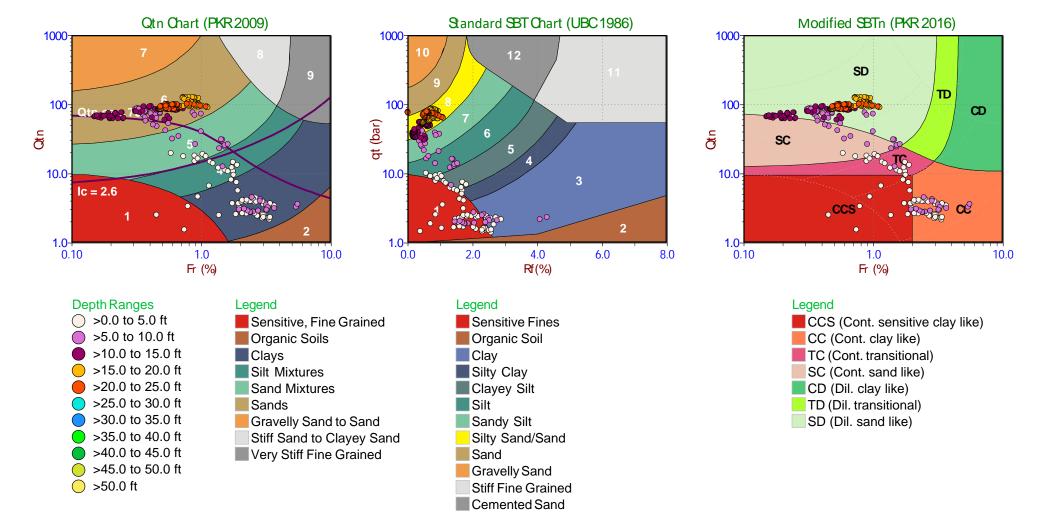


Job No: 21-59-22445

Date: 2021-07-16 09:40

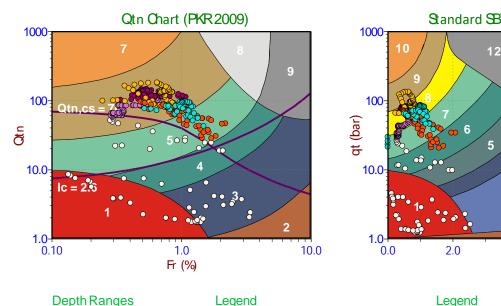
Site: LDW Phase 3

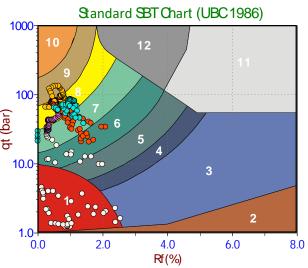
Sounding: LDW21-GT20-GC Cone: 681:T375F10U35

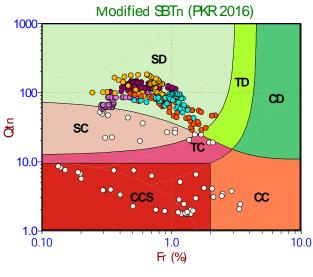




Job No: 21-59-22445 Date: 2021-07-13 19:06 Site: LDW Phase 3 Sounding: LDW21-GT22-GC Cone: 681:T375F10U35

















Job No: 21-59-22445 Date: 2021-07-16 08:30 Site: LDW Phase 3 Sounding: LDW21-GT27-GC Cone: 681:T375F10U35

Qtn Chart (PKR 2009) Standard SBT Chart (UBC 1986) Modified SBTn (PKR 2016) 1000 1000-1000 SD 9 TD 100 100 100 CD qt (bar) 鱼 g 10.0 10.0 Ic = 2.6CC 2 1.0 0.10 1.0 1.0 10.0 0.0 2.0 4.0 6.0 8.0 1.0 10.0 Fr (%) Rf(%) Fr (%) **Depth Ranges** Legend Legend Legend >0.0 to 5.0 ft Sensitive, Fine Grained Sensitive Fines CCS (Cont. sensitive clay like) >5.0 to 10.0 ft Organic Soils Organic Soil CC (Cont. clay like) >10.0 to 15.0 ft Clays Clav TC (Cont. transitional) >15.0 to 20.0 ft SC (Cont. sand like) Silt Mixtures Silty Clay >20.0 to 25.0 ft CD (Dil. clay like) Sand Mixtures Clayey Silt >25.0 to 30.0 ft Sands Silt TD (Dil. transitional) >30.0 to 35.0 ft Gravelly Sand to Sand SD (Dil. sand like) Sandy Silt >35.0 to 40.0 ft Stiff Sand to Clayey Sand Silty Sand/Sand >40.0 to 45.0 ft Very Stiff Fine Grained Sand >45.0 to 50.0 ft Gravelly Sand >50.0 ft Stiff Fine Grained

Cemented Sand

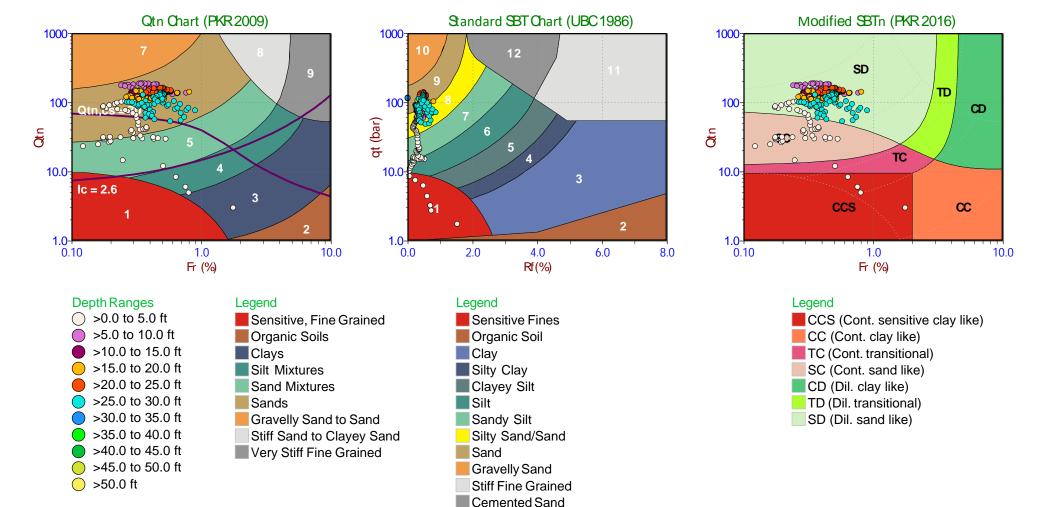


Job No: 21-59-22445

Date: 2021-07-21 15:09

Site: LDW Phase 3

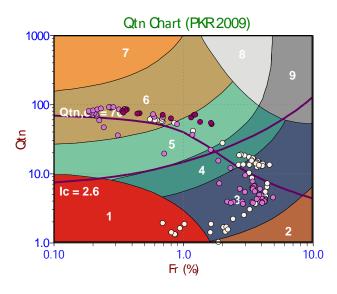
Sounding: LDW21-GT30-GC Cone: 681:T375F10U35

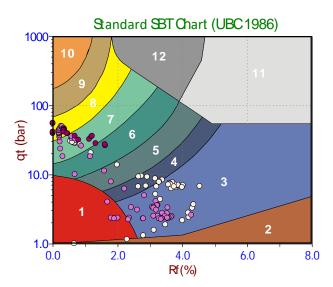


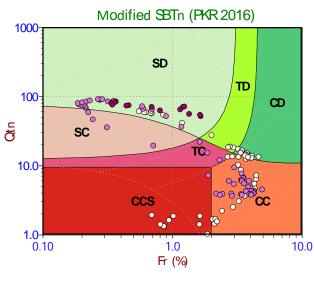


Job No: 21-59-22445 Date: 2021-07-09 10:35 Sounding: LDW21-GT31-GC Cone: 681:T375F10U35

Site: LDW Phase 3













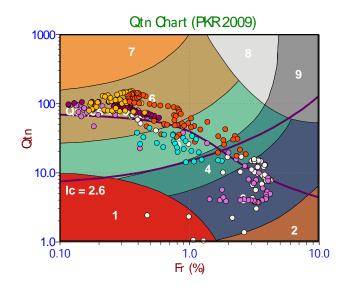


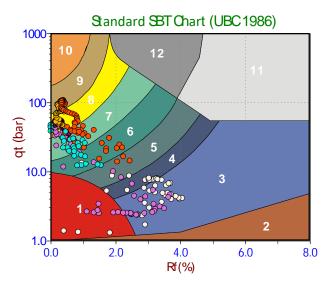


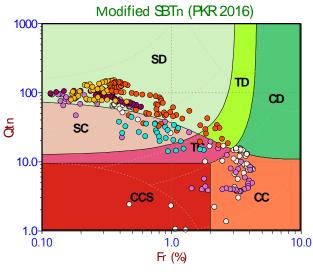
Job No: 21-59-22445 Date: 2021-07-13 17:56 Site: LDW Phase 3

Sounding: LDW21-GT31-GC-B

Cone: 681:T375F10U35











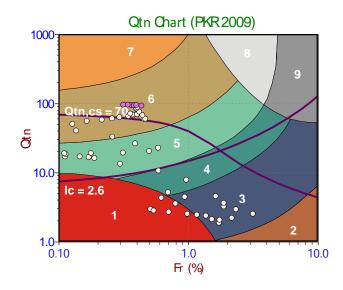


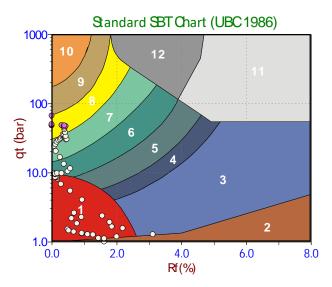


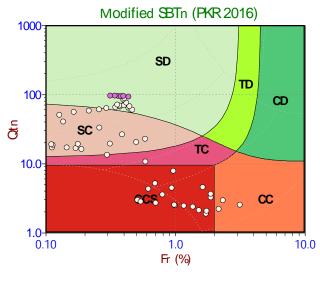
Job No: 21-59-22445 Date: 2021-07-09 11:18 Site: LDW Phase 3

Sounding: LDW21-GT32-GC

Cone: 681:T375F10U35















>50.0 ft

## Anchor QEA

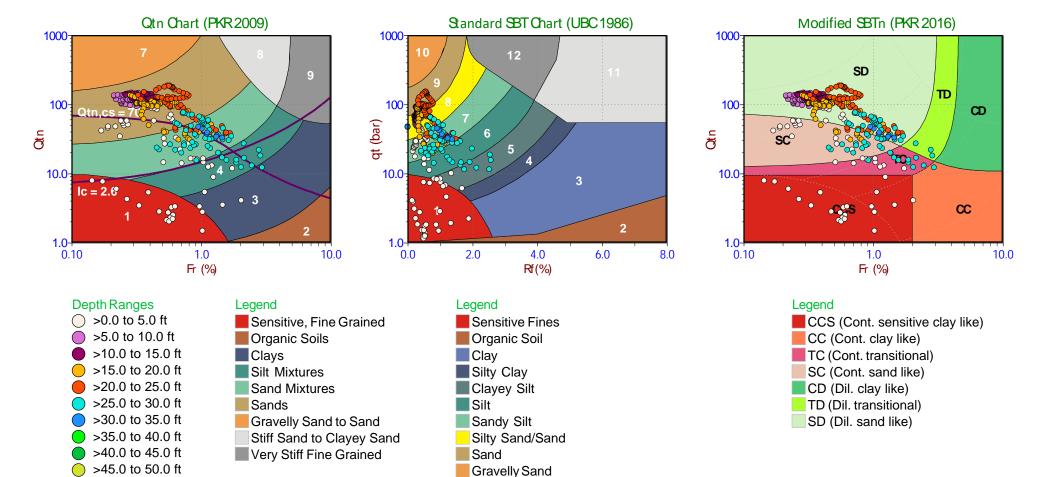
Job No: 21-59-22445

Date: 2021-07-21 13:24

Site: LDW Phase 3

Cone: 681:T375F10U35

Sounding: LDW21-GT32-GC-B



Stiff Fine Grained
Cemented Sand



>30.0 to 35.0 ft

>35.0 to 40.0 ft

>40.0 to 45.0 ft

>45.0 to 50.0 ft

>50.0 ft

## Anchor QEA

Gravelly Sand to Sand

Very Stiff Fine Grained

Stiff Sand to Clayey Sand

Job No: 21-59-22445 Date: 2021-07-21 14:17 Site: LDW Phase 3 Sounding: LDW21-GT34-GC Cone: 681:T375F10U35

SD (Dil. sand like)

Qtn Chart (PKR 2009) Standard SBT Chart (UBC 1986) Modified SBTn (PKR 2016) 1000 1000-1000 SD 9 TD 100 100 100 CD qt (bar) g 鱼 10.0-10.0 10.0-Ic = 2.63 **CCS** CC 2 1.0 0.10 1.0 1.0-1.0 10.0 0.0 2.0 4.0 6.0 8.0 1.0 10.0 Fr (%) Rf(%) Fr (%) **Depth Ranges** Legend Legend Legend >0.0 to 5.0 ft Sensitive, Fine Grained Sensitive Fines CCS (Cont. sensitive clay like) >5.0 to 10.0 ft Organic Soils Organic Soil CC (Cont. clay like) >10.0 to 15.0 ft Clays Clav TC (Cont. transitional) >15.0 to 20.0 ft Silt Mixtures Silty Clay SC (Cont. sand like) >20.0 to 25.0 ft CD (Dil. clay like) Sand Mixtures Clayey Silt >25.0 to 30.0 ft Sands Silt TD (Dil. transitional)

Sandy Silt

Sand

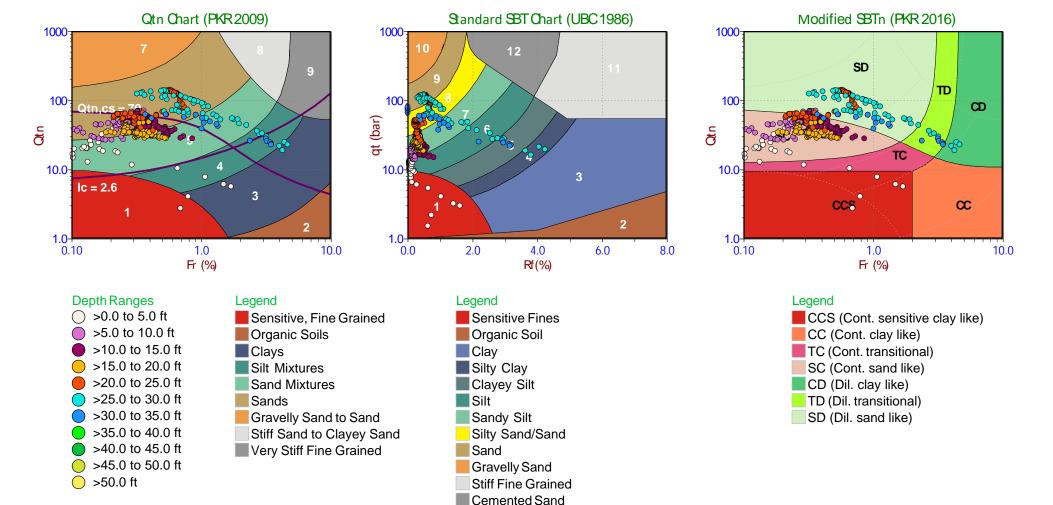
Silty Sand/Sand

Gravelly Sand

Stiff Fine Grained
Cemented Sand

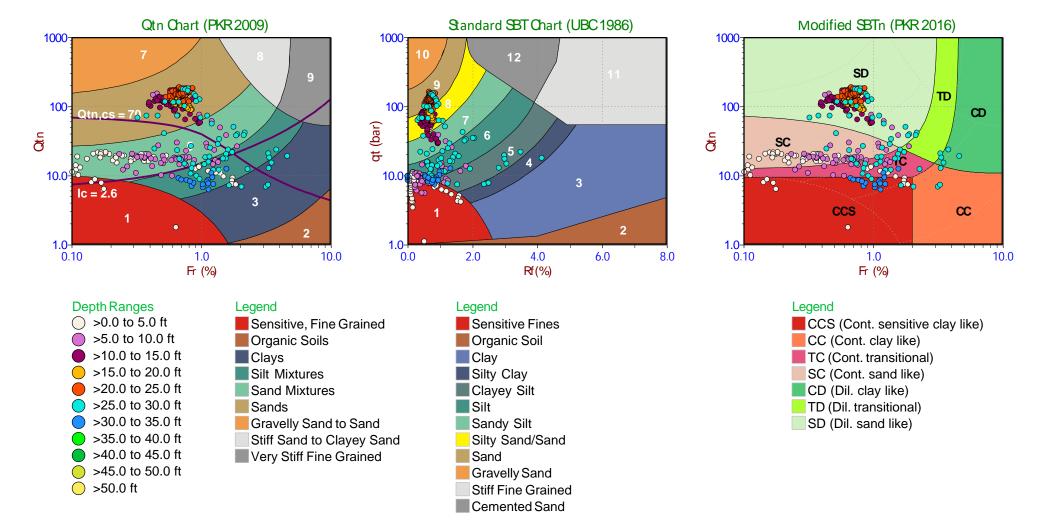


Job No: 21-59-22445 Date: 2021-07-19 13:58 Site: LDW Phase 3 Sounding: LDW21-GT40-GC Cone: 681:T375F10U35



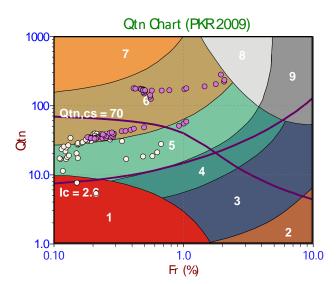


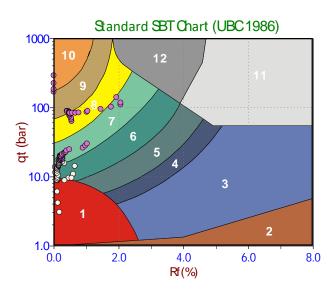
Job No: 21-59-22445 Date: 2021-07-28 18:24 Site: LDW Phase 3 Sounding: LDW21-GT45-GC Cone: 681:T375F10U35

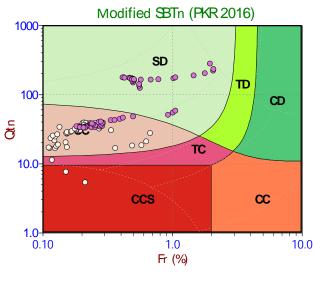




Job No: 21-59-22445 Date: 2021-07-26 09:49 Site: LDW Phase 3 Sounding: LDW21-GT46-GC Cone: 681:T375F10U35











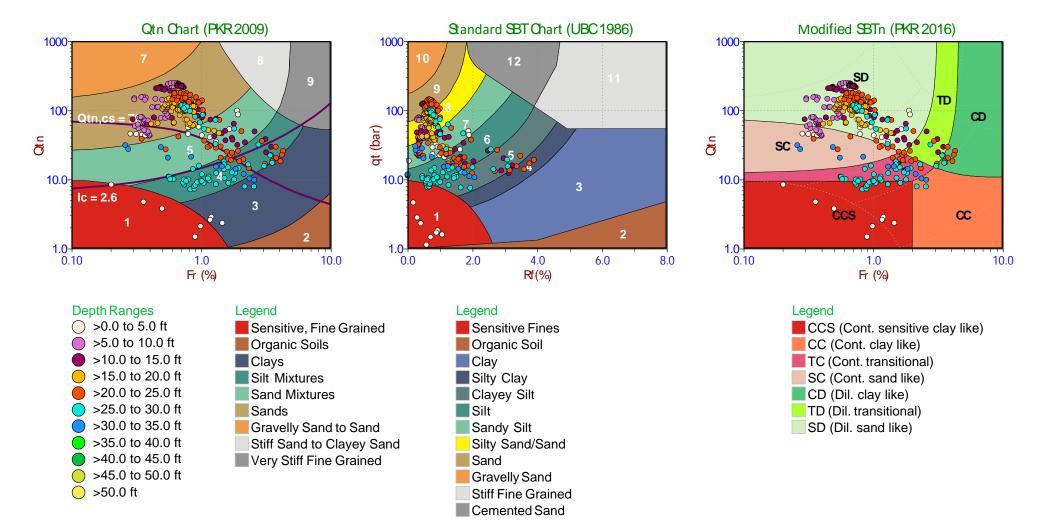






Job No: 21-59-22445 Date: 2021-07-27 20:39 Sounding: LDW21-GT47-GC Cone: 681:T375F10U35

Site: LDW Phase 3





>40.0 to 45.0 ft

>45.0 to 50.0 ft

>50.0 ft

## Anchor QEA

Very Stiff Fine Grained

Job No: 21-59-22445 Date: 2021-07-28 19:27 Site: LDW Phase 3 Sounding: LDW21-GT49-GC Cone: 681:T375F10U35

Qtn Chart (PKR 2009) Standard SBT Chart (UBC 1986) Modified SBTn (PKR 2016) 1000 1000-1000 9 TD 100 100 CD qt (bar) 鱼 g 10.0-10.0 10.0-Ic = 2.6 · P. ccs 3 CC 2 1.0 0.10 1.0 0.10 1.0 10.0 0.0 2.0 4.0 6.0 8.0 1.0 10.0 Fr (%) Rf(%) Fr (%) **Depth Ranges** Legend Legend Legend >0.0 to 5.0 ft Sensitive, Fine Grained Sensitive Fines CCS (Cont. sensitive clay like) >5.0 to 10.0 ft Organic Soils Organic Soil CC (Cont. clay like) >10.0 to 15.0 ft Clays Clav TC (Cont. transitional) >15.0 to 20.0 ft Silty Clay Silt Mixtures SC (Cont. sand like) >20.0 to 25.0 ft CD (Dil. clay like) Sand Mixtures Clayey Silt >25.0 to 30.0 ft Sands Silt TD (Dil. transitional) >30.0 to 35.0 ft Gravelly Sand to Sand SD (Dil. sand like) Sandy Silt >35.0 to 40.0 ft Stiff Sand to Clayey Sand Silty Sand/Sand

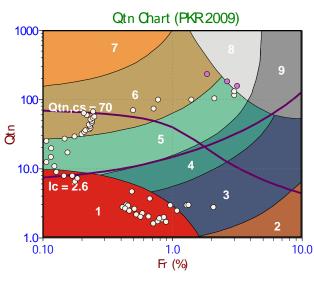
Sand

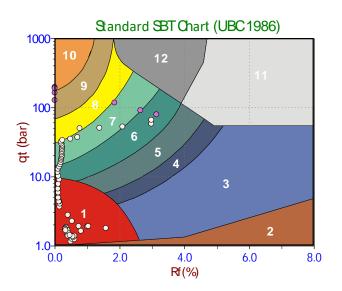
Gravelly Sand

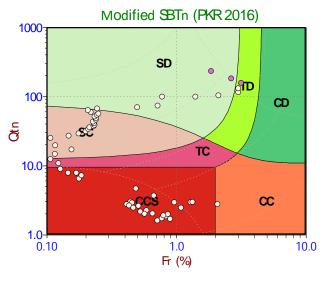
Stiff Fine Grained
Cemented Sand



Job No: 21-59-22445 Date: 2021-07-23 15:21 Site: LDW Phase 3 Sounding: LDW21-GT50-GC Cone: 681:T375F10U35







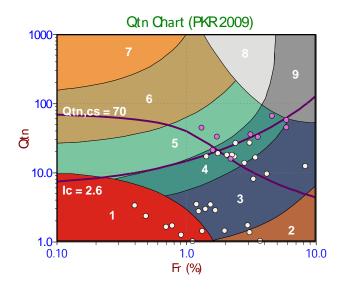


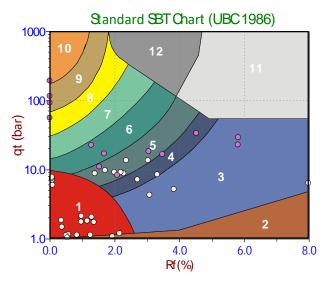


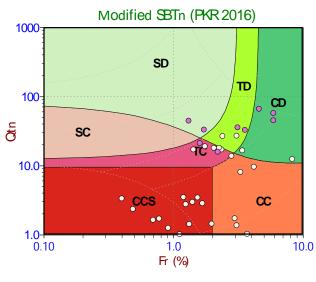




Job No: 21-59-22445 Date: 2021-07-26 19:23 Site: LDW Phase 3 Sounding: LDW21-GT51-GC Cone: 681:T375F10U35







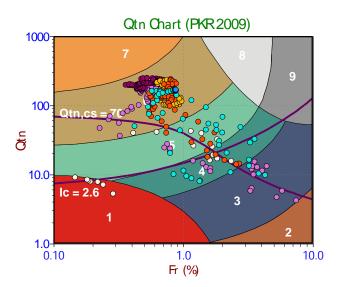


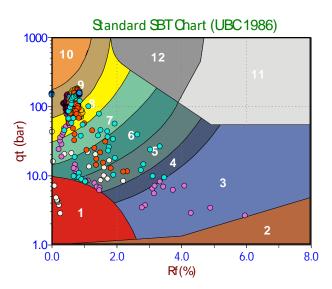


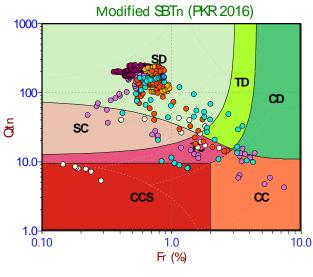




Job No: 21-59-22445 Date: 2021-07-27 19:40 Site: LDW Phase 3 Sounding: LDW21-GT52-GC Cone: 681:T375F10U35









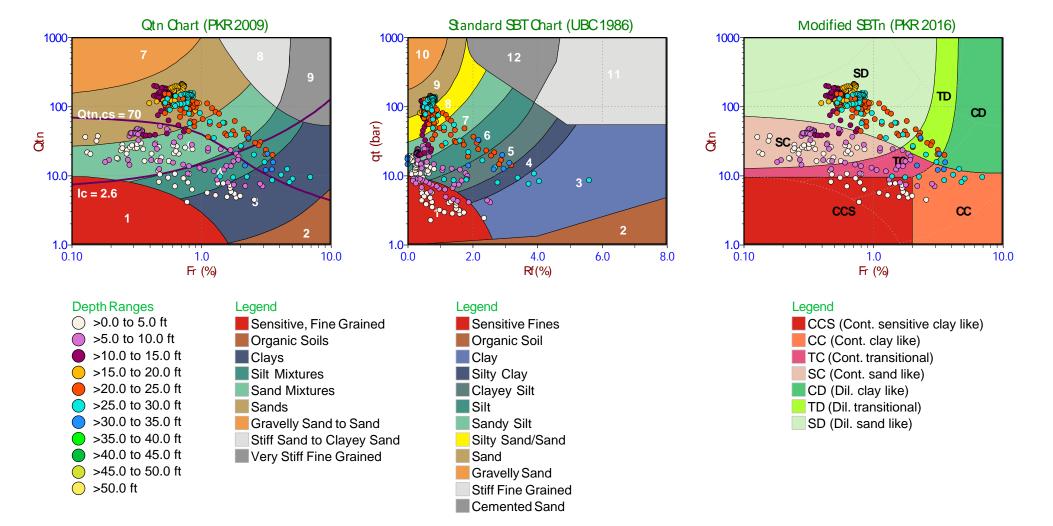






Job No: 21-59-22445 Date: 2021-07-27 18:31 Site: LDW Phase 3

Sounding: LDW21-GT54-GC Cone: 681:T375F10U35



Ball Full Flow Cone Penetration Test Summary and Plots





Job No: 21-59-22445
Client: Anchor QEA
Project: LDW Phase 3
Start Date: 06-Jul-2021
End Date: 29-Jul-2021

BALL FULL FLOW PENETRATION TEST SUMMARY													
Sounding ID	File Name	Date	Cone	Cone Area (cm²)	Ball Area (cm²)	Final Depth (ft)	Cycling Conducted	Latitude <sup>1</sup> (deg)	Longitude <sup>1</sup> (deg)	Refer to Notation Number			
LDW21-GT01-FFP	21-59-22445_BP01	14-Jul-2021	681:T375F10U35	15	150	4.0	YES	47.53230	-122.31937				
LDW21-GT03-FFP	21-59-22445_BP03	14-Jul-2021	681:T375F10U35	15	150	5.9	YES	47.52757	-122.31136				
LDW21-GT09-FFP	21-59-22445_BP09	14-Jul-2021	681:T375F10U35	15	150	12.1	YES			2			
LDW21-GT11-FFP	21-59-22445_BP11	16-Jul-2021	681:T375F10U35	15	150	9.4	YES	47.52623	-122.30963				
LDW21-GT26-FFP	21-59-22445_BP26	16-Jul-2021	681:T375F10U35	15	150	4.0	YES	47.52150	-122.30687				
LDW21-GT30-31-FFP	21-59-22445_BP30-31	21-Jul-2021	681:T375F10U35	15	150	5.2	YES	47.52051	-122.30581				
LDW21-GT32-34-FFP	21-59-22445_BP32-34	21-Jul-2021	681:T375F10U35	15	150	4.0	YES	47.51999	-122.30585				

<sup>1.</sup> Coordinates were provided by client

<sup>2.</sup> Coordinates currently not available. Coordinates will be provided by client at a later date

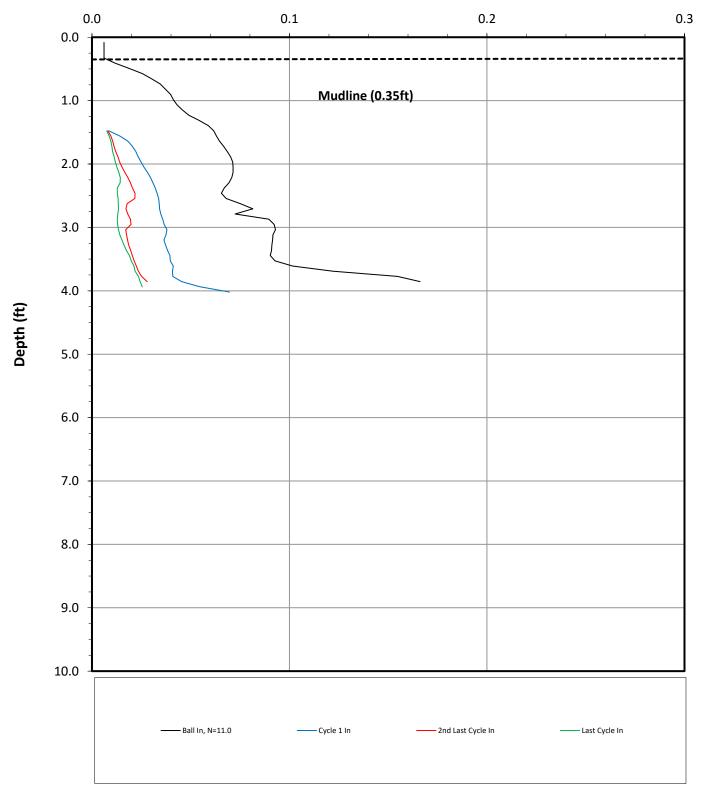


Sounding ID: LDW21-GT01-FFP Sounding Date: July 14, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.5322979 Long (deg): -122.3193655

### **Flow Penetrometer Undrained Strength**



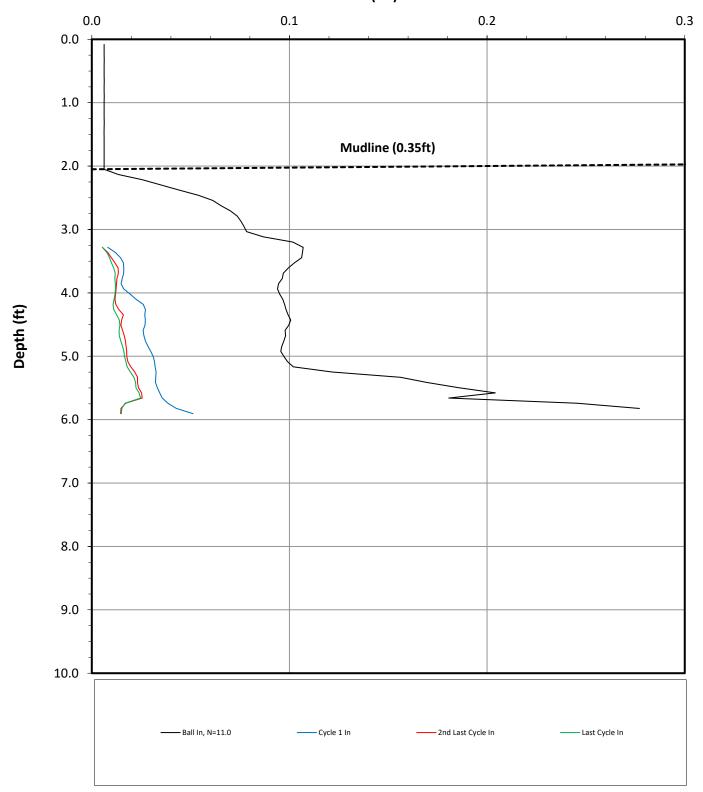


Sounding ID: LDW21-GT03-FFP Sounding Date: July 14, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.5275718 Long (deg): -122.3113628

### **Flow Penetrometer Undrained Strength**



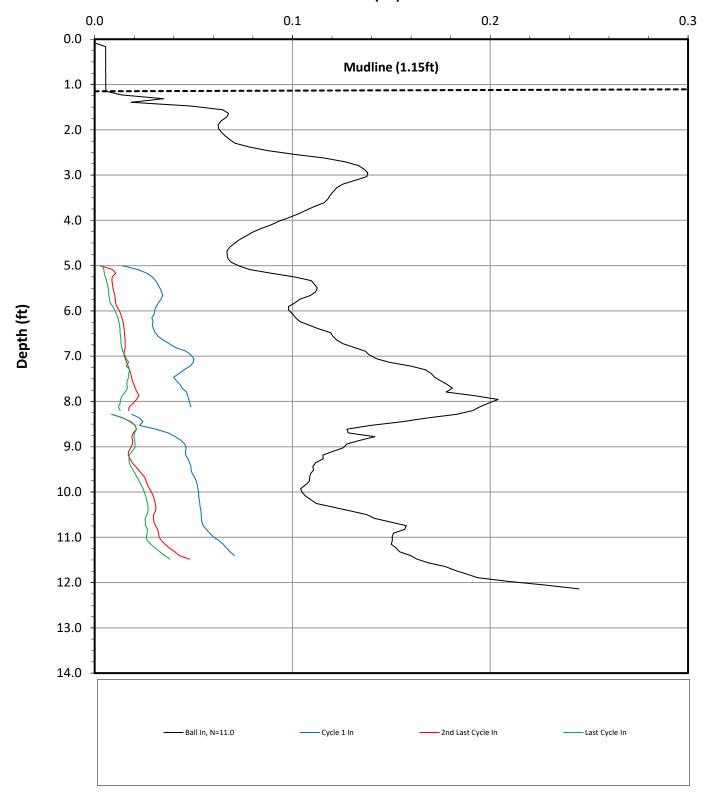


Sounding ID: LDW21-GT09-FFP Sounding Date: July 14, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): Long (deg):

### Flow Penetrometer Undrained Strength



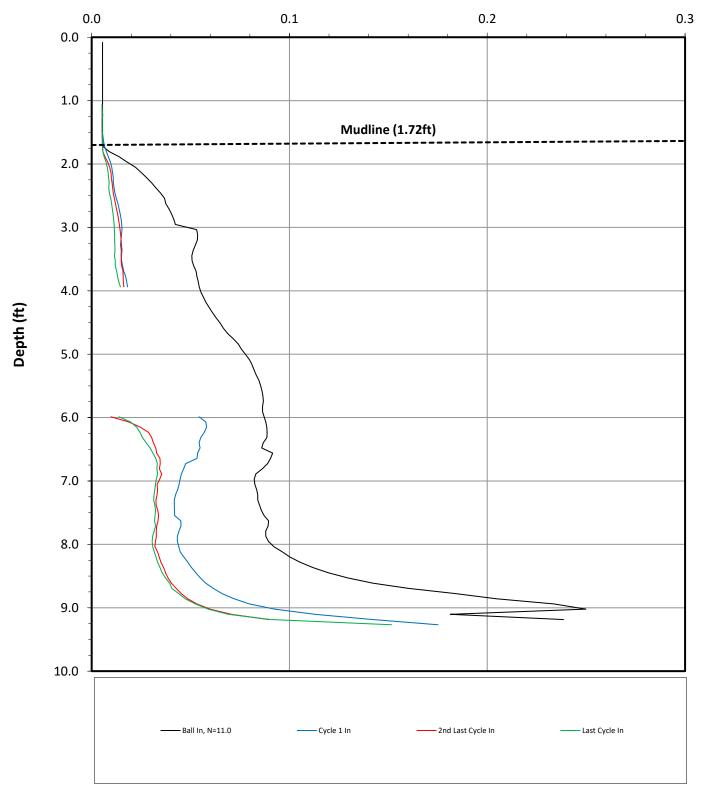


Sounding ID: LDW21-GT11-FFP Sounding Date: July 16, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.5262259 Long (deg): -122.3096315

### **Flow Penetrometer Undrained Strength**



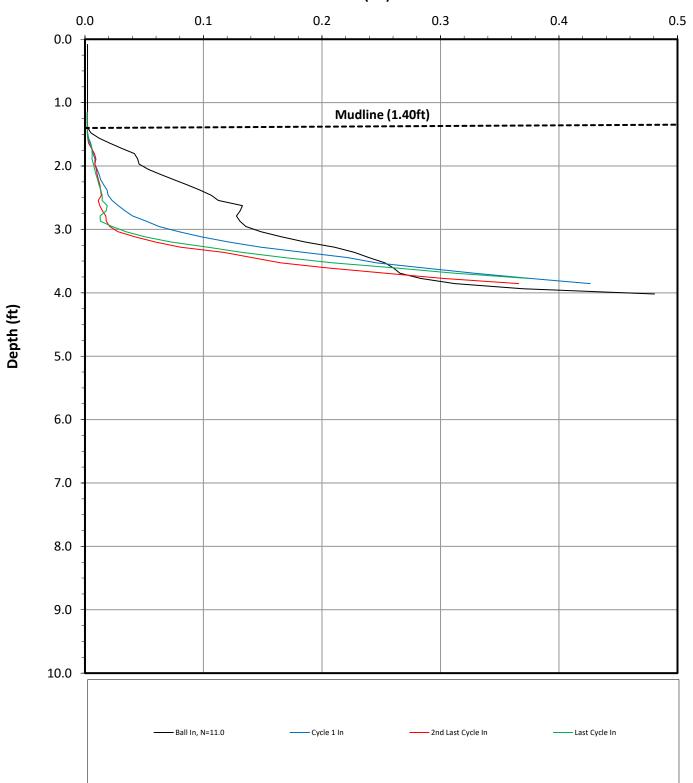


Sounding ID: LDW21-GT26-FFP Sounding Date: July 16, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.5215043 Long (deg): -122.3068749

### Flow Penetrometer Undrained Strength



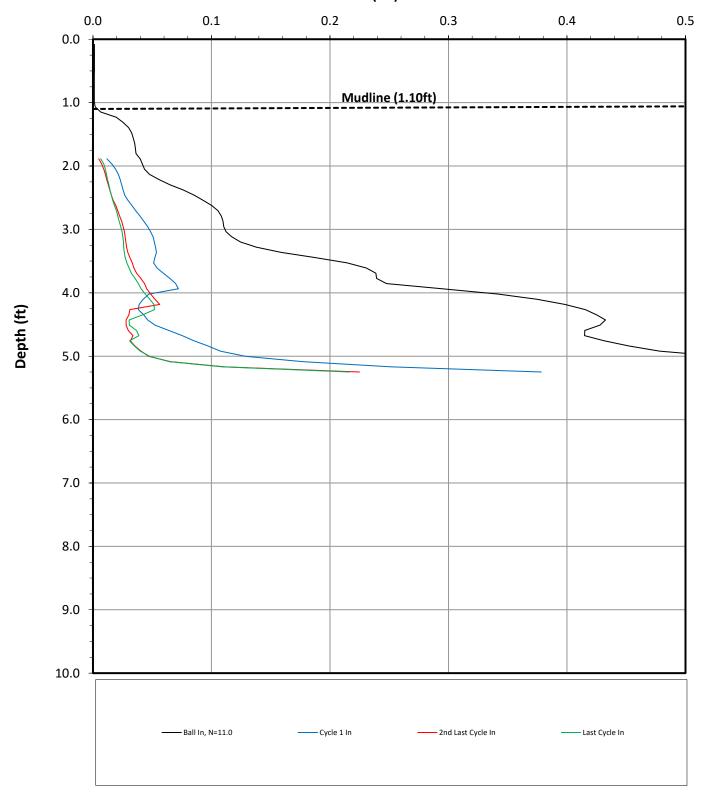


Sounding ID: LDW21-GT30-31-FFP Sounding Date: July 21, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.520508 Long (deg): -122.3058147

### Flow Penetrometer Undrained Strength



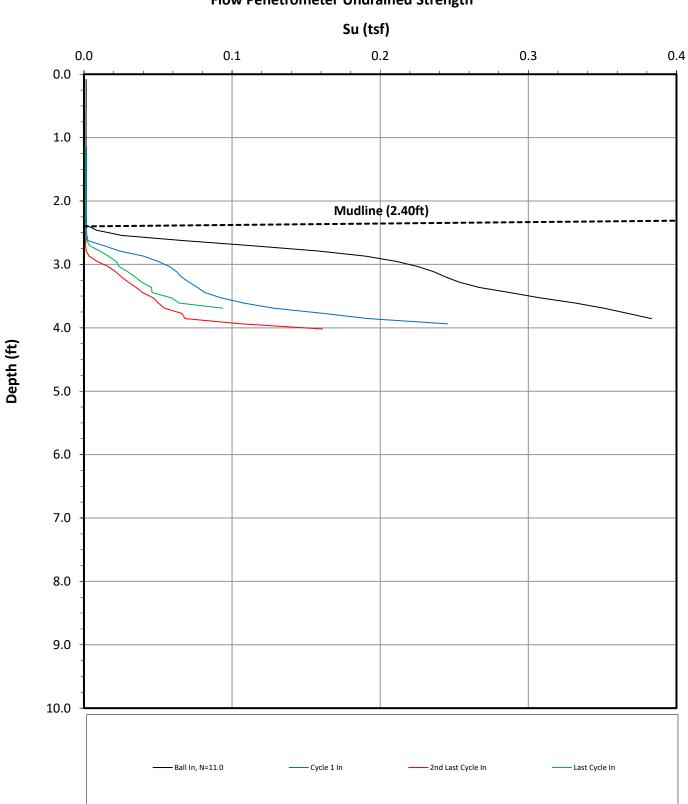


Sounding ID: LDW21-GT32-34-FFP Sounding Date: July 21, 2021

Coordinate System: WGS 84 Lat/Long

Lat (deg): 47.5199896 Long (deg): -122.3058465

### Flow Penetrometer Undrained Strength



Electronic Field Vane Shear Test Profile Summary and Results





Job Number: 21-59-22445
Client: Anchor QEA
Project: LDW Phase 3
Start Date: 06-Jul-2021
End Date: 29-Jul-2021

#### **ELECTRIC FIELD VANE SHEAR TEST SUMMARY**

Sounding ID	File Name	Adjacent CPT Sounding ID	Rig	Date From	Date To	Latitude <sup>1</sup>	Longitude <sup>1</sup>	Refer to Notation Number
LDW21-GT04-GV	21-59-22445_VST04	NONE	C05-023	12-Jul-2021	12-Jul-2021			2
LDW21-GT20-GV	21-59-22445_VST20	NONE	C05-023	19-Jul-2021	19-Jul-2021			2
LDW21-GT-26-GV	21-59-22445_VST26	NONE	C05-023	07-Jul-2021	07-Jul-2021	47.521510	-122.306837	
LDW21-GT-26-GV-B	21-59-22445_VST26B	NONE	C05-023	07-Jul-2021	07-Jul-2021	47.521522	-122.306805	
LDW21-GT43-GV	21-59-22445_VST43	NONE	C05-023	22-Jul-2021	22-Jul-2021	47.511105	-122.303294	

- 1. Coordinates were provided by client
- 2. Coordinates currently not available. Corrdiantes will be proviced by client at a later date
- 3. Test depth reference depth below mudline.
- 4. All vane tests were completed from the floating barge platform. The vane test results were affected by barge movement from local waves, local vessel traffic and river flow. Additionally, the vane results were susceptible to elevation charge from either rising or falling tide. Over the course of a vane test the barge would gain/lose approximately 1"-4" of elevation due to tidal effects.



 Job Number:
 21-59-22445

 Client:
 Anchor QEA

 Project:
 LDW Phase 3

 Start Date:
 06-Jul-2021

 End Date:
 29-Jul-2021

	ELECTRIC FIELD VANE SHEAR TEST RESULTS																				
Sounding ID	File Name	Date	Load Cell Serial Number	Load Cell Location	Casing/Drillout Depth (ft)	Test Depth <sup>1</sup> (ft)	Vane Diameter D (mm)	Vane Height H (mm)	Top Taper Angle i <sub>T</sub> (deg)	Bottom Taper Angle i <sub>B</sub> (deg)	Vane Factor (kPa/Nm)	Peak Torque (Nm)	Remolded Torque (Nm)	Peak Stress (tsf)	Remolded Stress (tsf)	Peak Frictional Stress (tsf)	Remolded Frictional Stress (tsf)	Su Peak (tsf)	Su Remolded (tsf)	Sensitivity	Refer to Notation Number
LDW21-GT04-GV	21-59-22445_VST04	12-Jul-2021	AVLC009	Surface	N/A	1.50	75	150	45	45	0.6106	10.28		0.07		0.003		0.06			
LDW21-GT04-GV	21-59-22445_VST04	12-Jul-2021	AVLC009	Surface	N/A	2.50	75	150	45	45	0.6106	16.52	2.69	0.11	0.02	0.001	0.002	0.10	0.02	6.83	
LDW21-GT20-GV	21-59-22445_VST20	19-Jul-2021	AVLC009	Surface	N/A	2.50	75	150	45	45	0.6106	67.49	5.27	0.43	0.03	0.003	0.002	0.43	0.03	13.40	
LDW21-GT20-GV	21-59-22445_VST20	19-Jul-2021	AVLC009	Surface	N/A	4.50	75	150	45	45	0.6106	13.50	3.49	0.09	0.02	0.002	0.003	0.08	0.02	4.26	
LDW21-GT-26-GV	21-59-22445_VST26	07-Jul-2021	AVLC013	Surface	N/A	1.17	60	120	45	45	1.1926	3.04	0.47	0.04	0.01	0.004	0.004	0.03	0.00	15.56	
LDW21-GT-26-GV	21-59-22445_VST26	07-Jul-2021	AVLC013	Surface	N/A	3.17	60	120	45	45	1.1926	6.79	2.51	0.08	0.03	0.007	0.008	0.08	0.02	3.36	
LDW21-GT-26-GV	21-59-22445_VST26	07-Jul-2021	AVLC013	Surface	N/A	4.42	60	120	45	45	1.1926	4.23		0.05		0.004		0.05			
LDW21-GT-26-GV-B	21-59-22445_VST26B	07-Jul-2021	AVLC013	Surface	N/A	1.17	75	150	45	45	0.6106	14.96		0.10		0.003		0.09			
LDW21-GT43-GV	21-59-22445_VST43	22-Jul-2021	AVLC009	Surface	N/A	1.08	75	150	45	45	0.6106	43.50	6.22	0.28	0.04	0.003	0.001	0.27	0.04	7.03	
LDW21-GT43-GV	21-59-22445_VST43	22-Jul-2021	AVLC009	Surface	N/A	3.17	75	150	45	45	0.6106	72.29		0.46		0.003		0.46			

<sup>1.</sup> Test depths are referenced to the middle of the vane.



Job Number: 21-59-22445
Client: Anchor QEA
Project: LDW Phase 3
Start Date: 06-Jul-2021
End Date: 29-Jul-2021

### **ELECTRIC FIELD VANE SHEAR TEST TIMING**

Sounding ID	Date	Test Depth <sup>1</sup> (ft)	Vane Insertion Time (HH:mm)	Peak Test Start Time (HH:mm)	Insertion to Start Interval (min)	Start to Failure Interval (sec)	Peak Test Avg Rate (deg/sec)	Remolding Completion Time (HH:mm)	Remold Test Start Time (HH:mm)	Remolding to Start Interval (min)	Remold Test Avg Rate (deg/sec)	Refer to Notation Number
LDW21-GT04-GV	12-Jul-2021	1.50	17:27	17:27	1	150	0.12					
LDW21-GT04-GV	12-Jul-2021	2.50	18:21	18:23	16	357	0.11	18:32	18:33	27	0.11	
LDW21-GT20-GV	19-Jul-2021	2.50	12:15	12:16	1	686	0.12	12:34	12:35	20	0.11	
LDW21-GT20-GV	19-Jul-2021	4.50	12:49	12:50	36	307	0.11	12:57	12:58	43	0.11	
LDW21-GT-26-GV	07-Jul-2021	1.17	14:08	14:10	2	210	0.08	14:22	14:23	16	0.09	
LDW21-GT-26-GV	07-Jul-2021	3.17	14:33	14:35	28	492	0.08	14:54	14:55	47	0.08	
LDW21-GT-26-GV	07-Jul-2021	4.42	15:08	15:11	63	269	0.08					
LDW21-GT-26-GV-B	07-Jul-2021	1.17	15:57	15:58	1	303	0.10					
LDW21-GT43-GV	22-Jul-2021	1.08	16:06	16:10	4	330	0.12	16:21	16:22	16	0.13	
LDW21-GT43-GV	22-Jul-2021	3.17	16:35	16:36	31	400	0.12					

<sup>1.</sup> Test depths are referenced to the middle of the vane.

**Electronic Field Vane Shear Test Plots** 





Job Number: 21-59-22445

Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT04-GV Test Date: 12-Jul-2021 17:27

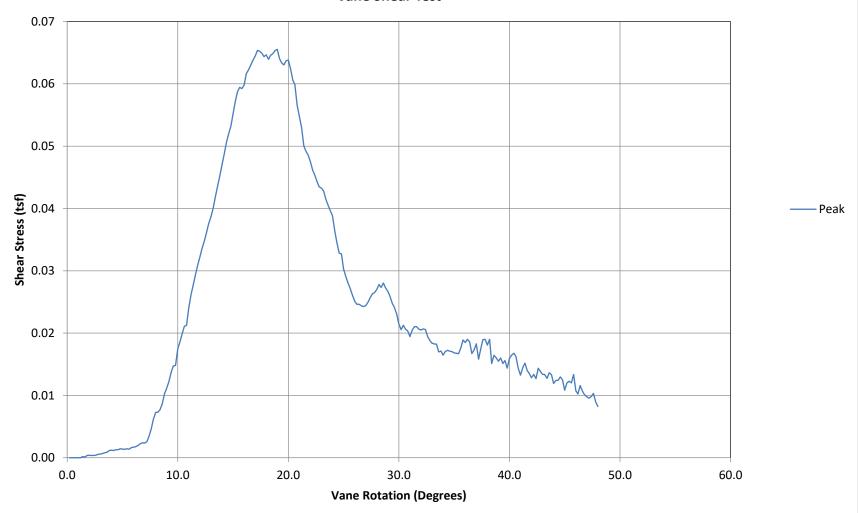
Test Depth (ft): 1.50 Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 0 Longitude: 0







0.00

0.0

10.0

20.0

Job Number: 21-59-22445

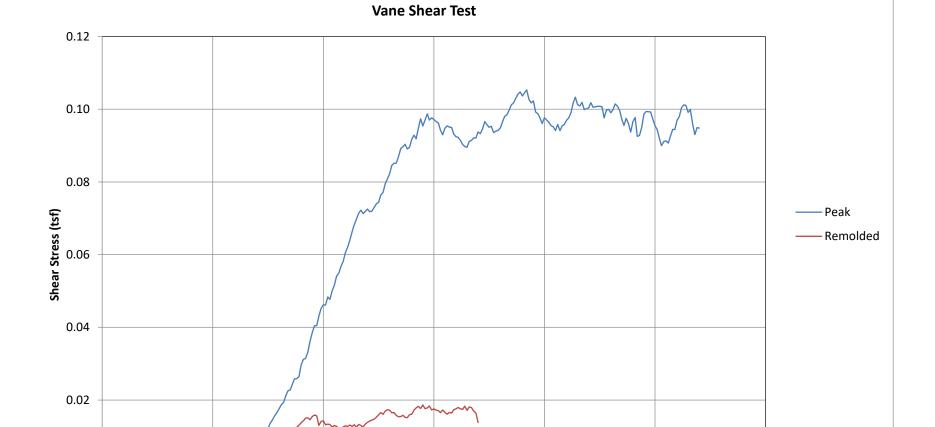
Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT04-GV Test Date: 12-Jul-2021 18:23 Test Depth (ft): 2.50

Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 0 Longitude: 0



30.0

Vane Rotation (Degrees)

40.0

50.0

60.0



Job Number: 21-59-22445

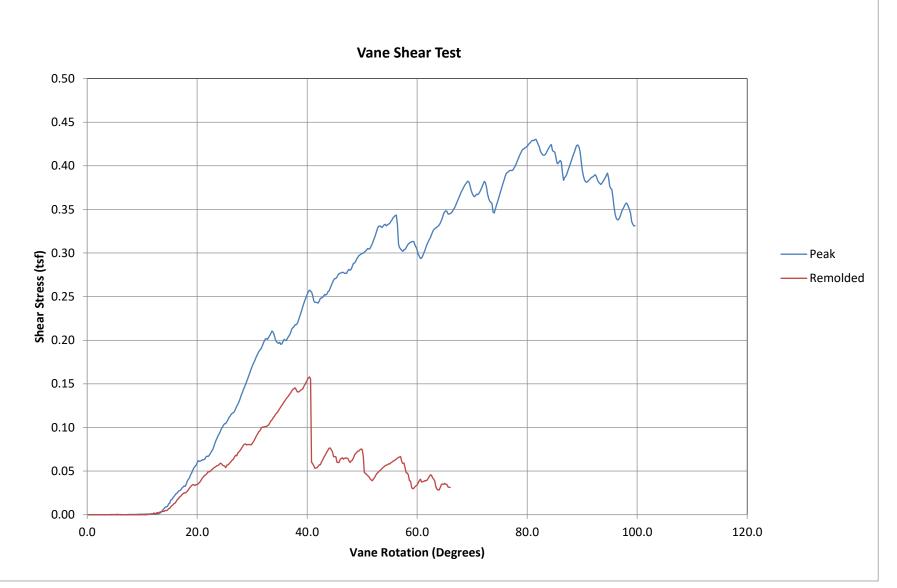
Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT20-GV Test Date: 19-Jul-2021 12:16 Test Depth (ft): 2.50

Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 0 Longitude: 0





Job Number: 21-59-22445 Client: Anchor QEA

Project: LDW Phase 3
Sounding: LDW21-GT20-GV

Test Date: 19-Jul-2021 12:50

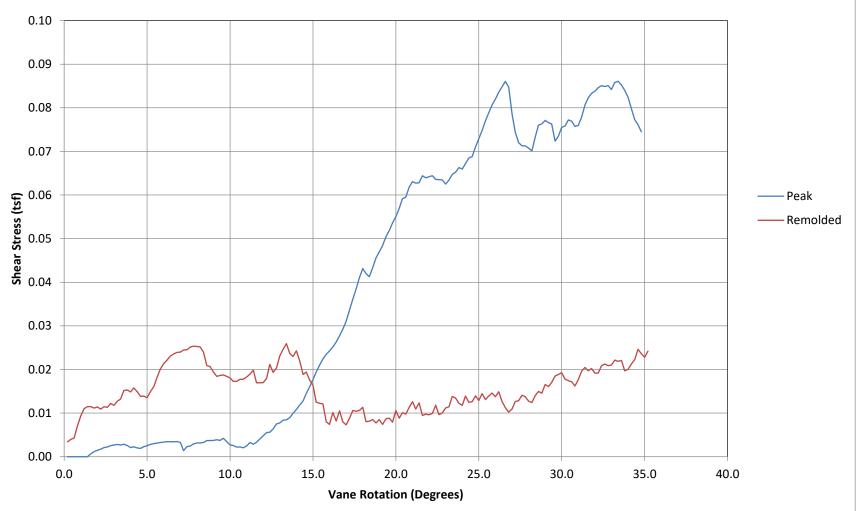
Test Depth (ft): 4.50 Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 0 Longitude: 0







Job Number: 21-59-22445

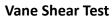
Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT-26-GV Test Date: 07-Jul-2021 14:10

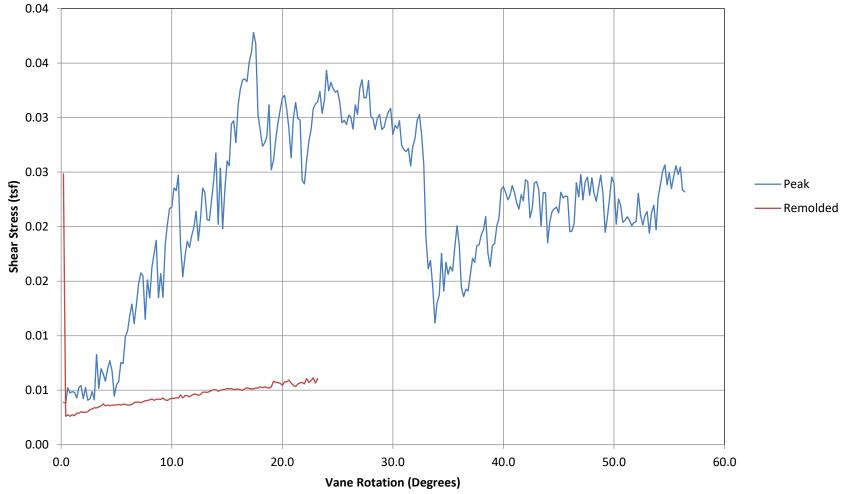
Test Depth (ft): 1.17 Vane Type: Adara solid double tapered 60 x 120

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 47.5215097 Longitude: -122.3068371







Job Number: 21-59-22445 Client: Anchor QEA

Project: LDW Phase 3
Sounding: LDW21-GT-26-GV

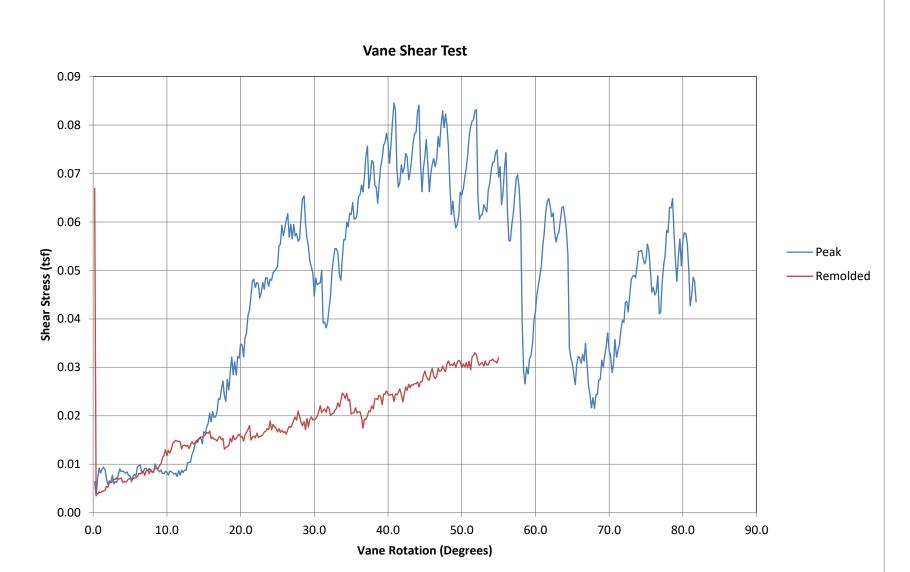
Test Date: 07-Jul-2021 14:35

Test Depth (ft): 3.17 Vane Type: Adara solid double tapered 60 x 120

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 47.5215097 Longitude: -122.3068371





Job Number: 21-59-22445

Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT-26-GV Test Date: 07-Jul-2021 15:11

Test Depth (ft): 4.42 Vane Type: Adara solid double tapered 60 x 120

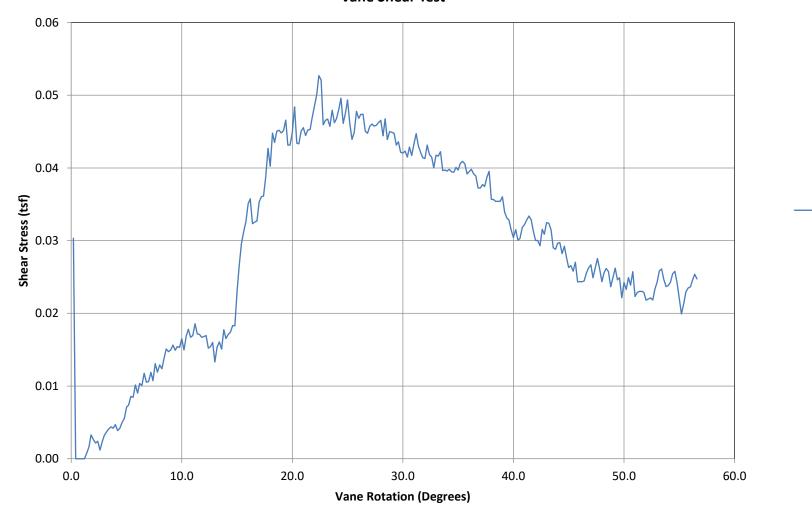
mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Peak

Latitude: 47.5215097 Longitude: -122.3068371

#### **Vane Shear Test**





Job Number: 21-59-22445

Client: Anchor QEA Project: LDW Phase 3

Sounding: LDW21-GT-26-GV-B

Test Date: 07-Jul-2021 15:58

Test Depth (ft): 1.17

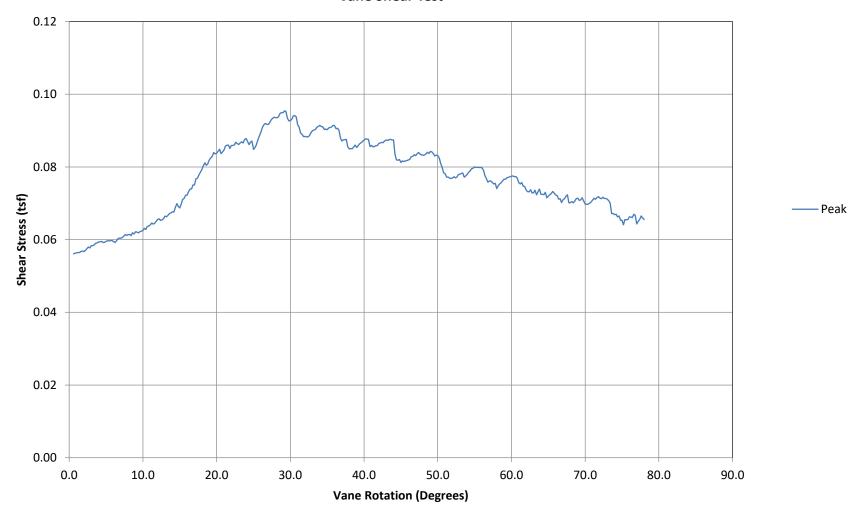
Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 47.5215216 Longitude: -122.3068046







Job Number: 21-59-22445 Client: Anchor QEA

Project: LDW Phase 3
Sounding: LDW21-GT43-GV

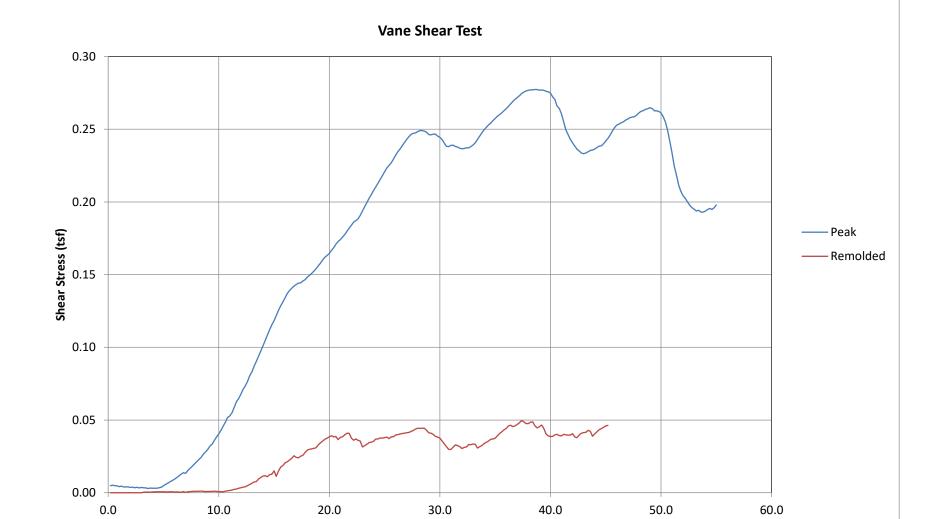
Test Date: 22-Jul-2021 16:10

Test Depth (ft): 1.08 Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 47.5111048 Longitude: -122.3032936



Vane Rotation (Degrees)



Job Number: 21-59-22445

Client: Anchor QEA Project: LDW Phase 3 Sounding: LDW21-GT43-GV Test Date: 22-Jul-2021 16:36

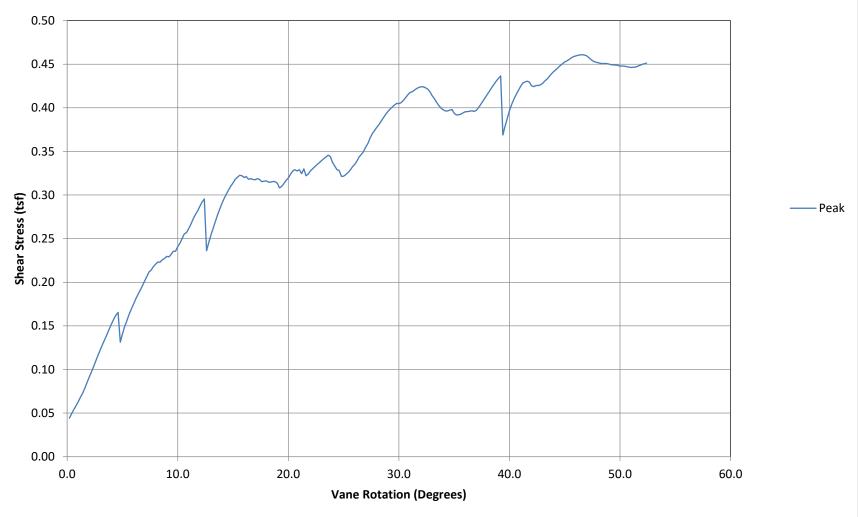
Test Depth (ft): 3.17 Vane Type: Adara solid double tapered 75 x 150

mm (45°, 45°)

Coordinate System: WGS 84 Lat/Long

Latitude: 47.5111048 Longitude: -122.3032936







Location ID: LDW21-GT8-GD

#### **Dynamic Cone Penetrometer**

**Exploration Log** 

180067-02.03 Lower Duwamish Waterway Upper Reach South Park Marina

Surface Elevation: -2.8 MLLW

Groundwater Depth: NA

Start Date 8/4/21 End Date 8/5/21

Performed By: A. Barrett, G. Timm Vert. Datum: NAD83 Hammer Weight: 35 lbs. Horiz. Datum: WA St. Plane N. Cone Area: 10 sq. cm Easting: 1275111.124 Northing: 195841.496

i Northing.	1330	41.450	Ī			Lilu Date 6/3/21			
	Blows	Resistance	Dynamic Con	e Resistano	ce (kg/cm²)	Correlated	Density/Co	onsistency	
Depth	per 10 cm	(kg/cm²)	0 50	100	150	SPT N-Value	Cohesionless	Cohesive	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 1 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 2 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 3 ft	0	0.0				0	V. Loose	V. Soft	
- 1 m	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 4 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 5 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 6 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 2 m	0	0.0				0	V. Loose	V. Soft	
- 7 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 8 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 9 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 3 m 10 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 11 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 12 ft	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
-	0	0.0				0	V. Loose	V. Soft	
- 4 m 13 ft	0	0.0				0	V. Loose	V. Soft	



**Exploration Log** 

eter 180067-02.03 Lower Duwamish Waterway Upper Reach South Park Marina

Location ID: LDW21-GT8-GD Surface Elevation:

Performed By: A. Barrett, G. Timm Groundwater Depth: NA

		Blows	Resistance	Dynam	nic Cone	e Resistance	(kg/cm <sup>2</sup> )	Correlated	Density/Co	onsistency
De	epth	per 10 cm	(kg/cm²)	0	50	100	150	SPT N-Value	Cohesionless	Cohesive
-		0	0.0					0	V. Loose	V. Soft
-		0	0.0					0	V. Loose	V. Soft
-	14 ft	4	11.1	<b></b>				3	V. Loose	Soft
-		5	13.9	<b> •••</b>				3	V. Loose	Soft
-		7	19.4	••••				5	Loose	M. Stiff
-	15 ft	13	36.0	•••••				10	Loose	Stiff
-		24	66.5	•••••	••••			18	M. Dense	V. Stiff
-	16 ft	41 10	113.6 27.7	••••••	••••••	•••••		25+ 7	Dense	Hard M. Stiff
- 5 m	1011	11	30.5	•••••				8	Loose Loose	M. Stiff
- 3		11	30.3					8	Loose	IVI. Still
_	17 ft									
_	17 10									
_										
-	18 ft									
-										
-										
-	19 ft									
-										
- 6 m										
-	20 ft									
-										
-	24 6									
-	21 ft									
	22 ft									
_	22 10									
_										
- 7 m	23 ft									
-										
-										
-	24 ft									
-										
-	_									
-	25 ft									
-										
-	2C ft									
0	26 ft									
- 8 m										
	27 ft									
_	27 IL									
_										
-	28 ft									
-	-									
		·						l		



Exploration Log

ter 180067-02.03 Lower Duwamish Waterway Upper Reach Boeing Development Center

Location ID: GT38-A Surface Elevation: 0.0

Performed By: A. Barrett, G. Timm Groundwater Depth: NA

Vert. Datum: NAD83 Hammer Weight: 35 lbs.

Horiz. Datum: WA St. Plane N. Cone Area: 10 sq. cm
Easting: 1277389.19 Start Date 8/4/21
Northing: 1906166.48 End Date 8/5/21

1101111111	1900100.4				<u> </u>	// / 2\	İ	Ellu Date	
	Blows	Resistance				e (kg/cm²)	Correlated		onsistency
Depth	per 10 cm		0	50	100	150	SPT N-Value	Cohesionless	Cohesive
-	1	4.4	<b> •</b>				1	V. Loose	V. Soft
-	2	8.9	••				2	V. Loose	Soft
- 1 ft	3	13.3	•••				3 5 3	V. Loose	Soft
-	4	17.8	••••				5	Loose	M. Stiff
-	3	13.3	<b></b>				3	V. Loose	Soft
- 2 ft	2	8.9	••				2	V. Loose	Soft
-	1	4.4	<b> •</b>				1	V. Loose	V. Soft
-	4	17.8	••••				5 5	Loose	M. Stiff
- 3 ft	4	17.8	••••				5	Loose	M. Stiff
- 1 m	3	13.3	•••				3	V. Loose	Soft
-	3	11.6	<b> </b>				3	V. Loose	Soft
- 4 ft	2	7.7	<b> </b>				2	V. Loose	Soft
-	3	11.6	<b> </b>				3	V. Loose	Soft
-	3	11.6	•••				3	V. Loose	Soft
- 5 ft	4	15.4					4	V. Loose	Soft
-	3	11.6					3	V. Loose	Soft
-	3	11.6	•••					V. Loose	Soft
- 6 ft	3	11.6	•••				3 3 5 7	V. Loose	Soft
-	5	19.3					5	Loose	M. Stiff
- 2 m	7	27.0					7	Loose	M. Stiff
- 7 ft									
-									
-									
- 8 ft									
_									
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- 9 ft									
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- 3 m 10 ft									
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- 1211									
[									
12 4 22 44									
- 4 m 13 ft									



**Exploration Log** 

Lower Duwamish Waterway Upper Reach Boeing Development Center

180067-02.03

Location ID: GT38-B Surface Elevation: 0.0

Performed By: A. Barrett, G. Timm Groundwater Depth: NA

Vert. Datum: NAD83 Hammer Weight: 35 lbs.

Horiz. Datum: WA St. Plane N. Cone Area: 10 sq. cm

Easting: 1277392.36 Start Date 8/4/21 Northing: 190614.83 End Date 8/5/21

	Blows	<b>5</b>	End Date 8/5/21						
	DIOWS	Resistance	Dynamic Cone	e Resistance	e (kg/cm²)	Correlated	Density/Co	onsistency	
Depth	per 10 cm	(kg/cm²)	0 50	100	150	SPT N-Value	Cohesionless	Cohesive	
-	3	13.3	•••			3	V. Loose	Soft	
-	2	8.9	<b></b>			2	V. Loose	Soft	
- 1 ft	1	4.4	<b> .</b>			1	V. Loose	V. Soft	
ļ-	2	8.9	••			2	V. Loose	Soft	
-	2	8.9	••			2	V. Loose	Soft	
- 2 ft	3	13.3	•••			3	V. Loose	Soft	
-	2	8.9	<b></b>			2	V. Loose	Soft	
ļ-	1	4.4	•			1	V. Loose	V. Soft	
- 3 ft	4	17.8	••••			5	Loose	M. Stiff	
- 1 m	4	17.8	••••			5	Loose	M. Stiff	
ļ-	2	7.7	••			2	V. Loose	Soft	
- 4 ft	3	11.6	•••			3	V. Loose	Soft	
ļ- ļ	3	11.6	•••			3	V. Loose	Soft	
<b> </b> -	3	11.6	•••			3	V. Loose	Soft	
- 5 ft	4	15.4	••••			4	V. Loose	Soft	
-	3	11.6	•••			3	V. Loose	Soft	
-	3	11.6	•••			3	V. Loose	Soft	
- 6 ft	3	11.6	•••			3	V. Loose	Soft	
-	7	27.0	•••••			7	Loose	M. Stiff	
- 2 m	4	15.4	••••			4	V. Loose	Soft	
- 7 ft	3	10.3				2	V. Loose	Soft	
İ- İ	9	30.8	•••••			8	Loose	M. Stiff	
İ- İ	5	17.1	••••			4	V. Loose	Soft	
- 8 ft	8	27.4	•••••			7	Loose	M. Stiff	
ļ-	7	23.9	•••••			6	Loose	M. Stiff	
ļ-	14	47.9	•••••			13	M. Dense	Stiff	
- 9 ft	15	51.3	•••••			14	M. Dense	Stiff	
ļ-	16	54.7	•••••			15	M. Dense	Stiff	
ļ-	19	65.0	•••••			18	M. Dense	V. Stiff	
- 3 m 10 ft	19	65.0	•••••			18	M. Dense	V. Stiff	
-	19	58.1	•••••			16	M. Dense	V. Stiff	
-	20	61.2	•••••			17	M. Dense	V. Stiff	
-	21	64.3	•••••			18	M. Dense	V. Stiff	
- 11 ft	28	85.7	•••••			24	M. Dense	V. Stiff	
-	23	70.4	•••••			20	M. Dense	V. Stiff	
-	18	55.1	•••••			15	M. Dense	Stiff	
- 12 ft	18	55.1	•••••			15	M. Dense	Stiff	
-	18	55.1	•••••			15	M. Dense	Stiff	
-	17	52.0	•••••			14	M. Dense	Stiff	
- 4 m 13 ft	24	73.4	•••••			20	M. Dense	V. Stiff	



**Exploration Log** 

ter 180067-02.03 Lower Duwamish Waterway Upper Reach Boeing Development Center

Location ID: GT38-B Surface Elevation:

Performed By: A. Barrett, G. Timm Groundwater Depth: NA

		Blows	Resistance	Dynamic Cone	e Resistance	(kg/cm <sup>2</sup> )	Correlated	Density/Co	onsistency
De	epth	per 10 cm	(kg/cm²)	0 50	100	150	SPT N-Value	Cohesionless	Cohesive
-		29	80.3	•••••			22	M. Dense	V. Stiff
-		25	69.3	•••••			19	M. Dense	V. Stiff
-	14 ft	20	55.4	•••••			15	M. Dense	Stiff
-		13	36.0	•••••			10	Loose	Stiff
-	45.0	13	36.0	•••••			10	Loose	Stiff
-	15 ft	10	27.7	•••••			7	Loose Loose	M. Stiff
		8 5	22.2 13.9	••••			6 3	V. Loose	M. Stiff Soft
	16 ft	7	19.4				5	Loose	M. Stiff
- 5 m	1011	8	22.2	••••			6	Loose	M. Stiff
-		Ĭ					Ü	20030	
-	17 ft								
-									
-									
-	18 ft								
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-	24.6								
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-	25 ft								
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-	26 ft								
- 8 m									
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-	27 ft								
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-	28 ft								
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# Attachment B Geotechnical Laboratory Testing



July 19, 2022

Anchor QEA, LLC. 1201 3<sup>rd</sup> Avenue, Suite 2600 Seattle, WA 98101

To Whom It May Concern,

MTC approves and authorizes the release and publication of statements, conclusions, and extracts from or regarding our reports to Anchor QEA, LLC.

If you have any other questions, feel free to call us at (360) 755-1990, or email me at <u>alex.eifrig@mtc-inc.net</u>.

Thank you,

MATERIALS TESTING & CONSULTING, INC.

Alex Eifrig

NW Region Laboratory Manager

Alex Eifrig

WABO Supervising Laboratory Technician



Client:	Anchor QEA	Date:	September 23, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1427 - 1446
Revised on:		Date sampled:	7-7-21 & 7-8-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	<del></del>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 23, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1427	LDW21-GT10-GB-0-1.5 ft	233.1	600.7	434.9	165.8	201.8	82.2%
B21-1428	LDW21-GT10-GB-0-9 ft	233.1	804.9	583.3	221.6	350.2	63.3%
B21-1429	LDW21-GT10-GB-9-14 ft	221.7	1019.4	669.5	349.9	447.8	78.1%
B21-1430	LDW21-GT10-GB-14-19 ft	224.1	475.2	368.0	107.2	143.9	74.5%
B21-1431	LDW21-GT10-GB-19-24 ft	217.2	895.4	719.1	176.3	501.9	35.1%
B21-1432	LDW21-GT10-GB-24-25.5 ft	233.7	639.9	567.2	72.7	333.5	21.8%
B21-1433	LDW21-GT28-GB-0-1.5 ft	208.6	1012.3	678.5	333.8	469.9	71.0%
B21-1434	LDW21-GT28-GB-0-10 ft	222.9	1087.3	729.8	357.5	506.9	70.5%
B21-1435	LDW21-GT28-GB-10-11.5 ft	302.0	1045.9	721.9	324.0	419.9	77.2%
B21-1436	LDW21-GT28-GB-10-15 ft	303.4	1236.5	827.0	409.5	523.6	78.2%
B21-1437	LDW21-GT28-GB-15-16.8 ft	311.0	880.9	647.2	233.7	336.2	69.5%
B21-1438	LDW21-GT28-GB-16.8-20 ft	223.0	1069.1	875.2	193.9	652.2	29.7%
B21-1439	LDW21-GT28-GB-20-21.5 ft	221.8	951.4	801.9	149.5	580.1	25.8%
B21-1440	LDW21-GT21-GB-0-1.5 ft	222.7	653.9	446.8	207.1	224.1	92.4%
B21-1441	LDW21-GT21-GB-0-13 ft	234.6	1463.8	860.0	603.8	625.4	96.5%
B21-1442	LDW21-GT21-GB-13-16 ft	225.2	1059.7	808.7	251.0	583.5	43.0%
B21-1443	LDW21-GT21-GB-16-17.5 ft	233.1	805.2	661.3	143.9	428.2	33.6%
B21-1444	LDW21-GT21-GB-16-21 ft	215.7	1239.6	953.1	286.5	737.4	38.9%
B21-1445	LDW21-GT21-GB-21-25.7 ft	225.1	772.5	628.4	144.1	403.3	35.7%
B21-1446	LDW21-GT21-GB-26-31 ft	108.4	1248.4	956.1	292.3	847.7	34.5%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 25, 2021	Tested by: A. Eifrig

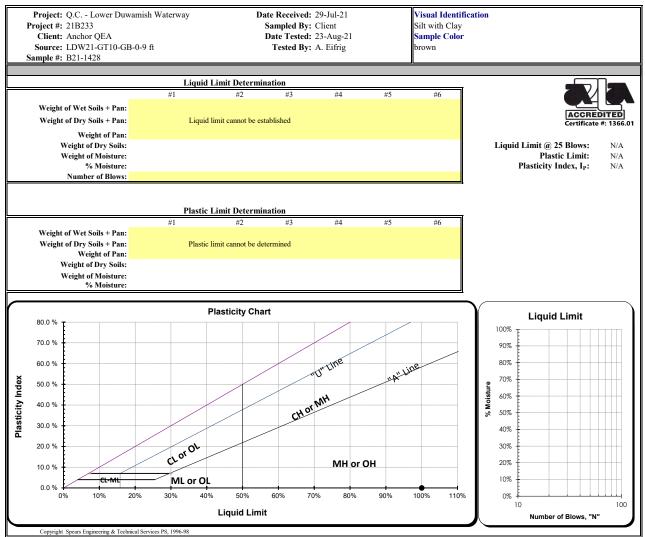
Sample #	Location	Tare	Tare	Mass of Dry Soil	Pycno ID	Mass of Pycno	Volume of Pycno	Water @ Tx		Mass of Pycno filled w/ water	Water, 0.1 *C	SpG of Soils	Factor	SpG
B21-1428	LDW21-GT10-GB-0-9 ft	584.04	660.85	76.8	TSA-011	190.3	499.5	0.99754	734.30	688.64	23.0	2.465721		2.464069
B21-1431	LDW21-GT10-GB-19-24 ft LDW21-GT21-GB-13-16 ft	501.90	602.67	100.8	TSA-021	183.4	499.4	0.99754	742.98	681.60			0.99933	
B21-1442 B21-1445	LDW21-GT21-GB-13-16 ft LDW21-GT21-GB-21-25.7 ft	510.13	611.47	101.3 76.7	TSA-020	195.0	499.5	0.99754	755.39	693.29			0.99933	
B21-1443	LDW21-G121-GB-21-23./ It	500.61	577.32	/0./	TSA-022	198.0	499.5	0.99754	742.91	696.21	23.0	2.5560327	0.99933	2.5543202
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo





All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough control of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization of statements, and an actual public and ourselves are also as the confidential property of clients, and authorization of statements, and all reports are also as the confidential property of clients, and authorization of statements, and all reports are also as the confidential property of clients, and authorization of statements, and all reports are also as the confidential property of clients, and all reports are also also as the confidential property of clients, and all reports are also as the confidential property of clients, and all reports are also as the confidential property of clients, and all reports are also as the confidential property of clients are al

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before

Reviewed by:



Date Received: 29-Jul-21 Visual Identification Project: Q.C. - Lower Duwamish Waterway Project #: 21B233 Silt with Clay Sampled By: Client Client: Anchor QEA Date Tested: 23-Aug-21 Sample Color Source: LDW21-GT10-GB-9-14 ft Tested By: A. Eifrig rown Sample #: B21-1429 **Liquid Limit Determination** Weight of Wet Soils + Pan: 40.29 42.71 29.23 Weight of Dry Soils + Pan: 37.17 38.71 25.20 Weight of Pan: 28.61 28.25 15.04 Liquid Limit @ 25 Blows: Weight of Dry Soils: 8 56 10.46 10.16 Weight of Moisture: Plastic Limit: 3.12 4.00 4.03 N/A % Moisture: Plasticity Index, I<sub>P</sub>: 36.5 % 38.2 % 39.7 % N/A Number of Blows: Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Plastic limit cannot be determined Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 80% 60.0 % A" Line Plasticity Index 50.0 % 60% 40.0 % 50% 30.0 % Cro, Or MH or OH 20% 10.0 % 10% ML or O 0.0 % 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our

Comments: Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



#### **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT10-GB-14-19 ft Sample#: B21-1430

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21 Tested By: A. Eifrig

Visual Identification

Clayey Silt Sample Color: brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.001 \\ D_{(10)} = 0.003 \\ D_{(15)} = 0.005 \\ D_{(30)} = 0.009 \\ \end{array}$ % Gravel = 0.0%% Sand = 8.0% mm % Silt & Clay = 92.0% mm Liquid Limit = n/a mm  $D_{(50)} = 0.024$ mm Plasticity Index = n/a  $D_{(60)}^{(60)} = 0.031$ mm Sand Equivalent = n/a  $D_{(90)} = 0.072$ Dust Ratio = 90/97 mm

Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

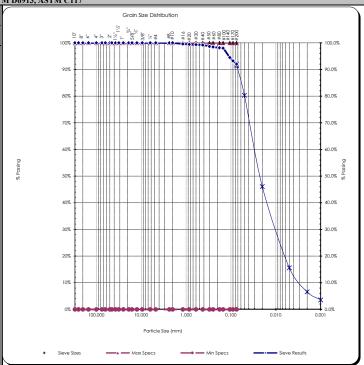
Coeff. of Curvature,  $C_C = 0.79$ Coeff. of Uniformity,  $C_U = 9.14$ Fineness Modulus = 0.04

Plastic Limit = n/a Moisture %, as sampled = 74.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

1101111 0100, 1101	in Doylo, Molini Cili
	/

				AS	TM C136, AS
		Actual	Interpolated		
		Cumulative	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00		100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00		100%	100.0%	0.0%
3/4"	19.00		100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50		100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		100%	100.0%	0.0%
#20	0.850		99%	100.0%	0.0%
#30	0.600		99%	100.0%	0.0%
#40	0.425	99%	99%	100.0%	0.0%



0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

Reviewed by: \_ Meghan Blodgett-Carrillo

92.0%

99%

98%

98%

98%

95%

93%

92.0%



# **Hydrometer Report**

Project:	Q.C Lower	Duwamish Wate	erway Date Recei	ived: 29-Jul-21	Visual Identific	cation						
Project #:	21B233		Sampled	By: Client	Clayey Silt							
Client :	Anchor QEA		Date Te	sted: 23-Aug-21	Sample Color							
Source:	LDW21-GT1	0-GB-14-19 ft	Tested	By: A. Eifrig	brown							
Sample#:	B21-1430			,								
	ASTM D79	28, HYDROM	IETER ANALYSIS		ASTM D6913							
Assumed Sp Gr :	2.65					Sieve A	nalysis					
Sample Weight:	50.30	grams				Grain Size I	Distribution					
Hydroscopic Moist.:	3.78%				Sieve	Percent	Soils P	article				
Adj. Sample Wgt :	48.47	grams		ACCREDITED	Size	Passing	Dian	ieter				
				Certificate #: 1366.01	3.0"	100%	75.000	mm				
Hydrometer					2.0"	100%	50.000	mm				
Reading	Corrected	Percent	Soils Particle		1.5"	100%	37.500					
Minutes	Reading	Passing	Diameter		1.25"	100%	31.500					
1	35	72.2%	0.0444 mm		1.0"	100%	25.000					
2	30.5	62.9%	0.0326 mm		3/4"	100%	19.000					
4	24.5	50.5%	0.0240 mm		5/8"	100%	16.000					
15	18.5	38.2%	0.0129 mm		1/2"	100%	12.500					
30	15	30.9%	0.0093 mm		3/8"	100%	9.500					
60 240	10.5 5	21.7%	0.0068 mm		1/4" #4	100% 100%	6.300					
	2.5	10.3%	0.0035 mm				4.750					
1440	2.3	5.2%	0.0014 mm		#10 #20	100% 99%	2.000					
% Gravel:	0.0%		T::		#20 #40	99%	0.850					
% Gravei: % Sand:	8.0%		Liquid Limit: n/a Plastic Limit: n/a		#100	98%	0.425 0.150					
% Salit:	76.4%		Plasticity Index: n/a		#200	92.0%	0.130					
% Clay:	15.6%		riasticity fluex: 11/a		#200 Silts	91.4%	0.073					
76 Clay.	15.070				Sitts	80.4%	0.050					
						46.1%	0.020					
					Clays	15.6%	0.005					
					Cinjo	6.6%	0.002					
					Colloids	3.6%	0.001					
	USDA	Soil Textural	Classification									
		Particle Size										
% Sand:		2.0 - 0.05 mm										
% Silt:		0.05 - 0.002 mm										
% Clay:		< 0.002 mm										
	USDA	A Soil Textural	Classification									
		Silt Loam										
All results apply only to actual location regarding our reports is reserved pen			clients, the public and ourselves, all repo	orts are submitted as the confidentia	l property of clients, and aut	horization for publication of	statements, conclusions or	extracts from or				
regarding our reports is reserved pen	unig our written appro	vai.										
Comments:												
<u>-</u>												
	1 11	abjet arillo										
	(Yogh to	orget and lo										
Reviewed by:		0										

Reviewed by:

#### **Direct Shear Test Results:**

#### ASTM D-3080



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1430
Sample Date:	7/7/2021
Test Date:	9/20/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT10-GB-14-19 ft

 Visual Soil Description:
 brown clayey silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

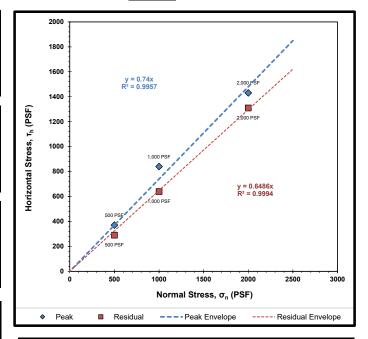
Specimen Height (in): 1
Rate of Strain (in/min): 0.0042
Estimated Specific Gravity of Solids: 2.65

Summary of Sampl	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	45.3	
	Initial	Post-Consolidation
Dry Density (PCF):	91.7	95.2
Void Ratio:	0.837	0.770
Porosity (%):	45.6	43.5
Degree of Saturation (%):	saturated	saturated

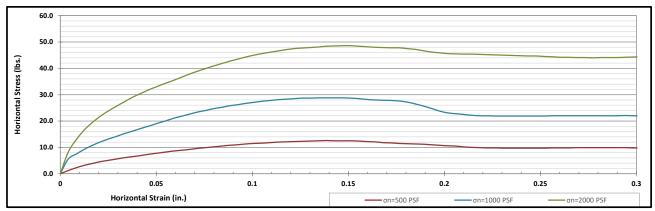
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	40.4	
	Initial	Post-Consolidation
Dry Density (PCF):	95.4	102.4
Void Ratio:	0.765	0.646
Porosity (%):	43.4	39.3
Degree of Saturation (%):	saturated	saturated

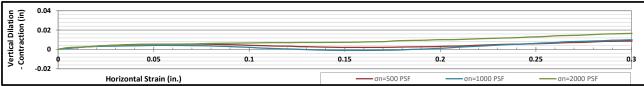
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	37.0	
	Initial	Post-Consolidation
Dry Density (PCF):	97.7	106.6
Void Ratio:	0.725	0.581
Porosity (%):	42.0	36.7
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS								
	PEAK	RESIDUAL						
Angle of Internal Friction, φ (°):	37	33						
Cohesion (PSF):	0	0						



Failure Envelope Test	Values:		
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	370	840	1430
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	640	1310





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#### **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#40

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Source: LDW21-GT10-GB-19-24 ft Sample#: B21-1431

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color: grayish-brown

mm



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.014 \\ D_{(10)} = 0.027 \\ D_{(15)} = 0.041 \\ D_{(30)} = 0.079 \\ \end{array}$ % Gravel = 0.0%% Sand = 72.5% mm % Silt & Clay = 27.5% mm Liquid Limit = n/a mm  $D_{(50)} = 0.108$ mm Plasticity Index = n/a  $D_{(60)} = 0.122$ mm  $D_{(90)} = 0.298$ Dust Ratio = 13/47

Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 1.85$ Coeff. of Uniformity,  $C_U = 4.47$ Fineness Modulus = 0.32

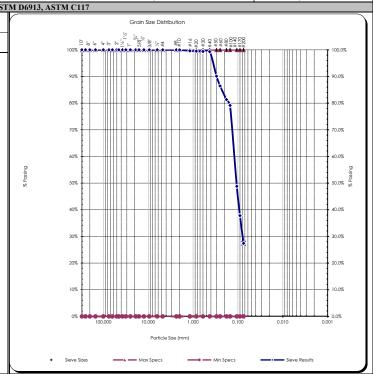
Plastic Limit = n/a Moisture %, as sampled = 35.1% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					The Cites
		Actual Cumulative	Interpolated e Cumulative	AS	TM C136,
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00		100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		100%	100.0%	0.0%
#20	0.850		99%	100.0%	0.0%
#30	0.600		99%	100.0%	0.0%

99%

27.5%



0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

Reviewed by: Meghan Blodgett-Carrillo

99%

90%

86%

81%

49%

38%

27.5%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%



Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Visual Identification Sampled By: Client Clay with Silt Client: Anchor QEA Date Tested: 25-Aug-21 Sample Color Source: LDW21-GT28-GB-0-10 ft Tested By: A. Eifrig dark brown Sample #: B21-1434 **Liquid Limit Determination** Weight of Wet Soils + Pan: 33.52 24.84 28.54 21.54 Weight of Dry Soils + Pan: 28.91 25.61 Weight of Pan: 19.45 14.96 19.90 Liquid Limit @ 25 Blows: Weight of Dry Soils: 9 46 6.58 5.71 Weight of Moisture: Plastic Limit: 4.61 3.30 2.93 N/A Plasticity Index, I<sub>P</sub>: % Moisture: 48.7 % 50.2 % 51.3 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 90% 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

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Comments: Plastic Limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Visual Identification Silty Clay **Sample Color** Sampled By: Client Client: Anchor QEA Date Tested: 25-Aug-21 Source: LDW21-GT28-GB-10-15 ft Tested By: A. Eifrig dark brown Sample #: B21-1436 **Liquid Limit Determination** Weight of Wet Soils + Pan: 30.19 31.68 32.21 27,44 27.75 Weight of Dry Soils + Pan: 26.52 Weight of Pan: 19.62 19.54 19.84 Liquid Limit @ 25 Blows: Weight of Dry Soils: 6.90 7.90 7 91 Weight of Moisture: Plastic Limit: 3.67 4.24 4.46 N/A Plasticity Index, I<sub>P</sub>: % Moisture: 53.2 % 53.7 % 56.4 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

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Comments: Plastic Limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Visual Identification Sampled By: Client Clay and Silt Client: Anchor QEA Date Tested: 25-Aug-21 Sample Color Source: LDW21-GT28-GB-15-16.8 ft Tested By: A. Eifrig dark brown Sample #: B21-1437 **Liquid Limit Determination** Weight of Wet Soils + Pan: 31.73 40.08 39.56 Weight of Dry Soils + Pan: 28.13 36.32 36.04 Weight of Pan: 28.53 19.86 28.17 Liquid Limit @ 25 Blows: Weight of Dry Soils: 8 27 8.15 7.51 Weight of Moisture: Plastic Limit: 3.60 3.76 3.52 N/A Plasticity Index, I<sub>P</sub>: % Moisture: 43.5 % 46.1 % 46.9 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

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Comments: Plastic Limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



#### **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT28-GB-16.8-20 ft

Sample#: B21-1438

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP, Poorly graded Sand Sample Color:

gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.085 \\ \textbf{D}_{(10)} = 0.125 \\ \textbf{D}_{(15)} = 0.157 \\ \textbf{D}_{(30)} = 0.213 \\ \textbf{D}_{(50)} = 0.288 \\ \textbf{D}_{(60)} = 0.325 \\ \textbf{D}_{(90)} = 0.827 \\ \textbf{D}_{(90)} = 0.$ % Gravel = 0.0%% Sand = 96.2% mm % Silt & Clay = 3.8% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 1.12$ Coeff. of Uniformity,  $C_U = 2.60$ Fineness Modulus = 1.53

Plastic Limit = n/a Moisture %, as sampled = 29.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

IX.	equiriaciure 70, i race –
Req	'd Fracture %, 2+ Faces =

					D	ust Ratio =	1/23		Fractu	ire %, 2	+ Fac	es = n	/a		Rec	q'd Fra	cture	%, 2⊣	Faces	=
				AS	TM C136, AS	FM D6913,	ASTM C11	7												
			Interpolated						Gr	ain Size Di	stributio	n								
			Cumulative			4			Ę.,											
Sieve		Percent	Percent	Specs	Specs		ė	90 40 4 W	2%:	8 8 4 :	# # <u></u>	28	8 4 8	8888	28					
US	Metric	Passing	Passing	Max	Min	4	100% 🏩					-	444	44	<del>Hi</del> ll	ттт		ПТТ	T	100.0%
12.00"	300.00		100%	100.0%	0.0%		-					<b>\</b>							1 1	
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8.00"	200.00		100%	100.0%	0.0%		90%					T N	•		*****			1111	1 1	90.0%
6.00"	150.00		100%	100.0%	0.0%		ţ						li						1 1	
4.00"	100.00		100%	100.0%	0.0%		80%								ШШ			Ш		80.0%
3.00"	75.00		100%	100.0%	0.0%		E E												1	
2.50"	63.00		100%	100.0%	0.0%		-												1 1	
2.00"	50.00		100%	100.0%	0.0%		70%		+++-+		+++		₩			+++		+++		70.0%
1.75"	45.00		100%	100.0%	0.0%		1												1 1	
1.50"	37.50		100%	100.0%	0.0%														1	
1.25"	31.50		100%	100.0%	0.0%		60%						****		*****	+++		+++	1 1	60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	Ď.	t						1111						1 1	g.
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%						1111						1 1.	50.0% %
5/8"	16.00		100%	100.0%	0.0%	96	30% T												T 7	30.0% 88
1/2"	12.50	100%	100%	100.0%	0.0%		-												1 1	
3/8"	9.50	100%	100%	100.0%	0.0%		40%							<u> </u>		444		$\square$	<b></b>	40.0%
1/4"	6.30		100%	100.0%	0.0%		ļ.							1						
#4	4.75	100%	100%	100.0%	0.0%		t							1					1 1	
#8	2.36		100%	100.0%	0.0%		30%		HHH					-		+++		+++	<del>     </del>	30.0%
#10	2.00	100%	100%	100.0%	0.0%		ŀ							1					1 1	
#16	1.18		93%	100.0%	0.0%		20%							ļ					11.	20.0%
#20	0.850		90%	100.0%	0.0%		20%						Ш					m		20.0%
#30	0.600		88%	100.0%	0.0%		1							Ĭ					1 1	
#40	0.425	87%	87%	100.0%	0.0%		10%					—Ш	Ш	$\perp$	ШШ	444		$\coprod$	1	10.0%
#50	0.300		53%	100.0%	0.0%														1 1	
#60	0.250		40%	100.0%	0.0%		1								*					
#80	0.180		21%	100.0%	0.0%		0%	100.000	-	10.000		1.000	9494	po-po-i	100		0.010	шп	0.001	0.0%
#100	0.150	13%	13%	100.0%	0.0%			100.000		10.000		1.000		0.	100		0.010		0.001	
#140	0.106	-270	8%	100.0%	0.0%					Partio	cle Size (r	nm)								
#170	0.090		6%	100.0%	0.0%															
#200	0.075	3.8%	3.8%	100.0%	0.0%		+ Sieve Size	ς.		Max Specs		_	_ M	tin Specs		_	Sie	eve Resu	ts	
	Spears Engineering & Tecl			100.070	0.070		. 56.75 5126	-						υρυυ			Sie		-	
				and ourselves, all reports are	submitted as the confide	ntial property of cl	lients, and authoriz	ation for pub	lication of	statements	conclusio	ons or evt	racts fro	om or rea	arding .	our repor	ts is reser	rved nen-	ling our w	ritten app

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1438
Sample Date:	7/7/2021
Test Date:	8/25/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT28-GB-16.8-20 ft

 Visual Soil Description:
 gray sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

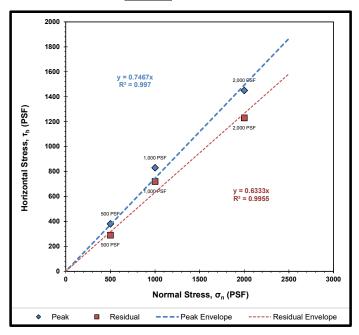
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Samp	le Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	31.3	
	Initial	Post-Consolidation
Dry Density (PCF):	105.4	106.7
Void Ratio:	0.598	0.579
Porosity (%):	37.4	36.7
Degree of Saturation (%):	saturated	saturated

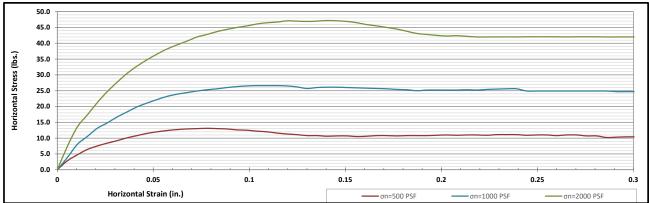
Summary of Sampl	e Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	31.0	
	Initial	Post-Consolidation
Dry Density (PCF):	105.6	107.2
Void Ratio:	0.595	0.572
Porosity (%):	37.3	36.4
Degree of Saturation (%):	saturated	saturated

Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	32.9	
	Initial	Post-Consolidation
Dry Density (PCF):	104.0	107.8
Void Ratio:	0.619	0.562
Porosity (%):	38.2	36.0
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS							
PEAK RESIDUAL							
Angle of Internal Friction, φ 37 32							
Cohesion (PSF):	0	0					



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	380	830	1450				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	720	1230				





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Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Visual Identification Silty Clay **Sample Color** Sampled By: Client Client: Anchor QEA Date Tested: 25-Aug-21 Source: LDW21-GT21-GB-0-13 ft Tested By: A. Eifrig dark brown Sample #: B21-1441 **Liquid Limit Determination** Weight of Wet Soils + Pan: 28.39 31.98 25.34 27.63 Weight of Dry Soils + Pan: 23.97 21.68 Weight of Pan: 15.01 19.45 14.80 Liquid Limit @ 25 Blows: Weight of Dry Soils: 8 96 8 18 6.88 52 % Weight of Moisture: Plastic Limit: 4.42 4.35 3.66 N/A Plasticity Index, I<sub>P</sub>: % Moisture: 53.2 % 49.3 % 53.2 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 90% 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

ut results apply only to actual locations and materians tested. As a mutual protection to citeria, the public and ourserves, air reports are summitted as the commental property of citeria, and authorization for publication of statements, concussions of extracts from or regarding our

Comments: Plastic Limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



## **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#200

0.075

22.0%

Meghan Blodgett-Carrillo

Source: LDW21-GT21-GB-13-16 ft Sample#: B21-1442

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21 Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.017 \\ D_{(10)} = 0.034 \\ D_{(15)} = 0.051 \\ D_{(30)} = 0.096 \\ \end{array}$ mm mm mm  $D_{(50)} = 0.150$ mm  $D_{(60)} = 0.239$ mm  $D_{(90)} = 1.216$ Dust Ratio = 3/11 mm

% Silt & Clay = 22.0% Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

% Gravel = 0.2%

% Sand = 77.9%

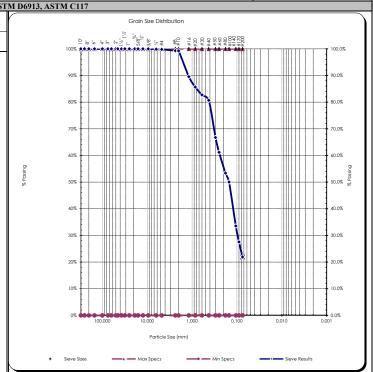
Coeff. of Curvature,  $C_C = 1.14$ Coeff. of Uniformity,  $C_U = 7.00$ Fineness Modulus = 1.12 Plastic Limit = n/a

Moisture %, as sampled = 96.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136, AST		
		Actual	Interpolated				
		Cumulative	Cumulative				
Sieve	Size	Percent	Percent Percent Specs 5				
US	Metric	Passing	Passing	Max	Min		
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00		100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%		
3/4"	19.00	100%	100%	100.0%	0.0%		
5/8"	16.00		100%	100.0%	0.0%		
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		99%	100.0%	0.0%		
#10	2.00	99%	99%	100.0%	0.0%		
#16	1.18		90%	100.0%	0.0%		
#20	0.850		86%	100.0%	0.0%		
#30	0.600		83%	100.0%	0.0%		
#40	0.425	81%	81%	100.0%	0.0%		
#50	0.300		67%	100.0%	0.0%		
#60	0.250		61%	100.0%	0.0%		
#80	0.180		53%	100.0%	0.0%		
#100	0.150	50%	50%	100.0%	0.0%		
#140	0.106		34%	100.0%	0.0%		
#170	0.090		28%	100.0%	0.0%		

22.0%



0.0%

Reviewed by:

100.0%



## **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT21-GB-16-21 ft Sample#: B21-1444

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color: dark gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{ASINID43} \\ \textbf{D}_{(5)} = 0.019 \\ \textbf{D}_{(10)} = 0.039 \\ \textbf{D}_{(15)} = 0.058 \\ \textbf{D}_{(30)} = 0.104 \\ \textbf{D}_{(50)} = 0.177 \\ \textbf{D}_{(60)} = 0.256 \\ \textbf{D}_{(90)} = 1.188 \\ \textbf{Partia} = 5/21 \\ \textbf{D}_{(10)} = 5/21 \\ \textbf{D}_$ % Gravel = 0.1% % Sand = 80.5% mm % Silt & Clay = 19.4% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 1.10$ Coeff. of Uniformity,  $C_U = 6.61$ Fineness Modulus = 1.15

Plastic Limit = n/a Moisture %, as sampled = 38.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

					Dı	ıst Ratio =	5/21		Fracture %, 2+	Faces =	n/a	R	teq'd Fr	racture '	%, 2+ I	races =
				AS	TM C136, AST	M D6913,	ASTM C11	7								
		Actual	Interpolated						Grain Size Dis	tribution						
		Cumulative	Cumulative													
Sieve		Percent	Percent	Specs	Specs		io	الماما ماما	1½" 1" 1½" 5/8"," 3/8" 1,"	<u>∞</u> 2 2 8	8 8 8 8	88888				
US	Metric	Passing	Passing	Max	Min		100% 🞎					*****	arr -	TTIT		<b>T</b> 100.0%
12.00"	300.00		100%	100.0%	0.0%		1			1						- 1
10.00"	250.00		100%	100.0%	0.0%					\						- 1
8.00"	200.00		100%	100.0%	0.0%		90%			++	HHHH	1	.###	1-11-11-1		90.0%
6.00"	150.00		100%	100.0%	0.0%		ŀ									1
4.00"	100.00		100%	100.0%	0.0%		80%						ШШ			80.0%
3.00"	75.00		100%	100.0%	0.0%						<b>   </b>					1 00.0%
2.50"	63.00		100%	100.0%	0.0%		F				<b> </b>					- 1
2.00"	50.00		100%	100.0%	0.0%		70%				₩₩				$\square$	70.0%
1.75"	45.00		100%	100.0%	0.0%		1									- 1
1.50"	37.50		100%	100.0%	0.0%											- 1
1.25"	31.50		100%	100.0%	0.0%		60%				***************************************		###	-		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0	ŀ					V III				9
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%					<i>I</i> III				50.0% <sub>k</sub> g
5/8"	16.00		100%	100.0%	0.0%	98	50% F					1				30.0% %
1/2"	12.50	100%	100%	100.0%	0.0%		-					1				- 1
3/8"	9.50	100%	100%	100.0%	0.0%		40%			$\square$		+1		<b>—Ш</b>	+++	40.0%
1/4"	6.30		100%	100.0%	0.0%		1					1 1 1 1 1				1
#4	4.75	100%	100%	100.0%	0.0%		t					1 11				1
#8	2.36		99%	100.0%	0.0%		30%					<b>+ i</b> #	###	1-111	++++	30.0%
#10	2.00	99%	99%	100.0%	0.0%		ŀ					N.				ł
#16	1.18		90%	100.0%	0.0%		20%					I N				20.0%
#20	0.850		86%	100.0%	0.0%		20% F					Ť	ППП			20.0%
#30	0.600		83%	100.0%	0.0%		-									- 1
#40	0.425	81%	81%	100.0%	0.0%		10%						Ш.	4	$\coprod$	10.0%
#50	0.300		66%	100.0%	0.0%											- 1
#60	0.250		59%	100.0%	0.0%		t									1
#80	0.180		50%	100.0%	0.0%		0%	100.000	10.000	1.00	-	0.100	, 4444	0.010		0.0%
#100	0.150	47%	47%	100.0%	0.0%			100.000	10.000	1.00	-	0.100		0.010		2.301
#140	0.106		31%	100.0%	0.0%				Particl	e Size (mm)						
#170	0.090		25%	100.0%	0.0%											
#200	0.075	19.4%	19.4%	100.0%	0.0%		Sieve Size	s <b>–</b>	<b>─</b> ▲ <b>─</b> Max Specs	_	- Mir	n Specs	_	Sie	eve Results	
Copyright	Spears Engineering & Tec	chnical Services PS, 1996-9	8													

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1444
Sample Date:	7/8/2021
Test Date:	9/13/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT21-GB-16-21 ft

 Visual Soil Description:
 dark gray sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

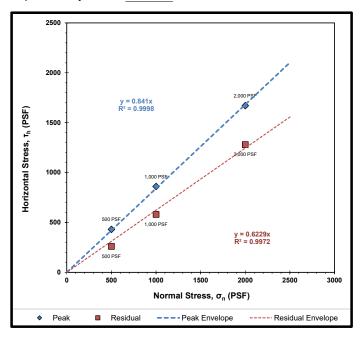
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%):	26.8	
	Initial	Post-Consolidation
Dry Density (PCF):	107.5	109.1
Void Ratio:	0.568	0.545
Porosity (%):	36.2	35.3
Degree of Saturation (%):	saturated	saturated

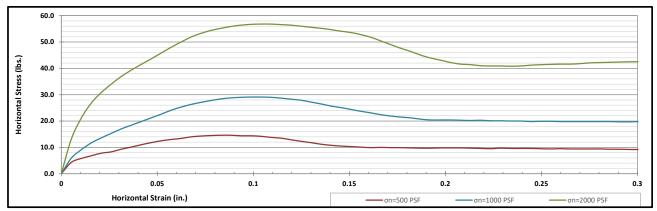
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	26.2	
	Initial	Post-Consolidation
Dry Density (PCF):	107.6	110.8
Void Ratio:	0.566	0.521
Porosity (%):	36.1	34.3
Degree of Saturation (%):	saturated	saturated

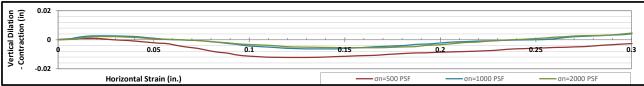
Summary of Sampl	e Data:	σ <sub>n</sub> =2000 PSF		
Initial Moisture Content (%):	24.9			
	Initial	Post-Consolidation		
Dry Density (PCF):	108.8	113.7		
Void Ratio:	0.549	0.481		
Porosity (%):	35.4	32.5		
Degree of Saturation (%):	saturated	saturated		

ESTIMATED STRENGTH PARAMETERS							
	PEAK	RESIDUAL					
Angle of Internal Friction, φ (°):	40	32					
Cohesion (PSF):	0	0					



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	430	860	1670				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	260	580	1280				





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#### **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#50

#60

#80 #100

#140

#170

#200

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Source: LDW21-GT21-GB-21-25.7 ft Sample#: B21-1445

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 23-Aug-21 Tested By: A. Eifrig

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

Visual Identification Sandy Silt

Sample Color: grayish-brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

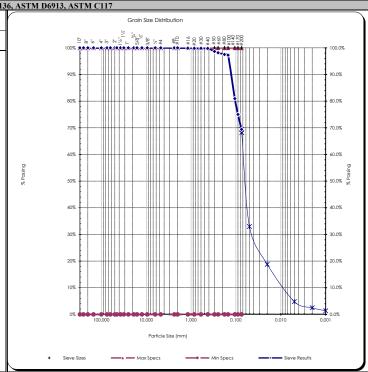
 $\begin{array}{c} D_{(5)} = 0.005 \\ D_{(10)} = 0.010 \\ D_{(15)} = 0.015 \\ D_{(30)} = 0.040 \\ D_{(30)} = 0.040 \end{array}$ % Gravel = 0.0%% Sand = 30.5% mm % Silt & Clay = 69.5% mm Liquid Limit = n/a mm  $D_{(50)} = 0.060$ mm  $D_{(60)} = 0.068$ mm

mm

Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 2.30$ Coeff. of Uniformity,  $C_U = 6.70$ Fineness Modulus = 0.04 Plastic Limit = n/a Moisture %, as sampled = 35.7%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(60)} - 0.008$
						$D_{(90)} = 0.130$
					Di	ust Ratio = 16/23
					ASTM C1	36, ASTM D6913,
		Actual	Interpolated			
		_	Cumulative	_		
	e Size	Percent	Percent	Specs	Specs	
US	Metric	Passing	Passing	Max	Min	1
12.00"	300.00		100%	100.0%	0.0%	
10.00"	250.00		100%	100.0%	0.0%	
8.00"	200.00		100%	100.0%	0.0%	
6.00"	150.00		100%	100.0%	0.0%	
4.00"	100.00		100%	100.0%	0.0%	
3.00"	75.00		100%	100.0%	0.0%	
2.50"	63.00		100%	100.0%	0.0%	
2.00"	50.00		100%	100.0%	0.0%	
1.75"	45.00		100%	100.0%	0.0%	
1.50"	37.50		100%	100.0%	0.0%	
1.25"	31.50		100%	100.0%	0.0%	
1.00"	25.00		100%	100.0%	0.0%	2
3/4"	19.00		100%	100.0%	0.0%	7 Passing
5/8"	16.00		100%	100.0%	0.0%	96
1/2"	12.50		100%	100.0%	0.0%	
3/8"	9.50	100%	100%	100.0%	0.0%	
1/4"	6.30		100%	100.0%	0.0%	
#4	4.75	100%	100%	100.0%	0.0%	
#8	2.36		100%	100.0%	0.0%	
#10	2.00	100%	100%	100.0%	0.0%	
#16	1.18		100%	100.0%	0.0%	
#20	0.850		100%	100.0%	0.0%	
#30	0.600		100%	100.0%	0.0%	
#40	0.425	100%	100%	100.0%	0.0%	
		2 30 70	1 20070	2.0.070	2.070	II



0.0%

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0.0%

**Comments:** Reviewed by: \_ Meghan Blodgett-Carrillo

69.5%

99%

98%

98%

97%

81%

75%

69.5%



# **Hydrometer Report**

Project:	Q.C Lower	Duwamish Water	way Date Rece	ived: 29-Jul-21	Visual Identific	cation		
Project #:	Project #: 21B233 Sampled By: Client				Sandy Silt			
Client :	Client: Anchor QEA Date Tested: 23-Aug-21							
Source:	1-GB-21-25.7 ft	gravish-brown						
Sample#:	B21-1445		,					
	ASTM D79	28, HYDROM	ETER ANALYSIS			ASTM	D6913	
Sp Gr :	2.55	, , , , , , , , , , , , , , , , , , ,				Sieve A		
Sample Weight:	51.07	grams				Grain Size I	•	
Hydroscopic Moist.:	0.72%	2			Sieve	Percent	Soils Particle	
Adj. Sample Wgt :	50.70	grams		ACCREDITED	Size	Passing	Diameter	
		C		Certificate #: 1366.01	3.0"	100%	75.000 mm	
Hydrometer					2.0"	100%	50.000 mm	
Reading	Corrected	Percent	Soils Particle		1.5"	100%	37.500 mm	
Minutes	Reading	Passing	Diameter		1.25"	100%	31.500 mm	
1	19.5	39.2%	0.0512 mm		1.0"	100%	25.000 mm	
2	14	28.2%	0.0373 mm		3/4"	100%	19.000 mm	
4	12	24.1%	0.0266 mm		5/8"	100%	16.000 mm	
15	7	14.1%	0.0142 mm		1/2"	100%	12.500 mm	
30	5	10.1%	0.0101 mm		3/8"	100%	9.500 mm	
60	3	6.0%	0.0072 mm		1/4"	100%	6.300 mm	
240	2	4.0%	0.0036 mm		#4	100%	4.750 mm	
1440	1	2.0%	0.0015 mm		#10	100%	2.000 mm	
					#20	100%	0.850 mm	
% Gravel:	0.0%		Liquid Limit: n/a		#40	100%	0.425 mm	
% Sand:	30.5%		Plastic Limit: n/a		#100	97%	0.150 mm	
% Silt:	64.7%	F	Plasticity Index: n/a		#200	69.5%	0.075 mm	
% Clay:	4.8%				Silts	68.2%	0.074 mm	
						33.0%	0.050 mm	
						18.8%	0.020 mm	
					Clays	4.8%	0.005 mm	
						2.5%	0.002 mm	
					Colloids	1.4%	0.001 mm	
	USDA	Soil Textural	Classification					
		Particle Size						
% Sand:		2.0 - 0.05 mm						
% Silt:		0.05 - 0.002 mm						
% Clay:		< 0.002 mm						
70 City.		· 0.002 mm						
	USDA	Soil Textural	Classification					
		Sandy Loam						
All results apply only to actual location	ons and materials teste	d. As a mutual protection to c	lients, the public and ourselves, all rep	orts are submitted as the confidentia	l property of clients, and aut	horization for publication of	statements, conclusions or extracts from or	
regarding our reports is reserved pen	ding our written appro	val.						
Comments:								
	1 11	alget aille						
	(Yogh the	Odget and 10						
Reviewed by:	0	O						



#### **Sieve Report**

Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT21-GB-26-31 ft

Sample#: B21-1446

#200

0.075

28.9%

Meghan Blodgett-Carrillo

28.9%

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 23-Aug-21 Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

gray



70.0%

30.0%

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASINID43} \\ \textbf{D}_{(5)} = 0.013 \\ \textbf{D}_{(10)} = 0.026 \\ \textbf{D}_{(15)} = 0.039 \\ \textbf{D}_{(30)} = 0.077 \\ \textbf{D}_{(50)} = 0.119 \\ \textbf{D}_{(60)} = 0.140 \\ \textbf{D}_{(90)} = 0.354 \end{array}$ % Gravel = 0.0%% Sand = 71.1% mm % Silt & Clay = 28.9% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture % 1 Face = n/a Coeff. of Curvature,  $C_C = 1.65$ Coeff. of Uniformity,  $C_U = 5.38$ Fineness Modulus = 0.53

Plastic Limit = n/a Moisture %, as sampled = 34.2% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = eq'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.354$	mm		ture %, 1 F			Re	
						ust Ratio = 12/41		Fractu	re %, 2+ Fa	ces = n/a		Req'	d
			T	AS	STM C136, AST	FM D6913, ASTM	C117						
		Actual	Interpolated Cumulative					Gro	ain Size Distribut	tion			
Ciarre	Size	Percent	Percent	Specs	Specs	_		š :.					
US	Metric	Passing	Passing	Max	Min		ادة ادادة الأمامة \$200	7 2 3 4 2 2 3 4 3 2 2 3 4	3/8′ #	# 19 8 9 # # 19 8 9 # # 19 8 9 # # 19 8 9 # # 19 8 9 # 19 8 9 # 19 8 9 # 19 8 9 # 19 8 9 9 # 19 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	88824	200	
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8.00"	200.00		100%	100.0%	0.0%		90%				₩-	++++	
6.00"	150.00		100%	100.0%	0.0%		11				N		
4.00"	100.00		100%	100.0%	0.0%						1		
3.00"	75.00		100%	100.0%	0.0%		80%				1	ШШ	
2.50"	63.00		100%	100.0%	0.0%						N		
2.00"	50.00		100%	100.0%	0.0%		70%				$\sqcup 1$	ЩШ	,
1.75"	45.00		100%	100.0%	0.0%						1 1		
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1.25"	31.50		100%	100.0%	0.0%		60%				+++		
1.00"	25.00	100%	100%	100.0%	0.0%	p							
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				<b> </b>		
5/8"	16.00		100%	100.0%	0.0%	₩.	50%						
1/2"	12.50	100%	100%	100.0%	0.0%								.
3/8"	9.50	100%	100%	100.0%	0.0%		40%				$HH^{-1}$	<b></b>	۲
1/4"	6.30		100%	100.0%	0.0%							l l	
#4	4.75	100%	100%	100.0%	0.0%							1	.
#8	2.36		100%	100.0%	0.0%		30%			1-1111			H
#10	2.00	100%	100%	100.0%	0.0%								.
#16	1.18		99%	100.0%	0.0%		20%						
#20	0.850		99%	100.0%	0.0%								
#30	0.600		99%	100.0%	0.0%		1						, 1
#40	0.425	99%	99%	100.0%	0.0%		10%				++-		
#50	0.300		83%	100.0%	0.0%								
#60	0.250		77%	100.0%	0.0%					⊥ <u>.</u>	Ш.	Щ	
#80	0.180		69%	100.0%	0.0%		U% <b>600-0</b>	00.000	10.000	1.000	0.	100	_
#100	0.150	65%	65%	100.0%	0.0%								
#140	0.106		44%	100.0%	0.0%				Particle Size	(mm)			
#170	0.090		36%	100.0%	0.0%								

0.0%

Reviewed by:

100.0%



Client:	Anchor QEA	Date:	September 28, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1321 - 1335
Revised on:		Date sampled:	7-26-21 & 7-27-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



## **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 24, 2021	Tested by: A. Eifrig

4-0-5 ft -5-13.6ft	233.2	6.10			Wgt. Of Soil	% Moisture
-5-13.6ft		648.4	595.4	53.0	362.2	14.6%
0 10.010	234.1	1046.2	877.7	168.5	643.6	26.2%
13.6-29 ft	232.6	1197.1	1046.9	150.2	814.3	18.4%
-33-35 ft	229.5	540.4	454.5	85.9	225.0	38.2%
-35-43 ft	233.3	1203.4	995.3	208.1	762.0	27.3%
-43-50 ft	223.9	840.4	682.9	157.5	459.0	34.3%
53.3-59 ft	234.6	1087.0	874.9	212.1	640.3	33.1%
5-0-3.6 ft	215.2	760.8	729.9	30.9	514.7	6.0%
·3.6-6.2 ft	217.1	499.1	461.2	37.9	244.1	15.5%
-6.2-9.5 ft	91.9	740.7	600.6	140.1	508.7	27.5%
9.5-11.7 ft	221.2	864.4	682.7	181.7	461.5	39.4%
11.7-32 ft	215.5	1106.1	985.3	120.8	769.8	15.7%
32-34.7 ft	223.9	674.7	563.9	110.8	340.0	32.6%
34.7-50 ft	759.4	1828.1	1623.0	205.1	863.6	23.7%
0.5-61.5 ft	233.5	678.3	545.8	132.5	312.3	42.4%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 26, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Dry Soil + Tare	Mass of Dry Soil	Pycno ID	Mass of Pycno	Volume of Pycno	Density of Water @ Tx	Mass of Pycno filled w/ water & soils	Mass of			Temp. Correction Factor	Corrected SpG
B21-1323	LDW21-GT24-13.6-29 ft	601.52	701.51	100.0	TSA-010	180.3	499.5	0.99754	742.00	678.62	23.0	2.7311347	0.99933	2.7293049
B21-1326	LDW21-GT24-43-50 ft	497.42	571.51	74.1	TSA-017	187.9	499.4	0.99754	731.68	686.06		2.6022626		2.600519
B21-1332	LDW21-GT36-11.7-32 ft	497.79	598.00	100.2	TSA-015	187.6	499.5	0.99754	748.84	685.87	23.0	2.6908295	0.99933	2.6890267
B21-1335	LDW21-GT36-50.5-61.5 ft	600.15	650.57	50.4	TSA-016	197.2	499.5	0.99754	726.46	695.45	23.0	2.5974523	0.99933	2.595712
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT24-5-13.6 ft Sample#: B21-1322

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 24-Aug-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

#100

#140

#170

#200

0.150

0.106

0.090

0.075

10%

4.0%

Sample Meets Specs? N/A

 $D_{(5)} = 0.087$   $D_{(10)} = 0.149$   $D_{(15)} = 0.176$   $D_{(30)} = 0.252$ % Gravel = 0.4% % Sand = 95.6% mm % Silt & Clay = 4.0% mm Liquid Limit = 0.0% mm  $D_{(50)} = 0.321$ mm Plasticity Index = 0.0%  $D_{(60)} = 0.355$ mm Sand Equivalent = n/a D<sub>(90)</sub> = 0.640 mm ust Ratio = 1/20 TM D6913, ASTM C117 mm

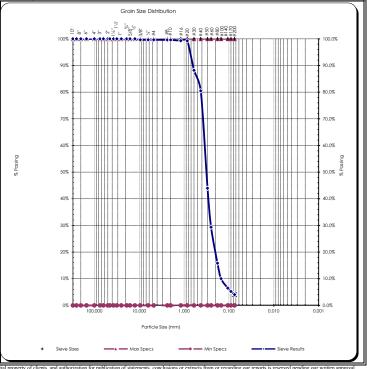
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.20$ Coeff. of Uniformity,  $C_U = 2.38$ 

Fineness Modulus = 1.60 Plastic Limit = 0.0% Moisture %, as sampled = 26.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

		,
Req'd Fract	ure %, 2	+ Faces =

				AG	TM C136,
		Actual Cumulative	Interpolated Cumulative	AS	1 M C130,
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		99%	100.0%	0.0%
#20	0.850	99%	99%	100.0%	0.0%
#30	0.600		88%	100.0%	0.0%
#40	0.425	81%	81%	100.0%	0.0%
#50	0.300		44%	100.0%	0.0%
#60	0.250	29%	29%	100.0%	0.0%
#80	0.180		16%	100.0%	0.0%



0.0%

0.0%

0.0%

0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

10%

7%

5%

4.0%

100.0%

100.0%

100.0%

100.0%

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1322
Sample Date:	7/26/2021
Test Date:	8/24/2021
Technician:	M. Carrillo

Sample Source: LDW-GT24-5-13.6 ft

Visual Soil Description: brown sand with silt

Type of Specimen: Remolded Cylindrical Shear Box

Specimen Diameter (in): 2.5

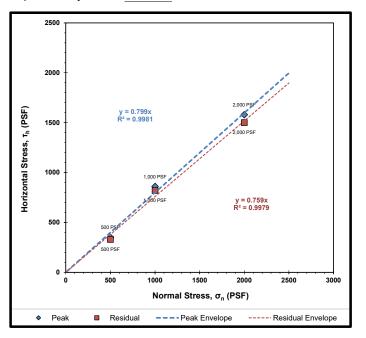
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample Data:		σ <sub>n</sub> =500 PSF		
Initial Moisture Content (%):	26.4			
	Initial	Post-Consolidation		
Dry Density (PCF):	108.1	108.3		
Void Ratio:	0.559	0.556		
Porosity (%):	35.9	35.7		
Degree of Saturation (%):	saturated	saturated		

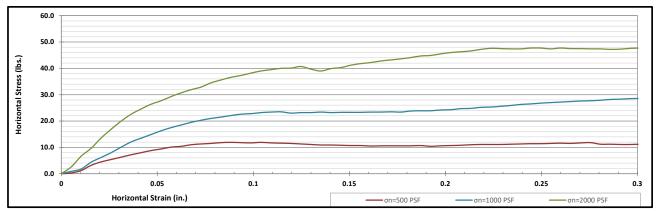
Summary of Sample	σ <sub>n</sub> =1000 PSF		
Initial Moisture Content (%):	al Moisture Content (%): 27.1		
	Initial	Post-Consolidation	
Dry Density (PCF):	107.4	109.3	
Void Ratio:	0.569	0.541	
Porosity (%):	36.3	35.1	
Degree of Saturation (%):	saturated	saturated	

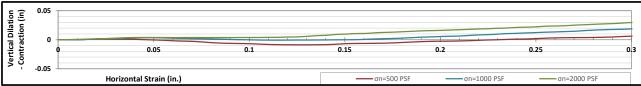
Summary of Sample Data:		σ <sub>n</sub> =2000 PSF		
Initial Moisture Content (%):	29.0			
	Initial	Post-Consolidation		
Dry Density (PCF):	105.6	108.6		
Void Ratio:	0.595	0.551		
Porosity (%):	37.3	35.5		
Degree of Saturation (%):	saturated	saturated		

ESTIMATED STRENGTH PARAMETERS								
PEAK RESIDUAL								
Angle of Internal Friction, φ (°):	39	37						
Cohesion (PSF):	0	0						



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF): 500 1000 2000							
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	350	860	1580				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	330	820	1500				





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT24-13.6-29 ft Sample#: B21-1323

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 24-Aug-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.091 \\ \textbf{D}_{(10)} = 0.163 \\ \textbf{D}_{(15)} = 0.201 \\ \textbf{D}_{(30)} = 0.292 \\ \textbf{D}_{(50)} = 0.389 \\ \textbf{D}_{(60)} = 0.457 \\ \textbf{D}_{(90)} = 0.815 \end{array}$ % Gravel = 0.0%% Sand = 95.9% mm % Silt & Clay = 4.1% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm

Sand Equivalent = n/a racture %, 1 Face = n/a aces = n/a

Coeff. of Curvature,  $C_C = 1.15$ Coeff. of Uniformity,  $C_U = 2.81$ Fineness Modulus = 1.94

Plastic Limit = 0.0% Moisture %, as sampled = 18.4% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.815$	mm	F	racture	%, 1	Fa
						ust Ratio = 1/14		Frac	cture %,	, 2+ I	Fac
			1-	AS	TM C136, AS	TM D6913, ASTM	C117				
		Actual Cumulative	Interpolated Cumulative						Grain Size		outio
Sieve	Size	Percent	Percent	Specs	Specs		ъ	7 3 3 <del>4</del> 5 2 3 <del>4</del> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	50 % ao	E. 44	œ <sup>2</sup>
US	Metric	Passing	Passing	Max	Min	10	- 0 0 0% <b>**</b> **	****	****	≥≟ Month	## Têê
12.00"	300.00		100%	100.0%	0.0%						
10.00"	250.00		100%	100.0%	0.0%						
8.00"	200.00		100%	100.0%	0.0%	9	0%			HH	H
6.00"	150.00		100%	100.0%	0.0%		ł l				
4.00"	100.00		100%	100.0%	0.0%		10%				
3.00"	75.00		100%	100.0%	0.0%	°	U76			Ш	П
2.50"	63.00		100%	100.0%	0.0%						
2.00"	50.00	100%	100%	100.0%	0.0%	7	10%			₩.	Ш
1.75"	45.00		100%	100.0%	0.0%						
1.50"	37.50		100%	100.0%	0.0%						
1.25"	31.50		100%	100.0%	0.0%	6	0% +			##	$\vdash$
1.00"	25.00	100%	100%	100.0%	0.0%	p p					
3/4"	19.00	100%	100%	100.0%	0.0%	Possing 8	0%				
5/8"	16.00		100%	100.0%	0.0%	P6 2	<sup>176</sup>			Ш	П
1/2"	12.50	100%	100%	100.0%	0.0%						
3/8"	9.50	100%	100%	100.0%	0.0%	4	10%	₩₩	4	Ш	Ш
1/4"	6.30		100%	100.0%	0.0%		11				
#4	4.75	100%	100%	100.0%	0.0%						
#8	2.36		100%	100.0%	0.0%	3	0%			###	$\vdash$
#10	2.00	99%	99%	100.0%	0.0%		1				
#16	1.18		95%	100.0%	0.0%		10%				
#20	0.850	93%	93%	100.0%	0.0%		<sup>176</sup> F	IIIIII		Ш	П
#30	0.600		72%	100.0%	0.0%						
#40	0.425	57%	57%	100.0%	0.0%	1	0%	+		Ш.	⇊
#50	0.300		32%	100.0%	0.0%						
#60	0.250	21%	21%	100.0%	0.0%						
#80	0.180		12%	100.0%	0.0%		0%	0.000	10.000	<b></b>	40
#100	0.150	8%	8%	100.0%	0.0%		100		10.000		
	0.106	1	50/	100.00/	0.00/	II			n.		

100.0%

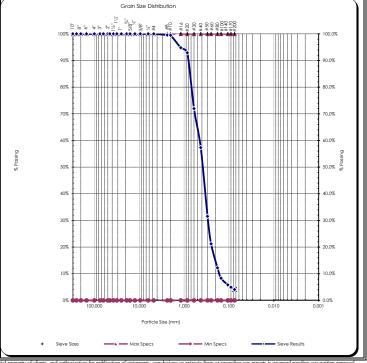
100.0%

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6%

5%

4.1%



Comments:			
	Soul Palacet and		

0.0%

0.0%

0.0%

Meghan Blodgett-Carrillo

4.1%

0.106

0.090

0.075

#140

#170

#200

Reviewed by:

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duv roject #: 21B233 Client: Anchor QEA Source: LDW-GT24-33-3: ample #: B21-1324	·	Sample Date T	eeived: 29-Jul-21 ed By: Client Cested: 25-Aug-21 ed By: C. Kriss	Sar Sar	ual Identific ndy Silt nple Color wn	ation
		Liquid Lim	it Determination				
		#1	#2 #	3 #4	#5	#6	
	Weight of Wet Soils + Pan:						
	Weight of Dry Soils + Pan:	Liquid L	imit cannot be establishe	d			
	Weight of Pan: Weight of Dry Soils:						Liquid Limit @ 25 Blows: N/A
	Weight of Moisture:						Plastic Limit: N/A
	% Moisture:						Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:						
		Plastic Lim	it Determination				
		#1		3 #4	#5	#6	
	Weight of Wet Soils + Pan:	DI di I		,			
	Weight of Dry Soils + Pan: Weight of Pan:	Plastic L	imit cannot be determine	d			
	Weight of Dry Soils:						ACCREDITED
	Weight of Moisture: % Moisture:						Certificate #: 1366.01, 1366.02 & 1366.04
_	% Moisture:						
		Plast	icity Chart			)	Liquid Limit
	<sup>70</sup> %						100% +
	60 %			"U" Line	, Lipe		90%
×	50 %			CHOrOH	WAX TO THE REAL PROPERTY OF THE PARTY OF THE		70%
Plasticity Index	40 %			CHO			Woishing 60%
sticity	30 %						<b>≥</b> 50% + 4
Plas	20 %	OL or Ot		MH or OH			30%
	10 % CL-ML	ML or OL		14111 01 011			20%
	0 % CL-IVIL	20% 30% 40%	50% 60%	70% 80%	90% 100%	110%	10%
	070 1070		quid Limit	7070 0070	3070 10070	11070	10 100 Number of Blows, "N"
	Copyright Spears Engineering & Tech	hnical Services PS, 1996-98					Number of Blows, 14
All manulan		1	11: 1 1 1	. 1 5 1 1 71		1 4 - 6 6	publication of statements, conclusions or extracts from or regarding

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA Source: LDW-GT24-35-43 ft

Sample#: B21-1325

#50

#60

#80 #100

#140

#170

#200

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 24-Aug-21

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

mm

gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

Sample Meets Specs ? N/A

 $\begin{array}{c} D_{(5)} = 0.042 \\ D_{(10)} = 0.082 \\ D_{(15)} = 0.114 \\ D_{(30)} = 0.175 \\ \end{array}$ % Gravel = 0.0%% Sand = 91.1% mm % Silt & Clay = 8.9% mm Liquid Limit = 0.0% mm  $D_{(50)} = 0.227$ mm Plasticity Index = 0.0%  $D_{(60)} = 0.257$   $D_{(90)} = 0.414$ mm Sand Equivalent = n/a

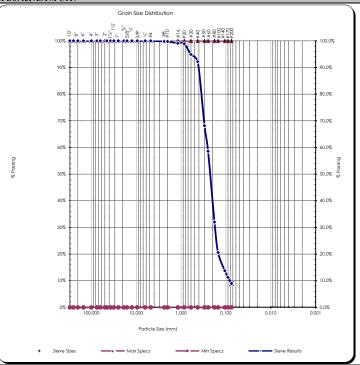
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.45$ Coeff. of Uniformity,  $C_U = 3.14$ Fineness Modulus = 1.17 Plastic Limit = 0.0% Moisture %, as sampled = 27.3%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

ASTM C136, ASTM D6913, ASTM C117	

						2(90)	0
						ust Ratio =	3/31
			T	AS	TM C136, AS	TM D6913,	ASTM
		Actual	Interpolated				
		_	Cumulative		1		
	e Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		1
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%	20	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	
5/8"	16.00		100%	100.0%	0.0%	96	
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		100%	100.0%	0.0%		
#10	2.00	100%	100%	100.0%	0.0%		
#16	1.18		99%	100.0%	0.0%		
#20	0.850	99%	99%	100.0%	0.0%		
#30	0.600		95%	100.0%	0.0%		
#40	0.425	92%	92%	100.0%	0.0%		



0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

59%

8.9%

68%

59%

32%

21%

14%

11%

8.9%

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Pı	Project: Q.C Lower Duv roject #: 21B233 Client: Anchor QEA Source: LDW-GT24-43-50 ample #: B21-1326	•	Date Received Sampled By Date Tested Tested By	: Client : 25-Aug-21	Silty San	al Identific Sand ple Color brown	ation	
			Determination					
	Weight of Wet Soils + Pan:	#1	#2 #3	#4	#5	#6		
	Weight of Dry Soils + Pan:	Liquid Lim	it cannot be established					
	Weight of Pan: Weight of Dry Soils:						Liquid Limit @ 25 Blows: N/A	A
	Weight of Moisture:						Plastic Limit: N/A Plasticity Index, I <sub>P</sub> : N/A	
	% Moisture: Number of Blows:						riasucity index, Ip: N/A	A
		Plastic Limit	Determination #2 #3	#4	#5	#6		
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan: Weight of Pan:	Plastic Lin	it cannot be determined					
	Weight of Dry Soils: Weight of Moisture:						ACCREDITED	
	% Moisture:						Certificate #: 1366.01, 1366.02 & 1366.04	
		Plastic	ity Chart					
	<sup>70 %</sup> T	i iastic	i – –				Liquid Limit	٦
	60 %			J' Line	, Lipe		90%	
	50 %			OH _	MAN LAKE		80%	
Plasticity Index	40 %		C)	TorOH			70% true	
city	30 %						60% 60% 50%	
lasti	20 %	ot					40%	
_		OL or OL		ЛH or OH			30%	
	10 % CL-ML	ML or OL					10%	
	0 % 10%	20% 30% 40%	50% 60% 70%	80%	90% 100%	110%	0%	-
		Liqu	id Limit				Number of Blows, "N"	00
	Copyright Spears Engineering & Tech	unical Services PS, 1996-98						

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT24-53.3-59 ft Sample#: B21-1327

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 24-Aug-21 Tested By: A. Eifrig

Visual Identification Sandy Silt Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

#50

#60

#80 #100

#140

#170

#200

Sample Meets Specs? N/A

 $D_{(5)} = 0.007$   $D_{(10)} = 0.014$   $D_{(15)} = 0.021$ % Gravel = 0.0%% Sand = 46.3% mm % Silt & Clay = 53.7% mm  $D_{(30)} = 0.042$ Liquid Limit = n/a mm  $D_{(50)} = 0.070$ mm Plasticity Index = n/a  $D_{(60)} = 0.088$ mm Sand Equivalent = n/a  $D_{(90)} = 0.161$ mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.42$ Coeff. of Uniformity,  $C_U = 6.33$ Fineness Modulus = 0.15

Plastic Limit = n/a Moisture %, as sampled = 33.1% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					-	D(90)	0.1
				_ 46	STM C136, AS	ust Ratio =	4.5
		Actual	Interpolated	Ac	51 W C130, AS	IMI D0913,	AS
		Cumulative	Cumulative				
Sieve	Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		
12.00"	300.00		100%	100.0%	0.0%	1	
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%	2	
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	
5/8"	16.00		100%	100.0%	0.0%	96	
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		100%	100.0%	0.0%		
#10	2.00	100%	100%	100.0%	0.0%		
#16	1.18		100%	100.0%	0.0%		
#20	0.850	100%	100%	100.0%	0.0%		
#30	0.600		99%	100.0%	0.0%		
#40	0.425	99%	99%	100.0%	0.0%		

98%

97%

92%

89%

68%

61%

53.7%

97%

53.7%

100.0%

100.0%

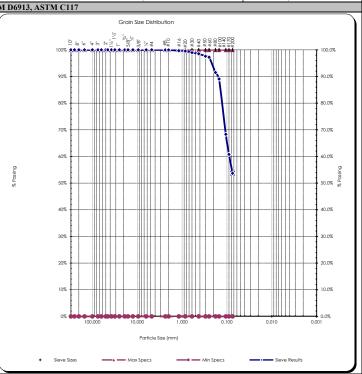
100.0%

100.0%

100.0%

100.0%

100.0%



**Comments:** Reviewed by: \_

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT36-3.6-6.2 ft Sample#: B21-1329

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 24-Aug-21 Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.016$   $D_{(10)} = 0.055$   $D_{(15)} = 0.058$   $D_{(30)} = 0.069$ % Gravel = 8.6% % Sand = 52.0% mm % Silt & Clay = 39.4% mm Liquid Limit = n/a mm  $D_{(50)} = 0.106$ mm Plasticity Index = n/a  $D_{(60)} = 0.135$ mm  $D_{(90)} = 4.129$ Dust Ratio = 39/80 mm

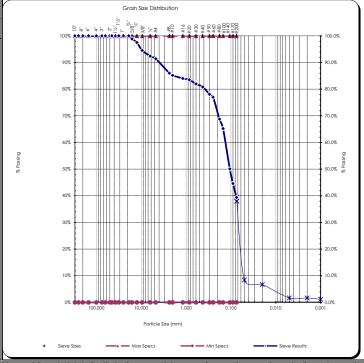
Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 0.64$ Coeff. of Uniformity,  $C_U = 2.46$ Fineness Modulus = 1.19

Plastic Limit = n/a Moisture %, as sampled = 15.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Req'd Fracture %, 2+ Faces =

	Du	ot reatio	37/00	Tracture 70, 2 - Taces III a	recqu	110
AS	TM C136, AST	M D6913	, ASTM C11	7		
				Grain Size Distribution		
	Specs Min			2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	98	·
	0.0%		1			
	0.0%		ţ			
	0.0%		90%		###	+

				AS	1 M C130, AS1
		Actual	Interpolated		
			Cumulative		
	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		99%	100.0%	0.0%
1/2"	12.50	98%	98%	100.0%	0.0%
3/8"	9.50	95%	95%	100.0%	0.0%
1/4"	6.30		92%	100.0%	0.0%
#4	4.75	91%	91%	100.0%	0.0%
#8	2.36		86%	100.0%	0.0%
#10	2.00	85%	85%	100.0%	0.0%
#16	1.18		84%	100.0%	0.0%
#20	0.850	84%	84%	100.0%	0.0%
#30	0.600		82%	100.0%	0.0%
#40	0.425	81%	81%	100.0%	0.0%
#50	0.300		78%	100.0%	0.0%
#60	0.250	77%	77%	100.0%	0.0%
#80	0.180		69%	100.0%	0.0%
#100	0.150	65%	65%	100.0%	0.0%
#140	0.106		50%	100.0%	0.0%
#170	0.090		45%	100.0%	0.0%
#200	0.075	39.4%	39.4%	100.0%	0.0%



Meghan Blodgett-Carrillo

Reviewed by:



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 24-Aug-21 Sample Color **Source:** LDW-GT36-3.6-6.2 ft Tested By: A. Eifrig brown Sample#: B21-1329 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 50.78 **Grain Size Distribution** 0.57% Soils Particle Hydroscopic Moist .: Sieve Percent ACCREDITED Adj. Sample Wgt: 50.49 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 31.500 mm Minutes Reading Passing 100% Diameter 0.0537 mm 100% 25.000 mm 8 4% 1.0" 8.4% 3/4" 19.000 mm 2 0.0380 mm 100% 8.4%  $0.0240 \ mm$ 5/8" 99% 16.000 mm 12.500 mm 15 2.5 4.2%  $0.0141 \ mm$ 1/2" 98% 30 1.7% 0.0100 mm 3/8" 95% 9.500 mm 0.0071 mm 60 1.7% 1/4" 92% 6.300 mm 240 1.7% 0.0035 mm 91% 4.750 mm #4 #10  $2.000\ mm$ 1440 1.7%  $0.0014 \ mm$ 85% #20 84%  $0.850 \ mm$ Liquid Limit: n/a % Gravel: 8.6% #40 81%  $0.425 \, mm$ % Sand: 52.0% Plastic Limit: n/a #100 65% 0.150 mm % Silt: 37.7% Plasticity Index: n/a #200 39.4%  $0.075 \ mm$ 38.0% 0.074 mm % Clay: 1.7% Silts 8.4% 0.050 mm 0.020 mm 6.7% 1.7% 0.005 mm Clays 1.7%  $0.002\ mm$ Colloids 1.2%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by:

Meghan Blodgett-Carrillo

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1329
Sample Date:	7/26/2021
Test Date:	8/26/2021
Technician:	M. Carrillo

 Sample Source:
 LDW-GT36-3.6-6.2 ft

 Visual Soil Description:
 brown silty sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

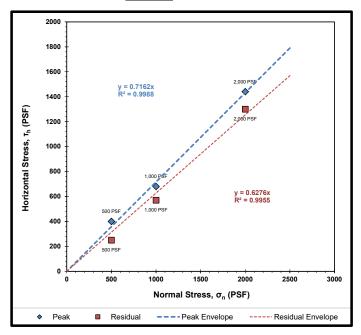
 Specimen Diameter (in):
 2.5

Summary of Sampl	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	19.8	
	Initial	Post-Consolidation
Dry Density (PCF):	114.5	115.4
Void Ratio:	0.472	0.460
Porosity (%):	32.1	31.5
Degree of Saturation (%):	saturated	saturated

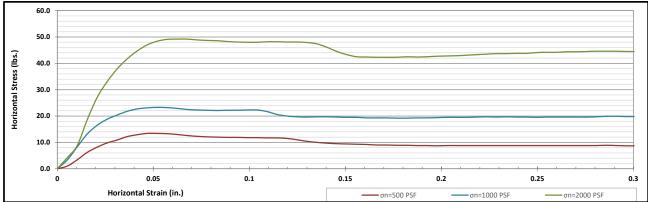
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	20.2	
	Initial	Post-Consolidation
Dry Density (PCF):	115.0	117.1
Void Ratio:	0.465	0.439
Porosity (%):	31.7	30.5
Degree of Saturation (%):	saturated	saturated

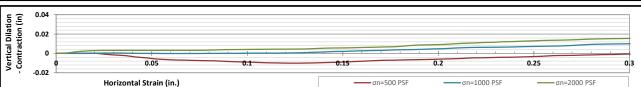
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	19.0	
	Initial	Post-Consolidation
Dry Density (PCF):	115.4	120.1
Void Ratio:	0.460	0.403
Porosity (%):	31.5	28.7
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS				
	PEAK	RESIDUAL		
Angle of Internal Friction, φ (°):	36	32		
Cohesion (PSF):	0	0		



Failure Envelope Test Values:					
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000		
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	400	680	1440		
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	250	570	1300		





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT36-6.2-9.5 ft Sample#: B21-1330

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 24-Aug-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#10 #16

#20

#30

#40 #50

#60

#80 #100

#140

#170

#200

Sample Meets Specs? N/A

 $D_{(5)} = 0.017$   $D_{(10)} = 0.035$   $D_{(15)} = 0.052$ % Gravel = 0.0%% Sand = 78.4% mm % Silt & Clay = 21.6% mm  $D_{(30)} = 0.092$ Liquid Limit = n/a mm  $D_{(50)} = 0.132$ mm Plasticity Index = n/a  $D_{(60)} = 0.152$ mm  $D_{(90)} = 0.240$ ust Ratio =  $\frac{7}{32}$ 

mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 1.59$ Coeff. of Uniformity,  $C_U = 4.38$ Fineness Modulus = 0.47

Plastic Limit = n/a Moisture %, as sampled = 27.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				4.6	Di
		Actual Cumulative	Interpolated Cumulative	AS	STM C136, AST
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00	1	100%	100.0%	0.0%
8.00"	200.00	1	100%	100.0%	0.0%
6.00"	150.00	1	100%	100.0%	0.0%
4.00"	100.00	1	100%	100.0%	0.0%
3.00"	75.00	1	100%	100.0%	0.0%
2.50"	63.00	1	100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50	1	100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00	1	100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30	1	100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2 36	1	100%	100.0%	0.0%

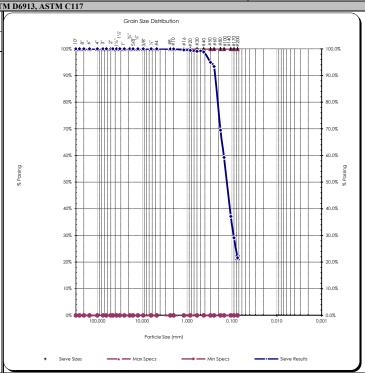
100%

99%

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93%

21.6%



**Comments:** Reviewed by: Meghan Blodgett-Carrillo

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100%

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

Meghan Blodgett-Carrillo

7.1%

Source: LDW-GT36-11.7-32 ft Sample#: B21-1332

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 24-Aug-21 Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = \textbf{0.053} \\ \textbf{D}_{(10)} = \textbf{0.129} \\ \textbf{D}_{(15)} = \textbf{0.186} \\ \textbf{D}_{(30)} = \textbf{0.285} \\ \textbf{D}_{(50)} = \textbf{0.368} \\ \textbf{D}_{(60)} = \textbf{0.410} \\ \textbf{D}_{(90)} = \textbf{0.738} \end{array}$ % Gravel = 0.0%% Sand = 92.9% mm % Silt & Clay = 7.1% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm

Sand Equivalent = n/a racture %, 1 Face = n/a ces = n/a Coeff. of Curvature,  $C_C = 1.53$ Coeff. of Uniformity,  $C_U = 3.18$ Fineness Modulus = 1.77

Plastic Limit = n/a Moisture %, as sampled = 15.7% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.738$	mm	F	racture 9	%, 1	Fac
						ust Ratio = 1/9		Frac	cture %,	2+ F	ace
				AS	STM C136, AST	ГМ D6913, ASTM	I C117				
		Actual	Interpolated						Grain Size	Distrib	utio
		_	Cumulative		T						
	eve Size	Percent	Percent	Specs	Specs		ما ما ف	7 3 3 <del>4</del> 5 3 <del>4</del> 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	. os ~os	€+ <del>**</del>	<sub>φ</sub> 2
US	Metric	Passing	Passing	Max	Min		100%			n i	-4.0
12.00"	300.00		100%	100.0%	0.0%						.
10.00"	250.00		100%	100.0%	0.0%						.
8.00"	200.00		100%	100.0%	0.0%		90%		+-+++++++++++++++++++++++++++++++++++		
6.00"	150.00		100%	100.0%	0.0%		11				.
4.00"	100.00		100%	100.0%	0.0%		80%			Ш	
3.00"	75.00		100%	100.0%	0.0%						.
2.50"	63.00		100%	100.0%	0.0%		- [ ]				.
2.00"	50.00	100%	100%	100.0%	0.0%		70%		+-+++++++++++++++++++++++++++++++++++	Ш	$\dashv$
1.75"	45.00		100%	100.0%	0.0%						. 1
1.50"	37.50		100%	100.0%	0.0%						.
1.25"	31.50		100%	100.0%	0.0%		60%				_
1.00"	25.00	100%	100%	100.0%	0.0%	2	ł I				.
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				.
5/8"	16.00		100%	100.0%	0.0%	₩.	30%				П
1/2"	12.50	100%	100%	100.0%	0.0%						.
3/8"	9.50	100%	100%	100.0%	0.0%		40%			Ш	_
1/4"	6.30		100%	100.0%	0.0%						.
#4	4.75	100%	100%	100.0%	0.0%		- 11				.
#8	2.36		100%	100.0%	0.0%		30%		+-++		-
#10	2.00	100%	100%	100.0%	0.0%		- 1				. 1
#16	1.18		100%	100.0%	0.0%		20%				.
#20	0.850	99%	99%	100.0%	0.0%		20%				П
#30	0.600		78%	100.0%	0.0%						
#40	0.425	64%	64%	100.0%	0.0%		10%		4-4	Щ	_
#50	0.300		34%	100.0%	0.0%						
#60	0.250	22%	22%	100.0%	0.0%						.
#80	0.180		14%	100.0%	0.0%		0%	000.00	10.000	للواو	-00
#100	0.150	11%	11%	100.0%	0.0%		10	0.000	10.000		

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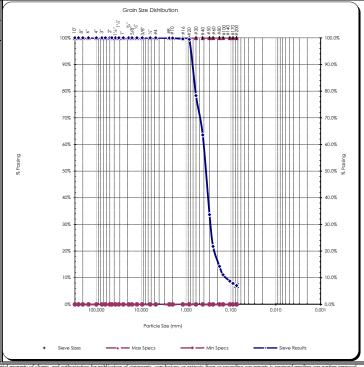
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Comments:			
	Magh Baket aillo		
Reviewed by:	" (Maja Delaya Cara 2		

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duwa roject #: 21B233 Client: Anchor QEA Source: LDW-GT36-32-34. ample #: B21-1333	·			Sand	al Identification  with Silt  ple Color  n	on	
		Liquid Lim	it Determination					
		#1	#2 #3	#4	#5	#6		
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan:	Liquid L	mit cannot be established					
	Weight of Pan:						Limit Limit @ 25 Bloom	
	Weight of Dry Soils: Weight of Moisture:						Liquid Limit @ 25 Blows: N/A Plastic Limit: N/A	
	% Moisture:						Plasticity Index, I <sub>P</sub> : N/A	
	Number of Blows:							
			t Determination					
	Weight of Wet Soils + Pan:	#1	#2 #3	#4	#5	#6		
	Weight of Dry Soils + Pan:	Plastic L	imit cannot be determined					
	Weight of Pan:							
	Weight of Dry Soils: Weight of Moisture:						ACCREDITED  Certificate #: 1366.01, 1366.02 & 1366.04	
	% Moisture:							
		Diset	icity Chart					
	70 % <b>F</b>	Plast	City Chart				Liquid Limit	
	60 %			"U" Line	" Lipe		90%	
×e	50 %			HorOH	Marie .		80%	
/ Inde	40 %		1 9	n'			% Woisture 60%	
Plasticity Index	30 %						<b>X</b> 50% 40%	
Plas	20 %	CLorOt		MH or OH			30%	
	10 %			VIII OI OII			20%	
	0 % CL-ML 10%	ML or OL	50% 60% 70	% 80%	90% 100%	110%	10%	
	070 1070 2		uid Limit	,o 00 /o	3070 10070	11070	10 Number of Blows, "N"	00
	Copyright Spears Engineering & Techni						Nulliber of blows, N	
4.11	apply only to actual locations and materials				ial property of clients, and	1 1 2 6 11		

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Meghan Blodgett-Carrillo

Corporate ~ 777 Chrysler Drive • Burlington, WA 98233 • Phone (360) 755-1990 • Fax (360) 755-1980

**Regional Offices:** Olympia ~ 360.534.9777 Bellingham ~ 360.647.6111 Silverdale ~ 360.698.6787 Tukwila ~ 206.241.1974 Visit our website: www.mtc-inc.net



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW-GT36-34.7-50 ft Sample#: B21-1334

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 24-Aug-21 Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP-SM, Poorly graded Sand with Silt

Sample Color: grayish-brown

mm



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Space

#170

#200

0.090

0.075

Sample Meets Specs? N/A

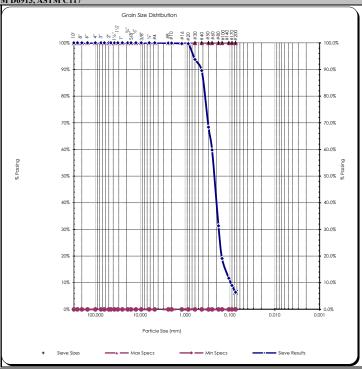
 $D_{(5)} = 0.058$   $D_{(10)} = 0.096$   $D_{(15)} = 0.126$   $D_{(30)} = 0.177$ % Gravel = 0.0%% Sand = 93.5% mm % Silt & Clay = 6.5% mm Liquid Limit = n/a mm  $D_{(50)} = 0.226$ mm Plasticity Index = n/a  $D_{(60)} = 0.251$ mm Sand Equivalent = n/a

Coeff. of Curvature,  $C_C = 1.30$ Coeff. of Uniformity,  $C_U = 2.62$ Fineness Modulus = 1.19 Plastic Limit = n/a Moisture %, as sampled = 23.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

 $D_{(90)} = 0.441$ Oust Ratio = 6/83 Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a TM D6913, ASTM C117

- 1	eq a riactare 70, r race
Req	'd Fracture %, 2+ Faces =

			Tr . 1 . 1	AS	TM C136,
		Actual	Interpolated		
		Percent	Cumulative	_	
	Sieve Size		Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		100%	100.0%	0.0%
#20	0.850	100%	100%	100.0%	0.0%
#30	0.600	10070	94%	100.0%	0.0%
#40	0.425	90%	90%	100.0%	0.0%
#50	0.300	,370	68%	100.0%	0.0%
#60	0.250	60%	60%	100.0%	0.0%
#80	0.180	0070	31%	100.0%	0.0%
#100	0.150	19%	19%	100.0%	0.0%
#140	0.106	1970	12%	100.0%	0.0%
#1 <b>4</b> 0	0.100		12/0	100.070	0.076



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**Comments:** Reviewed by: Meghan Blodgett-Carrillo

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# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

	Liquid I	imit Determinat	ion				
	#l	#2	#3	#4	#5	#6	
Weight of Wet Soils + Pan:	29.50	30.28	27.77				
Weight of Dry Soils + Pan:	26.95	27.50	24.20				
Weight of Pan: Weight of Dry Soils:	19.61 7.34	19.98 7.52	14.98 9.22				Liquid Limit @ 25 Blows: 36 9
Weight of Moisture:	2.55	2.78	3.57				Plastic Limit: 25 9
% Moisture:	34.7 %	37.0 %	38.7 %				Plasticity Index, I <sub>P</sub> : 11 °
Number of Blows:	30	21	11				• , •
		imit Determinat		1/4	115		
Weight of Wet Soils + Pan:	#1 34.74	#2 35.86	#3	#4	#5	#6	
Weight of Dry Soils + Pan:	33.48	35.86					
Weight of Pan:	28.53	28.24					
Weight of Dry Soils:	4.95	6.08					ACCREDITED
Weight of Moisture:	1.26	1.54					Certificate #: 1366.01, 1366.02 & 1366.04
% Moisture:	25.5 %	25.3 %					
	Pla	sticity Chart					
<sup>70</sup> % T							Liquid Limit
60 %				The			
100 10			, il	E.C.	WHIRE		40%
50 % 🛔				or OH	MAN TO THE REAL PROPERTY OF THE PARTY OF THE		35%
E I		/   /	-14	or			2 30%
40 % {			9				25% - 25% -
30 %							
50 %							× 20% =
20 %	Chorot						15%
	\Q\0		M	H or OH			10%
10 %		1					5% =
CL-ML	ML or OL	1					
CL-ML		50% 6	0% 70%	80%	90% 10	00% 110%	0% +
CL-ML	% 30% 40%		0% 70%	80%	90% 10	00% 110%	
CL-ML	% 30% 40%	50% 6	70%	80%	90% 10	00% 110% 	

Meghan Blodgett-Carrillo

Corporate ~ 777 Chrysler Drive • Burlington, WA 98233 • Phone (360) 755-1990 • Fax (360) 755-1980

**Regional Offices:** Olympia ~ 360.534.9777 Bellingham ~ 360.647.6111 Silverdale ~ 360.698.6787 Tukwila ~ 206.241.1974 Visit our website: www.mtc-inc.net



Client:	Anchor QEA	Date:	September 29, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1447 - 1466
Revised on:		Date sampled:	7-8-21 & 7-9-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



## **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 31, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1447	LDW21-GT21-GB-31-32.5 ft	222.3	700.9	590.1	110.8	367.8	30.1%
B21-1448	LDW21-GT12-GB-0-1.5 ft	208.8	636.4	466.8	169.6	258.0	65.7%
B21-1449	LDW21-GT12-GB-0-12 ft	224.0	851.3	609.9	241.4	385.9	62.6%
B21-1450	LDW21-GT12-GB-12-13.5 ft	233.8	567.3	458.5	108.8	224.7	48.4%
B21-1451	LDW21-GT12-GB-18-22 ft	222.9	780.0	643.4	136.6	420.5	32.5%
B21-1452	LDW21-GT12-GB-22-23.5 ft	229.4	723.2	606.3	116.9	376.9	31.0%
B21-1453	LDW21-GT11-GB-0-1.5 ft	221.8	617.6	440.0	177.6	218.2	81.4%
B21-1454	LDW21-GT11-GB-0-8.5 ft	233.8	686.2	473.2	213.0	239.4	89.0%
B21-1455	LDW21-GT11-GB-8.5-10 ft	224.8	616.6	455.4	161.2	230.6	69.9%
B21-1456	LDW21-GT11-GB-8.5-16.7 ft	182.3	495.3	374.9	120.4	192.6	62.5%
B21-1457	LDW21-GT11-GB-16.7-18.5 ft	186.7	993.2	821.5	171.7	634.8	27.0%
B21-1458	LDW21-GT11-GB-18.5-20 ft	220.1	643.5	566.8	76.7	346.7	22.1%
B21-1459	LDW21-GT9-GB-0-1.5 ft	221.4	388.1	331.3	56.8	109.9	51.7%
B21-1460	LDW21-GT9-GB-10-11.5 ft	225.6	534.4	429.8	104.6	204.2	51.2%
B21-1461	LDW21-GT9-GB <del>-16-20 ft</del>	225.7	665.4	521.2	144.2	295.5	48.8%
B21-1462	LDW21-GT9-GB-20-21.5 ft	235.5	299.4	285.9	13.5	50.4	26.8%
B21-1463	LDW21-GT7-GB-0-1.5 ft	301.1	545.2	480.4	64.8	179.3	36.1%
B21-1464	LDW21-GT7-GB-0-5.7 ft	182.9	988.2	806.6	181.6	623.7	29.1%
B21-1465	LDW21-GT7-GB-8.5-10 ft	217.2	591.3	504.5	86.8	287.3	30.2%
B21-1466	LDW21-GT7-GB-8.5-18.5 ft	233.4	693.2	578.2	115.0	344.8	33.4%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: August 31, 2021	Tested by: A. Eifrig

Sample # B21-1449 B21-1451	Location LDW21-GT12-GB-0-12 ft LDW21-GT12-GB-18-22 ft	Tare 493.02 497.56	Tare 545.53 597.70	Mass of Dry Soil 52.5 100.1	Pycno ID TSA-012 TSA-023	Mass of Pycno 180.4 163.9	Volume of Pycno 499.5 498.7	Water @ Tx 0.99749 0.99749	w/ water & soils 742.00 723.96	w/ water 709.46 661.41	Water, 0.1 *C 23.2 23.2	SpG of Soils 2.6294442 2.6641366	Factor 0.99929 0.99929	Corrected SpG 2.6275773 2.6622451
B21-1459	LDW21-GT9-GB-0-1.5 ft	601.92	676.89	75.0	TSA-015	187.6	499.5	0.99749	732.66	685.85		2.6626339		2.6607434
B21-1461	LDW21-GT7-GB-0-5.7 ft	502.15	601.95	99.8	TSA-021	183.4	499.4	0.99749	744.55	681.58	23.2	2.7100064	0.99929	2.7080823
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Il results apply only to actual locations and materials tested.	As a mutual protection to clients, the public and ourselves, all re	ports are submitted as the confidential property of clients, a	nd authorization for publication of statements, conclusions	s or extracts from or regarding our reports is reserved p	inding our written approval.
1	//				

Reviewed by:

Meghan Blodgett-Carrillo



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Visual Identification Date Received: 29-Jul-21 Clayey Silt with Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT12-GB-0-12 ft Tested By: C. Kriss brown Sample #: B21-1449 **Liquid Limit Determination** Weight of Wet Soils + Pan: Liquid limit cannot be established Weight of Dry Soils + Pan: Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CLOrOL 20.0 % MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98
All results apply only to actual locations and materials tested. As a mutual protest

clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statem

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT12-GB-18-22 ft Sample#: B21-1451

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 31-Aug-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

ASTM C136, ASTM D6913, ASTM C117

Specifications No Specs

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

39%

19.3%

#80

#140

#170

#200

Sample Meets Specs? N/A

Actual

 $\begin{array}{c} D_{(5)} = 0.010 \\ D_{(10)} = 0.035 \\ D_{(15)} = 0.062 \\ D_{(30)} = 0.115 \\ D_{(30)} = 0.128 \end{array}$ % Gravel = 0.2% % Sand = 80.4% mm % Silt & Clay = 19.3% mm Liquid Limit = 0.0% mm  $D_{(50)} = 0.188$ mm Plasticity Index = 0.0%  $D_{(60)} = 0.222$ mm Sand Equivalent = n/a  $D_{(90)} = 0.417$ Dust Ratio = 7/33 mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.73$ Coeff. of Uniformity,  $C_U = 6.41$ Fineness Modulus = 0.95

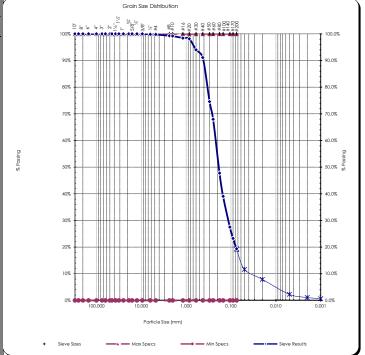
Plastic Limit = 0.0% Moisture %, as sampled = 32.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

Specs	Specs
Max	Min
100.0%	0.0%
100.0%	0.0%
100.0%	0.0%
100.0%	0.0%
100.0%	0.0%
100.0%	0.0%
100.0%	0.0%

		Cumulative	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		99%	100.0%	0.0%
#10	2.00	99%	99%	100.0%	0.0%
#16	1.18		98%	100.0%	0.0%
#20	0.850	98%	98%	100.0%	0.0%
#30	0.600		94%	100.0%	0.0%
#40	0.425	91%	91%	100.0%	0.0%
#50	0.300		75%	100.0%	0.0%
#60	0.250	68%	68%	100.0%	0.0%

Interpolated



0.0%

0.0%

0.0%

0.0%

0.0%

**Comments:** Reviewed by:

48%

39%

28%

23%

19.3%

100.0%

100.0%

100.0%

100.0%

100.0%



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SM, Silty Sand Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT12-GB-18-22 ft Tested By: C. Kriss brown Sample#: B21-1451 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: Sieve Analysis 2.66 Sample Weight: 102.98 **Grain Size Distribution** Hydroscopic Moist.: 1.38% Soils Particle Sieve Percent ACCREDITED Passing Adj. Sample Wgt: 101.58 grams Size Diameter 75.000 mm 3.0" 100% 2.0" 100% 50.000 mm Hydrometer Soils Particle 37.500 mm 1.5" 100% Reading Corrected Percent 1.25" 31.500 mm 100% Minutes Reading **Passing** Diameter 0.0516 mm 100% 25.000 mm 11.7% 1.0" 0.0370 mm 10.3% 3/4" 10.5 100% 19.000 mm 0.0235 mm 5 9 8.8% 5/8" 100% 16.000 mm 15 6.5 6.3%  $0.0138\ mm$ 1/2" 100% 12.500 mm 30 5 4 9%  $0.0098\ mm$ 3/8" 100% 9.500 mm 60 3.5 3.4% $0.0070\ mm$ 1/4" 100% 6.300 mm 240 1.5 1.5%  $0.0035 \ mm$ #4 100% 4.750 mm 1440 1.0%  $0.0014\ mm$ #10 99% 2.000 mm 0.850 mm #20 98% % Gravel: 0.2% Liquid Limit: 0.0 % #40 0.425 mm % Sand: 80.4% Plastic Limit: 0.0 % #100 39% 0.150 mm % Silt: 17.1% Plasticity Index: 0.0 % #200 19.3% 0.075 mm 0.074 mm % Clay: 2.3% Silts 19.0% 0.050 mm 11.7% 7.9% 0.020 mm 2.3% 0.005 mm Clavs 0.002 mm 1.1% Colloids 0.7% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding **Comments:** 

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1451
Sample Date:	7/8/2021
Test Date:	8/23/2021
Technician:	M. Carrillo

| Sample Source: LDW21-GT12-GB-18-22 ft |
| Visual Soil Description: brown clayey silt |
| Type of Specimen: Remolded Cylindrical Shear Box |
| Specimen Diameter (in): 2.5

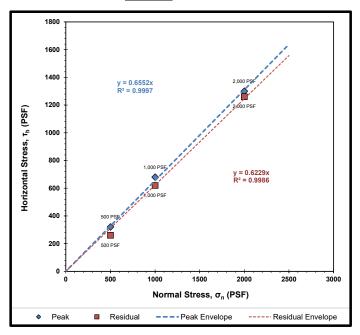
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%):	34.3		
	Initial	Post-Consolidation	
Dry Density (PCF):	104.7	112.4	
Void Ratio:	0.609	0.499	
Porosity (%):	37.9	33.3	
Degree of Saturation (%):	saturated	saturated	

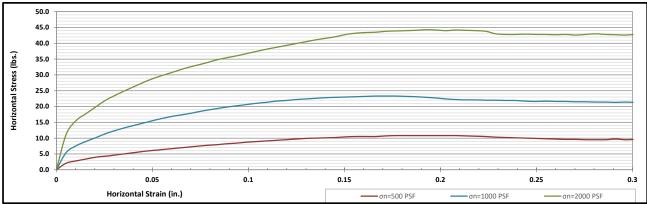
Summary of Sample	σ <sub>n</sub> =1000 PSF	
Initial Moisture Content (%):	32.5	
	Initial	Post-Consolidation
Dry Density (PCF):	106.6	117.5
Void Ratio:	0.580	0.433
Porosity (%):	36.7	30.2
Degree of Saturation (%):	saturated	saturated

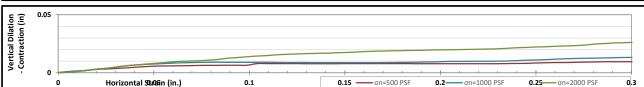
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	34.7	
	Initial	Post-Consolidation
Dry Density (PCF):	104.7	119.6
Void Ratio:	0.609	0.409
Porosity (%):	37.8	29.0
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS						
	PEAK	RESIDUAL				
Angle of Internal Friction, φ (°):	33	32				
Cohesion (PSF):	0	0				



Failure Envelope Test Values:						
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000			
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	320	680	1300			
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	260	620	1260			





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT11-GB-0-8.5 ft Sample#: B21-1454

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 31-Aug-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

ML, Sandy Silt Sample Color:

brown



30.0%

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM P43} \\ \textbf{D}_{(1)} = 0.004 \\ \textbf{D}_{(10)} = 0.007 \\ \textbf{D}_{(15)} = 0.010 \\ \textbf{D}_{(30)} = 0.041 \\ \textbf{D}_{(50)} = 0.063 \\ \textbf{D}_{(60)} = 0.069 \\ \textbf{D}_{(90)} = 0.146 \end{array}$ % Gravel = 0.0%% Sand = 31.3% mm % Silt & Clay = 68.7% mm Liquid Limit = 40.6% mm Plasticity Index = 0.0% mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 3.47$ Coeff. of Uniformity,  $C_U = 9.80$ Fineness Modulus = 0.14

Plastic Limit = 0.0% Moisture %, as sampled = 89.0% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

re %, 2+ Faces =

						$D_{(90)} = 0.146$		Fracture %, 1 Face = n/a Req'd Fra	
						ust Ratio = $68/9$		Fracture %, 2+ Faces = n/a Req'd Fract	ure
				AS	TM C136, AST	TM D6913, AST	M C117		
		Actual	Interpolated					Grain Size Distribution	
		7	Cumulative	_	_	4		÷ .	
	Size	Percent	Percent	Specs	Specs			6 6' 3' 3' 3' 3' 3' 3' 3' 3' 3' 3' 3' 3' 3'	
US 12.00"	Metric 300.00	Passing	Passing 100%	Max 100.0%	Min 0.0%	4	100%		Ш
10.00"	250.00		100%	100.0%	0.0%				
8.00"	200.00		100%	100.0%	0.0%		90%		Ш
6.00"	150.00		100%	100.0%	0.0%				
4.00"	100.00		100%	100.0%	0.0%		ł I		
3.00"	75.00		100%	100.0%	0.0%		80%	<u>\</u>	
2.50"	63.00		100%	100.0%	0.0%				
2.00"	50.00	100%	100%	100.0%	0.0%		70%		
1.75"	45.00	10070	100%	100.0%	0.0%		/0%		
1.50"	37.50		100%	100.0%	0.0%				
1.25"	31.50		100%	100.0%	0.0%		60%		
1.00"	25.00	100%	100%	100.0%	0.0%	g.			
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing			
5/8"	16.00		100%	100.0%	0.0%	₩.	50%		-##
1/2"	12.50	100%	100%	100.0%	0.0%				
3/8"	9.50	100%	100%	100.0%	0.0%		40%		Ш
1/4"	6.30		100%	100.0%	0.0%				
#4	4.75	100%	100%	100.0%	0.0%			*	
#8	2.36		100%	100.0%	0.0%		30%	<del></del>	-##
#10	2.00	100%	100%	100.0%	0.0%		ł I		
#16	1.18		99%	100.0%	0.0%		20%		
#20	0.850	99%	99%	100.0%	0.0%		20,0		V
#30	0.600		98%	100.0%	0.0%				N
#40	0.425	98%	98%	100.0%	0.0%		10%		-#}
#50	0.300		97%	100.0%	0.0%				
#60	0.250	96%	96%	100.0%	0.0%		<u> </u>		
#80	0.180		93%	100.0%	0.0%		0%	100.000 10.000 1.000 0.100 0	0.010
#100	0.150	91%	91%	100.0%	0.0%				
#140	0.106		78%	100.0%	0.0%			Particle Size (mm)	
#170	0.090		73%	100.0%	0.0%				

0.0%

#200

Reviewed by:

Meghan Blodgett-Carrillo

68.7%

68.7%

100.0%

0.075



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client ML, Sandy Silt Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT11-GB-0-8.5 ft Tested By: C. Kriss brown Sample#: B21-1454 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: Sieve Analysis 2.65 53.60 Sample Weight: **Grain Size Distribution** Hydroscopic Moist.: 4.63% Soils Particle Sieve Percent 51.23 Passing Adj. Sample Wgt: grams Size Diameter 75.000 mm 3.0" 100% 2.0" 100% 50.000 mm Hydrometer Soils Particle 37.500 mm 1.5" 100% Reading Corrected Percent 1.25" 31.500 mm 100% Minutes Reading **Passing** Diameter 0.0505 mm 100% 25.000 mm 31.2% 1.0" 29.3% 0.0359 mm 3/4" 15 100% 19.000 mm 5 14 27.3%  $0.0228\ mm$ 5/8" 100% 16.000 mm 15 9.5 18.5%  $0.0136\ mm$ 1/2" 100% 12.500 mm 30 7.5 14.6%  $0.0097\ mm$ 3/8" 100% 9.500 mm 60 5 9.8% $0.0069\ mm$ 1/4" 100% 6.300 mm 240 2.5 4.9%  $0.0035 \ mm$ #4 100% 4.750 mm 1440 2.0%  $0.0014\ mm$ #10 100% 2.000 mm 0.850 mm #20 99% % Gravel: 0.0% Liquid Limit: 40.6 % #40 98% 0.425 mm % Sand: 31.3% Plastic Limit: 0.0 % #100 91% 0.150 mm % Silt: 61.7% Plasticity Index: 0.0 % #200 68.7% 0.075 mm 0.074 mm % Clay: Silts 67.1% 0.050 mm 31.4% 24.6% 0.020 mm 7.0% 0.005 mm Clavs 2.7% 0.002 mm Colloids 1.4% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding Comments:

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Reviewed by:



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Unified Soils Classification System, ASTM D-2487 Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Project #: 21B233 Sampled By: Client ML, Sandy Silt Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT11-GB-0-8.5 ft Tested By: C. Kriss brown Sample #: B21-1454 **Liquid Limit Determination** Weight of Wet Soils + Pan: 32.18 28.53 30.48 27.32 Weight of Dry Soils + Pan: 28.57 24.52 15.03 Weight of Pan: 19.55 19.88 Liquid Limit @ 25 Blows: Weight of Dry Soils: 9.02 9 49 7 44 Weight of Moisture: Plastic Limit: 3.61 4.01 3.16 N/A % Moisture: Plasticity Index, I<sub>P</sub>: 40.0 % 42.3 % 42.5 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CLOrOL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** 

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Comments: Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling.

Reviewed by:

Meghan Blodgett-Carrillo

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1454
Sample Date:	7/8/2021
Test Date:	8/26/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT11-GB-0-8.5 ft

 Visual Soil Description:
 brown silty clay

 Type of Specimen:
 Remolded Cylindrical Shear Box

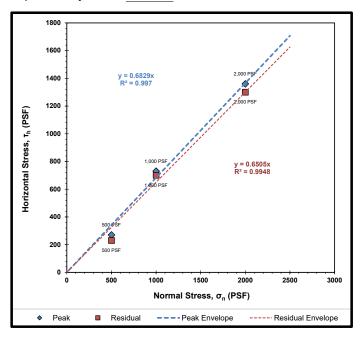
 Specimen Diameter (in):
 2.5

Summary of Sample	Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	58.2	
	Initial	Post-Consolidation
Dry Density (PCF):	76.6	86.1
Void Ratio:	1.201	0.957
Porosity (%):	54.6	48.9
Degree of Saturation (%):	saturated	saturated

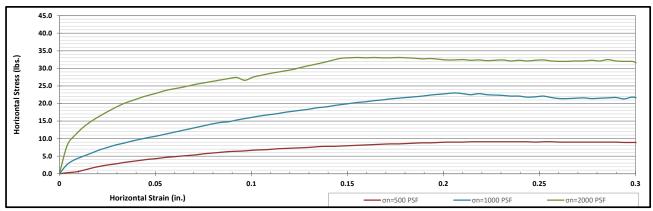
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	54.1	
	Initial	Post-Consolidation
Dry Density (PCF):	78.1	94.3
Void Ratio:	1.157	0.786
Porosity (%):	53.6	44.0
Degree of Saturation (%):	saturated	saturated

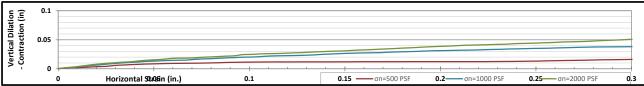
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	57.2	
	Initial	Post-Consolidation
Dry Density (PCF):	78.4	103.4
Void Ratio:	1.149	0.630
Porosity (%):	53.5	38.6
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS						
PEAK RESIDUAL						
Angle of Internal Friction, φ (°):	34	33				
Cohesion (PSF):	0	0				



Failure Envelope Test Values:						
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000			
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	270	730	1360			
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	230	700	1300			





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# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Visual Identification Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Project #: 21B233 Sampled By: Client Clayey Silt Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT11-GB-8.5-16.7 ft Tested By: C. Kriss brown Sample #: B21-1456 **Liquid Limit Determination** Weight of Wet Soils + Pan: 33.23 29.16 29.46 25.20 Weight of Dry Soils + Pan: 29.57 25.24 Weight of Pan: 19.86 15.05 14.81 Liquid Limit @ 25 Blows: Weight of Dry Soils: 9 71 10.15 10.43 38 % Weight of Moisture: Plastic Limit: 3.66 3.96 4.22 N/A % Moisture: 40.5 % Plasticity Index, I<sub>P</sub>: 37.7 % 39.0 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CLOrOL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 90% 100% 10 100 **Liquid Limit** 

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Comments: Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT11-GB-16.7-18.5 ft Sample#: B21-1457

Sampled By: Client Date Tested: 31-Aug-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487 Date Received: 29-Jul-21

SM, Silty Sand Sample Color:

mm

gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.019$   $D_{(10)} = 0.038$   $D_{(15)} = 0.057$   $D_{(30)} = 0.126$ % Gravel = 0.0%% Sand = 80.2% mm % Silt & Clay = 19.8% mm Liquid Limit = 0.0% mm  $D_{(50)} = 0.220$   $D_{(60)} = 0.279$   $D_{(90)} = 0.733$ mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.50$ Coeff. of Uniformity,  $C_U = 7.34$ Fineness Modulus = 1.22

Plastic Limit = 0.0% Moisture %, as sampled = 27.0% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					-	(50)	22/00		
				AS	TM C136, AS	oust Ratio = 2		7	
		Actual Cumulative	Interpolated Cumulative	AS	11WI C130, AS	1 N D0913, F	ISTM CIT	/	_
Sieve S	ize	Percent	Percent	Specs	Specs	1	-		
US	Metric	Passing	Passing	Max	Min		100% 🔩	lo lo la	
12.00"	300.00		100%	100.0%	0.0%	1	T	T	11
10.00"	250.00		100%	100.0%	0.0%		ŀ		I
8.00"	200.00		100%	100.0%	0.0%		90%	-	H
6.00"	150.00		100%	100.0%	0.0%				I
4.00"	100.00		100%	100.0%	0.0%		80%		I
3.00"	75.00		100%	100.0%	0.0%		80%		Ħ
2.50"	63.00		100%	100.0%	0.0%				I
2.00"	50.00	100%	100%	100.0%	0.0%		70%		Ц
1.75"	45.00		100%	100.0%	0.0%		1		I
1.50"	37.50		100%	100.0%	0.0%		ŀ		I
1.25"	31.50		100%	100.0%	0.0%		60%	-	H
1.00"	25.00	100%	100%	100.0%	0.0%	2	-		I
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%		I
5/8"	16.00		100%	100.0%	0.0%	96	50% T		I
1/2"	12.50	100%	100%	100.0%	0.0%				I
3/8"	9.50	100%	100%	100.0%	0.0%		40%	_	4
1/4"	6.30		100%	100.0%	0.0%				I
#4	4.75	100%	100%	100.0%	0.0%		1		I
#8	2.36		100%	100.0%	0.0%		30%	-	H
#10	2.00	99%	99%	100.0%	0.0%		ł		I
#16	1.18		96%	100.0%	0.0%		20%		I
#20	0.850	95%	95%	100.0%	0.0%		<sup>2070</sup> F		I
#30	0.600		85%	100.0%	0.0%		-		I
#40	0.425	77%	77%	100.0%	0.0%		10%	-	$\mathbb{H}$
#50	0.300		63%	100.0%	0.0%				I

57%

41%

35%

26%

23%

19.8%

100.0%

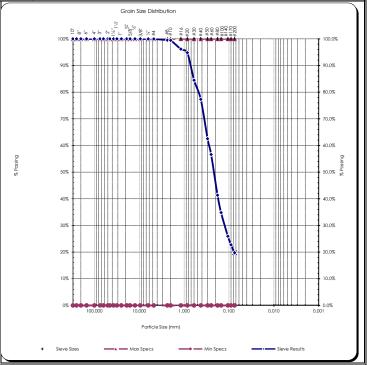
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**Comments:** 

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0.0%

0.0%

0.0%

0.0%

0.0%

Meghan Blodgett-Carrillo

0.250

0.180

0.150

0.106

0.090

0.075

#60

#80 #100

#140

#170

#200

Reviewed by: \_

57%

19.8%



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Visual Identification Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Project #: 21B233 Sampled By: Client Sandy Silt Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT9-GB-0-1.5 ft Tested By: C. Kriss brown Sample #: B21-1459 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Liquid limit cannot be established Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CLOrOL 20.0 % MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98
All results apply only to actual locations and materials tested. As a mutual protest

clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statem

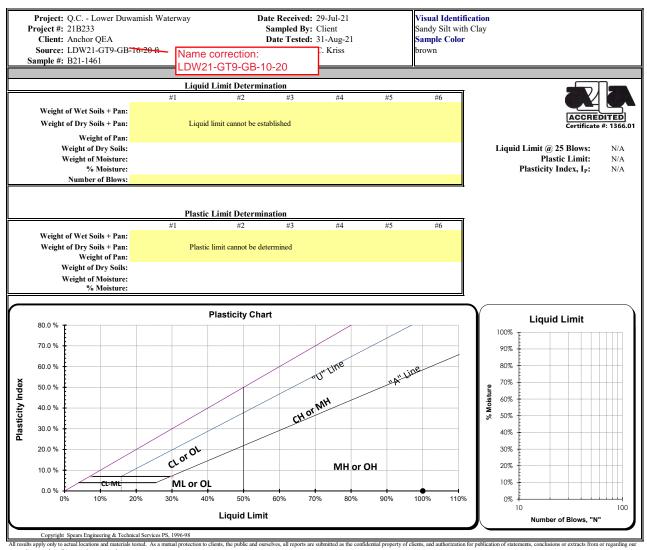
Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT9-GB-20-21.5 ft

Sample#: B21-1462

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 31-Aug-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: brown

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

0.180

0.150

0.106

0.090

0.075

#80

#140

#170

#200

Sample Meets Specs? N/A

 $D_{(5)} = 0.006$   $D_{(10)} = 0.010$   $D_{(15)} = 0.019$ % Gravel = 1.6% % Sand = 55.5% mm % Silt & Clay = 43.0% mm  $D_{(30)} = 0.058$ Liquid Limit = n/a mm  $D_{(50)} = 0.108$ Plasticity Index = n/a  $D_{(60)} = 0.159$ mm Sand Equivalent = n/a  $D_{(90)} = 1.026$ mm

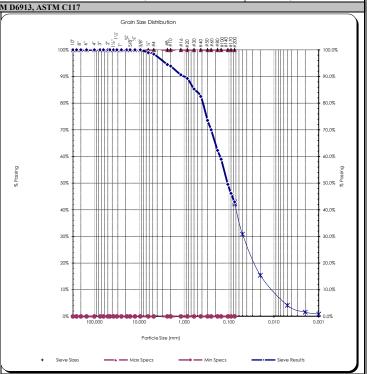
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 2.18$ Coeff. of Uniformity,  $C_U = 16.63$ Fineness Modulus = 0.99

Plastic Limit = n/a Moisture %, as sampled = 26.8% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					_	D <sub>(90)</sub> - 1	
				1.0		ust Ratio =	
		Actual Cumulative	Interpolated Cumulative	AS	STM C136, AS	TM D6913, A	ASTM
Sieve	Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		1
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%	2	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	
5/8"	16.00		100%	100.0%	0.0%	96	
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		
1/4"	6.30		99%	100.0%	0.0%		
#4	4.75	98%	98%	100.0%	0.0%		
#8	2.36		95%	100.0%	0.0%		
#10	2.00	94%	94%	100.0%	0.0%		
#16	1.18		91%	100.0%	0.0%		
#20	0.850	89%	89%	100.0%	0.0%		
#30	0.600		85%	100.0%	0.0%		
#40	0.425	83%	83%	100.0%	0.0%		
#50	0.300		74%	100.0%	0.0%		
#60	0.250	70%	70%	100.0%	0.0%		



0.0%

0.0%

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0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

43.0%

62%

59%

50%

46%

43.0%

100.0%

100.0%

100.0%

100.0%

100.0%



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SM, Silty Sand Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT9-GB-20-21.5 ft Tested By: C. Kriss brown Sample#: B21-1462 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: Sieve Analysis 2.65 Sample Weight: 75.17 **Grain Size Distribution** Hydroscopic Moist.: 1.11% Soils Particle Sieve Percent Passing Adj. Sample Wgt: 74.34 grams Size Diameter 75.000 mm 3.0" 100% 2.0" 100% 50.000 mm Hydrometer Soils Particle 37.500 mm 1.5" 100% Reading Corrected Percent 1.25" 31.500 mm 100% Minutes Reading **Passing** Diameter 0.0496 mm 100% 25.000 mm 24.0% 1.0" 0.0357 mm 3/4" 16.5 20.8% 100% 19.000 mm 5 13.5 17.1%  $0.0230\ mm$ 5/8" 100% 16.000 mm 15 9.5 12.0%  $0.0136\ mm$ 1/2" 100% 12.500 mm 30 8 10.1%  $0.0097\ mm$ 3/8" 100% 9.500 mm 60 6.3%  $0.0069\ mm$ 1/4" 99% 6.300 mm 240 2.5%  $0.0035 \ mm$ #4 98% 4.750 mm 1440 1.3%  $0.0014\ mm$ #10 94% 2.000 mm 0.850 mm #20 89% % Gravel: Liquid Limit: n/a #40 83% 0.425 mm % Sand: 55.5% Plastic Limit: n/a #100 59% 0.150 mm % Silt: 38.8% Plasticity Index: n/a #200 43.0% 0.075 mm 42.2% 0.074 mm % Clay: 4.2% Silts 30.9% 0.050 mm 15.4% 0.020 mm 4.2% 0.005 mm Clavs 1.6% 0.002 mm Colloids 0.9% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding Comments:

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1462
Sample Date:	7/8/2021
Test Date:	8/31/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT9-GB-20-21.5 ft

 Visual Soil Description:
 brown silty sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

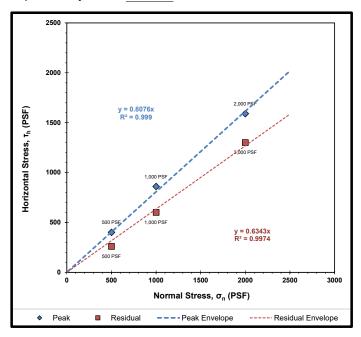
Specimen Height (in): 1
Rate of Strain (in/min): 0.0042
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	22.7	
	Initial	Post-Consolidation
Dry Density (PCF):	112.8	114.5
Void Ratio:	0.494	0.471
Porosity (%):	33.0	32.0
Degree of Saturation (%):	saturated	saturated

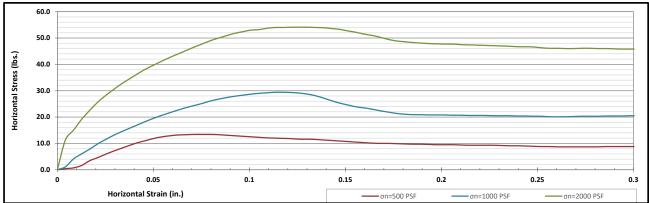
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF			
Initial Moisture Content (%):	21.4				
	Initial	Post-Consolidation			
Dry Density (PCF):	113.5	120.4			
Void Ratio:	0.485	0.399			
Porosity (%):	32.7	28.5			
Degree of Saturation (%):	saturated	saturated			

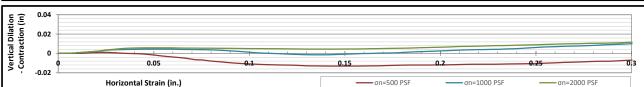
Summary of Sampl	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	19.9	
	Initial	Post-Consolidation
Dry Density (PCF):	114.3	123.5
Void Ratio:	0.474	0.364
Porosity (%):	32.1	26.7
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS						
	PEAK	RESIDUAL				
Angle of Internal Friction, φ (°):	39	32				
Cohesion (PSF):	0	0				



Failure Envelope Test Values:						
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000			
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	400	860	1590			
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	260	600	1300			





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT7-GB-0-5.7 ft Sample#: B21-1464

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 31-Aug-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} D_{(5)} = 0.066 \\ D_{(10)} = 0.135 \\ D_{(15)} = 0.170 \\ D_{(30)} = 0.247 \\ D_{(50)} = 0.327 \\ D_{(60)} = 0.367 \\ D_{(90)} = 0.741 \\ \end{array}$ % Gravel = 0.2% % Sand = 94.1% mm % Silt & Clay = 5.6% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a aces = n/a Coeff. of Curvature,  $C_C = 1.24$ Coeff. of Uniformity,  $C_U = 2.73$ Fineness Modulus = 1.68

Plastic Limit = 0.0% Moisture %, as sampled = 29.1% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

					D	$D_{(90)} = 0.741$ rust Ratio = 4/53			acture %				
				AS		TM D6913, AST		110	ictare /	, 2	Tue		
		Actual Cumulative	Interpolated Cumulative		Ź				Grain Size				
Sieve Size		Percent	Percent Specs Spe		Specs	D 80 4 4 90 12 12 12 12 12 12 12 12 12 12 12 12 12				in in			
US	Metric	Passing	Passing	Max	Min		100% ♦ ♦ ♦	<b>♦=♦*♦♦*(♦</b> €(		SE E¢x∳a	##		
12.00"	300.00		100%	100.0%	0.0%						7"		
10.00"	250.00		100%	100.0%	0.0%		- 11						
8.00"	200.00		100%	100.0%	0.0%		90%		-	₩₩	+		
6.00"	150.00		100%	100.0%	0.0%		- 1						
4.00"	100.00		100%	100.0%	0.0%		80%						
3.00"	75.00		100%	100.0%	0.0%		80%			Ш	П		
2.50"	63.00		100%	100.0%	0.0%		- 11						
2.00"	50.00	100%	100%	100.0%	0.0%		70%			Ш	44		
1.75"	45.00		100%	100.0%	0.0%		- 11						
1.50"	37.50		100%	100.0%	0.0%		11						
1.25"	31.50		100%	100.0%	0.0%		60%			Ш	+		
1.00"	25.00	100%	100%	100.0%	0.0%	2	- H						
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%						
5/8"	16.00		100%	100.0%	0.0%	P6	30%			Ш			
1/2"	12.50	100%	100%	100.0%	0.0%								
3/8"	9.50	100%	100%	100.0%	0.0%		40%			Ш	$\perp$		
1/4"	6.30		100%	100.0%	0.0%								
#4	4.75	100%	100%	100.0%	0.0%								
#8	2.36		99%	100.0%	0.0%		30%			HH	+		
#10	2.00	99%	99%	100.0%	0.0%		ł l						
#16	1.18		96%	100.0%	0.0%		20%			ШШ			
#20	0.850	95%	95%	100.0%	0.0%		20/8			Ш			
#30	0.600		83%	100.0%	0.0%		- [ ]						
#40	0.425	75%	75%	100.0%	0.0%		10%		+++	Ш	+-		
#50	0.300		43%	100.0%	0.0%								
#60	0.250	31%	31%	100.0%	0.0%								
#80	0.180		17%	100.0%	0.0%		0%	100,000	10 000 0	<del>Top</del>			

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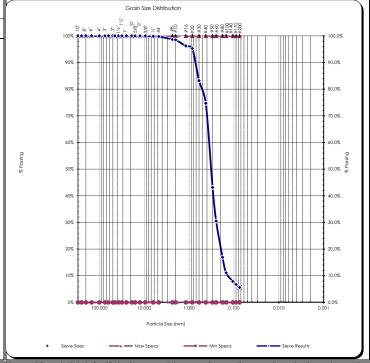
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7%

5.6%



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**Comments:** 

Meghan Blodgett-Carrillo

0.150

0.106

0.090

0.075

#100

#140

#170

#200

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233

1/4"

#4

#8

#10 #16

#20

#30

#40

#50

#60

#80

#100

#140

#170

#200

Comments:

6.30

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Source: LDW21-GT7-GB-8.5-18.5 ft Sample#: B21-1466

Client: Anchor QEA

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 31-Aug-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Dust Ratio = 13/66

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.022$   $D_{(10)} = 0.063$   $D_{(15)} = 0.080$ % Gravel = 0.2% mm % Silt & Clay = 14.4% mm  $D_{(30)} = 0.186$ Liquid Limit = n/a mm  $D_{(50)} = 0.299$ mm  $D_{(60)} = 0.354$ mm  $D_{(90)} = 0.799$ mm

Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

% Sand = 85.4%

Coeff. of Curvature,  $C_C = 1.55$ Coeff. of Uniformity,  $C_U = 5.61$ Fineness Modulus = 1.54 Plastic Limit = n/a

Moisture %, as sampled = 33.4% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136, AST
		Actual Cumulative	Interpolated Cumulative		
Sieve	e Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%

100%

92%

73%

41%

100%

100%

98%

97%

94%

92%

81%

73%

50%

41%

29%

24%

18%

16%

14.4%

100.0%

100.0%

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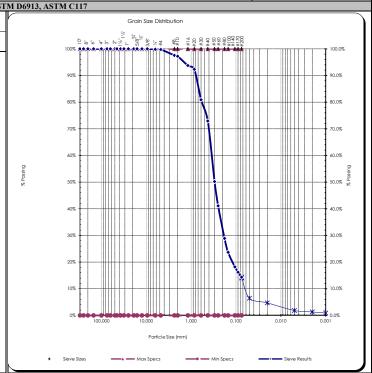
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Reviewed by: Meghan Blodgett-Carrillo



## **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SM, Silty Sand Client: Anchor QEA Date Tested: 31-Aug-21 Sample Color Source: LDW21-GT7-GB-8.5-18.5 ft Tested By: C. Kriss brown Sample#: B21-1466 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: Sieve Analysis 2.65 75.16 Sample Weight: **Grain Size Distribution** Hydroscopic Moist.: 1.29% Soils Particle Sieve Percent ACCREDITED Passing Adj. Sample Wgt: 74.20 grams Size Diameter 75.000 mm 3.0" 100% 2.0" 100% 50.000 mm Hydrometer Soils Particle 37.500 mm 1.5" 100% Reading Corrected Percent 1.25" 31.500 mm 100% Minutes Reading **Passing** Diameter 0.0537 mm 100% 25.000 mm 6.6% 1.0" 0.0381 mm 3/4" 4.5 5.9% 100% 19.000 mm 5 4 5.2%  $0.0241\ mm$ 5/8" 100% 16.000 mm 15 3.9%  $0.0140\ mm$ 1/2" 100% 12.500 mm 30 2.5 3.3%  $0.0100\ mm$ 3/8" 100% 9.500 mm 60 2 2.6% $0.0070\ mm$ 1/4" 100% 6.300 mm 240 1.3%  $0.0035 \ mm$ #4 100% 4.750 mm 1440 1.3%  $0.0014\ mm$ #10 97% 2.000 mm 0.850 mm #20 92% % Gravel: 0.2% Liquid Limit: n/a #40 73% 0.425 mm % Sand: 85.4% Plastic Limit: n/a #100 24% 0.150 mm % Silt: 12.5% Plasticity Index: n/a #200 14.4% 0.075 mm 0.074 mm % Clay: 1.9% 14.0% 0.050 mm 6.5% 4.7% 0.020 mm 1.9% 0.005 mm Clavs 1.3% 0.002 mm Colloids 0.9% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding **Comments:** 

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1466
Sample Date:	7/9/2021
Test Date:	9/1/2021
Technician:	M. Carrillo

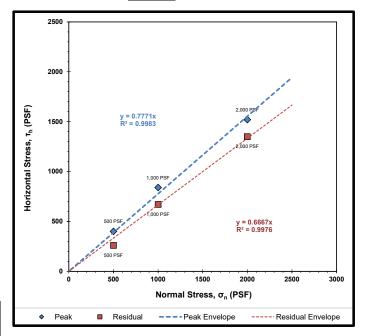
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	36.5	
	Initial	Post-Consolidation
Dry Density (PCF):	99.2	102.6
Void Ratio:	0.698	0.642
Porosity (%):	41.1	39.1
Degree of Saturation (%):	saturated	saturated

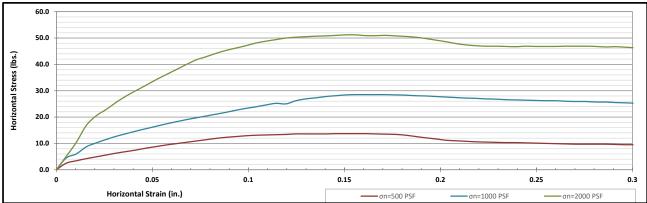
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	37.7	
	Initial	Post-Consolidation
Dry Density (PCF):	97.5	105.0
Void Ratio:	0.728	0.605
Porosity (%):	42.1	37.7
Degree of Saturation (%):	saturated	saturated

Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	36.6	
	Initial	Post-Consolidation
Dry Density (PCF):	99.4	106.9
Void Ratio:	0.694	0.576
Porosity (%):	41.0	36.5
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS		
	PEAK	RESIDUAL
Angle of Internal Friction, φ (°):	38	34
Cohesion (PSF):	0	0



Failure Envelope Test Values:				
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000	
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	400	840	1520	
Residual Horizontal Stress, τ <sub>h</sub> (PSF): 260 670 1350				





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Client:	Anchor QEA	Date:	September 30, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1535-1552
Revised on:		Date sampled:	July 9, 2021

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



## **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	<del></del>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 1, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1535	LDW21-GT7-GB-5.7-8.5 ft	220.0	955.7	691.6	264.1	471.6	56.0%
B21-1536	LDW21-GT7-GB-18.5-23.5 ft	233.7	1022.0	763.2	258.8	529.5	48.9%
B21-1537	LDW21-GT7-GB-23.5-25 ft	229.6	808.5	686.6	121.9	457.0	26.7%
B21-1538	LDW21-GT3-GB-0-1.5 ft	222.7	822.9	608.9	214.0	386.2	55.4%
B21-1539	LDW21-GT3-GB-0-8 ft	223.1	775.1	560.8	214.3	337.7	63.5%
B21-1540	LDW21-GT3-GB-8-9.5 ft	235.0	596.2	499.4	96.8	264.4	36.6%
B21-1541	LDW21-GT3-GB-13.6-18 ft	224.3	840.2	686.6	153.6	462.3	33.2%
B21-1542	LDW21-GT3-GB-18-19.5 ft	208.8	713.1	597.6	115.5	388.8	29.7%
B21-1543	LDW21-GT2-GB-0-1.5 ft	221.9	1015.5	706.7	308.8	484.8	63.7%
B21-1544	LDW21-GT2-GB-0-9 ft	221.9	1057.2	726.4	330.8	504.5	65.6%
B21-1545	LDW21-GT2-GB-9-10.5 ft	234.7	881.9	693.4	188.5	458.7	41.1%
B21-1546	LDW21-GT2-GB-16-19ft	319.9	776.4	594.5	181.9	274.6	66.2%
B21-1547	LDW21-GT1-GB-19-20.5 ft	268.9	932.1	798.3	133.8	529.4	25.3%
B21-1548	LDW21-GT1-GB-0-1.5 ft	270.2	991.8	734.1	257.7	463.9	55.6%
B21-1549	LDW21-GT1-GB-0-10 ft	266.5	951.7	694.7	257.0	428.2	60.0%
B21-1550	LDW21-GT1-GB-10-11.5 ft	303.8	1160.1	875.7	284.4	571.9	49.7%
B21-1551	LDW21-GT1-GB-10-20 ft	311.0	1013.9	756.9	257.0	445.9	57.6%
B21-1552	LDW21-GT1-GB-20-21.5 ft	306.5	1105.1	926.6	178.5	620.1	28.8%
		+	1	1			

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



## **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 1, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Dry Soil + Tare	Mass of Dry Soil	Pycno ID	Mass of Pycno	Volume of Pycno	Density of Water @ Tx	Mass of Pycno filled w/ water & soils				Temp. Correction Factor	Corrected SpG
B21-1536	LDW21-GT7-GB-18.5-23.5 ft	414.24	485.84	71.6	TSA-010	180.3	499.5	0.99752	753.80	709.46	23.1	2.6265591	0.99931	2.6247467
B21-1541	LDW21-GT7-GB-18.3-23.5 ft LDW21-GT3-GB-13.6-18 ft	379.79	481.87	102.1	TSA-010	190.3	499.5	0.99732	752.15	688.62	23.2	2.6482538		2.6463735
B21-1546	LDW21-GT3-GB-13.0-16 ft LDW21-GT2-GB-16-19ft	417.55	468.99	51.4	TSA-017	187.9	499.4	0.99754	717.30	686.06	23.0	2.546361	0.99933	2.5446549
B21-1549	LDW21-GT1-GB-0-10 ft	411.71	488.70	77.0	TSA-022	198.0	499.5	0.99749	742.60	696.19	23.2	2.5179566		2.5161689
B21-1551	LDW21-GT1-GB-10-20 ft	380.03	474.50	94.5	TSA-020	195.0	499.5	0.99749	750.48	693.27	23.2			2.5338864
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Visual Identification Sand with Silt and Clay Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT7-GB-5.7-8.5 ft Tested By: C. Kriss Sample #: B21-1535 **Liquid Limit Determination** Weight of Wet Soils + Pan: 34.38 32.59 32.44 ACCREDITED 28.85 Weight of Dry Soils + Pan: 30.26 28.70 Weight of Pan: 19.58 19.73 19.89 Liquid Limit @ 25 Blows: Weight of Dry Soils: 10.68 9.12 8 81 40 % Weight of Moisture: Plastic Limit: 4.12 3.74 3.74 N/A % Moisture: Plasticity Index, I<sub>P</sub>: 38.6 % 41.0 % 42.5 % N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 100% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

ut results apply only to actual locations and materians tested. As a mutual protection to citeria, the public and ourserves, air reports are summitted as the commental property of citeria, and authorization for publication of statements, concussions of extracts from or regarding our

Comments: Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

Meghan Blodgett-Carrillo

43.5%

Source: LDW21-GT7-GB-18.5-23.5 ft Sample#: B21-1536

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.009 \\ \textbf{D}_{(10)} = 0.017 \\ \textbf{D}_{(15)} = 0.026 \\ \textbf{D}_{(30)} = 0.052 \\ \textbf{D}_{(50)} = 0.094 \\ \textbf{D}_{(60)} = 0.122 \\ \textbf{D}_{(90)} = 0.372 \end{array}$ % Gravel = 0.1% % Sand = 56.4% mm % Silt & Clay = 43.5% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.27$ Coeff. of Uniformity,  $C_U = 7.08$ Fineness Modulus = 0.55

Plastic Limit = 0.0% Moisture %, as sampled = 48.9% Req'd Sand Equivalent =

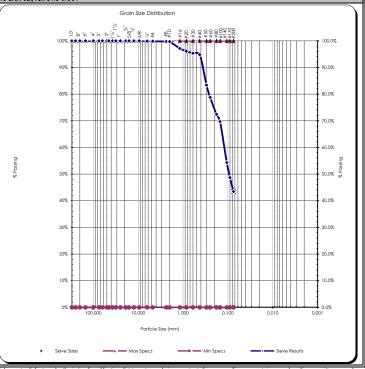
Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0$	0.372 mm	1
						Oust Ratio =		
				AS	TM C136, AS	TM D6913,	ASTM C117	
		Actual Cumulative	Interpolated Cumulative					
Sieve	Size	Percent	Percent	Specs	Specs		ъ:	9 4 E
US	Metric	Passing	Passing	Max	Min		100%	<b>~\$~\$∧\$\$</b>
12.00"	300.00		100%	100.0%	0.0%			
10.00"	250.00		100%	100.0%	0.0%			
8.00"	200.00		100%	100.0%	0.0%		90%	
6.00"	150.00		100%	100.0%	0.0%		ł l	
4.00"	100.00		100%	100.0%	0.0%		80%	
3.00"	75.00		100%	100.0%	0.0%		80%	
2.50"	63.00		100%	100.0%	0.0%		ļ.	
2.00"	50.00	100%	100%	100.0%	0.0%		70%	
1.75"	45.00		100%	100.0%	0.0%		<u> </u>	
1.50"	37.50		100%	100.0%	0.0%		t l	
1.25"	31.50		100%	100.0%	0.0%		60%	
1.00"	25.00	100%	100%	100.0%	0.0%	0	-	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	[-]	
5/8"	16.00		100%	100.0%	0.0%	PG.	50%	
1/2"	12.50	100%	100%	100.0%	0.0%			
3/8"	9.50	100%	100%	100.0%	0.0%		40%	
1/4"	6.30		100%	100.0%	0.0%		<u> </u>	
#4	4.75	100%	100%	100.0%	0.0%		t l	
#8	2.36		100%	100.0%	0.0%		30%	
#10	2.00	100%	100%	100.0%	0.0%		<b> </b>	
#16	1.18		97%	100.0%	0.0%			
#20	0.850		96%	100.0%	0.0%		20%	
#30	0.600		95%	100.0%	0.0%			
#40	0.425	95%	95%	100.0%	0.0%		10%	
#50	0.300		83%	100.0%	0.0%		<u> </u>	
#60	0.250		79%	100.0%	0.0%		<u> </u>	
#80	0.180		72%	100.0%	0.0%		0%	100.000
#100	0.150	70%	70%	100.0%	0.0%			.00.000
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54%

49%

43.5%



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Comments: Reviewed by:

100.0%

100.0%

100.0%



# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification **Project #:** 21B233 Sampled By: Client Sandy Silt Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT3-GB-0-8 ft Tested By: C. Kriss brown Sample #: B21-1539 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Liquid limit cannot be established Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: Number of Blows: Plastic Limit Determination Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Plastic limit cannot be determined Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 100% 70.0 % 90% 80% A" Line 60.0 % Plasticity Index 50.0 % 60% 40.0 % 50% 30.0 % CL Or OL 20.0 % 30% MH or OH 20% 10.0 % 10% ML or OL 100% 80% 0% -**Liquid Limit** Number of Blows, "N

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the

liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT3-GB-8-9.5 ft Sample#: B21-1540

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 1-Sep-21 Tested By: C. Kriss

SM, Silty Sand Sample Color: brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{ASTM D43} \\ \textbf{D}_{(5)} = 0.017 \\ \textbf{D}_{(10)} = 0.034 \\ \textbf{D}_{(15)} = 0.051 \\ \textbf{D}_{(30)} = 0.100 \\ \textbf{D}_{(50)} = 0.178 \\ \textbf{D}_{(60)} = 0.238 \\ \textbf{D}_{(60)} = 0.417 \end{array}$ % Gravel = 0.5% % Sand = 77.3% mm % Silt & Clay = 22.3% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

 $D_{(90)} = 0.417$ mm Fracture %, 1 Face = n/a

Unified Soil Classification System, ASTM-2487

Coeff. of Curvature,  $C_C = 1.25$ Coeff. of Uniformity,  $C_U = 7.06$ Fineness Modulus = 0.99

Plastic Limit = 0.0% Moisture %, as sampled = 36.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

					D	ust Ratio = 19/	/78	F	racture %,	2+ Fa	ces = n/a		Req'd	Fractui	re %, 2	2+ Fac	es =
				AS	TM C136, AS	TM D6913, AS	TM C117										
		Actual	Interpolated						Grain Size	Distribu	tion						
		1	Cumulative	_		_											
Sieve		Percent	Percent	Specs	Specs		b in	6 44 V	2 % % E	. 4 9	5 5885	8888	28				
US	Metric	Passing	Passing	Max	Min	_	100%			7		+++++	**	т-т	штт	т-т	T 100.0%
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1.25"	31.50		100%	100.0%	0.0%		60%			###		11	####		mm	_	60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0	1					11					ju B
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%						ШШ				50.0% lg
5/8"	16.00		100%	100.0%	0.0%	96	50%					1					1 00.0% be
1/2"	12.50	100%	100%	100.0%	0.0%		- [ ]					1 1					1
3/8"	9.50	100%	100%	100.0%	0.0%		40%		+ + - + + + + + + + + + + + + + + + + +	HHH		+++		$\vdash$	₩₩	₩-	40.0%
1/4"	6.30		100%	100.0%	0.0%		11					111					1
#4	4.75	100%	100%	100.0%	0.0%							1					1
#8	2.36		99%	100.0%	0.0%		30%			###		++-	•		HHH	+	30.0%
#10	2.00	99%	99%	100.0%	0.0%		ł l						ì				i
#16	1.18		95%	100.0%	0.0%		20%						*				20.0%
#20	0.850		93%	100.0%	0.0%		20,0										20.0%
#30	0.600		92%	100.0%	0.0%		- [ ]										1
#40	0.425	91%	91%	100.0%	0.0%		10%		+ + - + + + + + + + + + + + + + + + + +	+++		++-		$\vdash$	₩₩		10.0%
#50	0.300		70%	100.0%	0.0%		11										1
#60	0.250		62%	100.0%	0.0%												1
#80	0.180		50%	100.0%	0.0%		0%	100,000	10.000	بلنور	1.000	0.1	00	0.01	10	<del></del> 0	♣ 0.0% .001
#100	0.150	45%	45%	100.0%	0.0%							0.1		5.0		0.	
#140	0.106		32%	100.0%	0.0%				Pa	rticle Size	(mm)						
#170	0.090		27%	100.0%	0.0%												
#200	0.075	22.3%	22.3%	100.0%	0.0%		Sieve Sizes	_	■ Max Spe	ecs	<b>→</b> -	Min Specs			Sieve Re	isults	
Convright	Spears Engineering & Tec	hnical Services PS, 1996-9															

	$\alpha \sim a$
	Month Bladgett anillo
Reviewed by:	
	Meghan Blodgett-Carrillo

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1540
Sample Date:	7/9/2021
Test Date:	9/24/2021
Technician:	M. Carrillo

Sample Source: LDW21-GT3-GB-8-9.5 ft

Visual Soil Description: brown silty sand

Type of Specimen: Remolded Cylindrical Shear Box

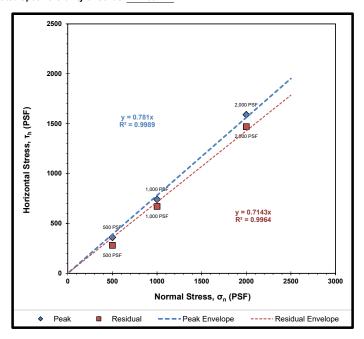
Specimen Diameter (in): 2.5

Summary of Samp	le Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	33.7	
	Initial	Post-Consolidation
Dry Density (PCF):	102.4	104.0
Void Ratio:	0.645	0.620
Porosity (%):	39.2	38.3
Degree of Saturation (%):	saturated	saturated

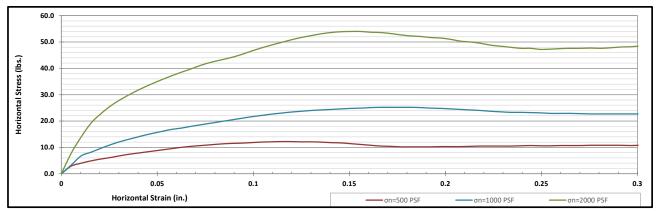
Summary of Sample	e Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	31.2	
	Initial Post-Consolidation	
Dry Density (PCF):	104.0	109.1
Void Ratio:	0.620	0.544
Porosity (%):	38.3	35.2
Degree of Saturation (%):	saturated	saturated

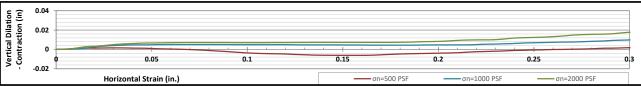
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	30.1	
	Initial	Post-Consolidation
Dry Density (PCF):	105.0	110.4
Void Ratio:	0.605	0.526
Porosity (%):	37.7	34.5
Degree of Saturation (%):	saturated	saturated

ESTIMATED STR	ENGTH PARA	METERS
	PEAK	RESIDUAL
Angle of Internal Friction, φ (°):	38	36
Cohesion (PSF):	0	0



Failure Envelope Test	Values:		
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	360	740	1590
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	280	670	1470





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Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

Source: LDW21-GT3-GB-13.6-18  $\operatorname{ft}$ 

Sample#: B21-1541

3/8"

1/4"

#4

#8

#10

#16

#20

#30

#40 #50

#60

#80

#100

#140

#170

#200

Comments:

Reviewed by:

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21

Date Tested: 1-Sep-21 Tested By: C. Kriss Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

mm

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

 $D_{(90)} = 1.234$ Dust Ratio = - 17/89

M D6913, ASTM C117

Specifications No Specs

9.50

6.30

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Sample Meets Specs ? N/A

Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

Moisture %, as sampled = 33.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

		Actual Cumulativ	Interpolated e Cumulative		
Sieve US	Size Metric	Percent Passing	Percent Passing	Specs Max	Specs Min
12.00"	300.00	1 assing	100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%

100%

100%

100%

100%

100%

89%

85%

82%

80%

47%

34%

16%

8%

-6%

-11%

-15.2%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

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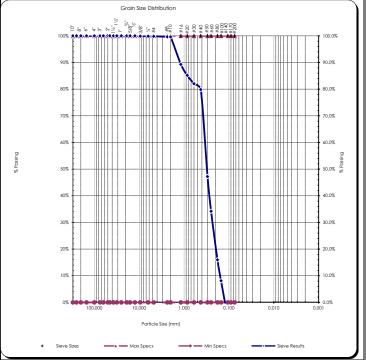
100%

100%

100%

80%

-15.2%



Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval

Nante De bott ai No



# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification **Project #:** 21B233 Sampled By: Client Sandy Silt Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT2-GB-0-9 ft Tested By: C. Kriss brown Sample #: B21-1544 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Liquid limit cannot be established Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: Number of Blows: Plastic Limit Determination Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Plastic limit cannot be determined Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 100% 70.0 % 90% 80% A" Line 60.0 % Plasticity Index 50.0 % 60% 40.0 % 50% 30.0 % CL Or OL 20.0 % 30% MH or OH 20% 10.0 % 10% ML or OL 100% 80% 0% -**Liquid Limit** Number of Blows, "N

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the

liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT2-GB-16-19 ft Sample#: B21-1546

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21 Tested By: C. Kriss

Visual Identification Sandy Silt with Clay Sample Color: brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASINID43} \\ \textbf{D}_{(5)} = 0.003 \\ \textbf{D}_{(10)} = 0.006 \\ \textbf{D}_{(15)} = 0.009 \\ \textbf{D}_{(30)} = 0.025 \\ \textbf{D}_{(50)} = 0.061 \\ \textbf{D}_{(60)} = 0.072 \\ \textbf{D}_{(90)} = 0.265 \\ \textbf{Partia} = 25/30 \\ \end{array}$ mm % Silt & Clay = 63.3% mm mm mm mm mm

Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a

% Gravel = 0.3% % Sand = 36.4% Coeff. of Curvature,  $C_C = 1.57$ Coeff. of Uniformity,  $C_U = 12.88$ Fineness Modulus = 0.28 Plastic Limit = n/a

Moisture %, as sampled = 66.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

		Actual Cumulative	Interpolated Cumulative							rain Size									
Sieve	Size	Percent	Percent	Specs	Specs		h.		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ni Zog	: + a	2 20	8 2 8	8888	8				
US	Metric	Passing	Passing	Max	Min		100%	<b>♦^•=♦</b> / <b>•</b> 0.40 4.90	• <b></b>	ે છે. •••••	₹ <u>₩</u> #		# # #	* * * * *	-C2 			<b>-</b>	100
12.00"	300.00		100%	100.0%	0.0%								ΠŢ					1	
10.00"	250.00		100%	100.0%	0.0%								₩ Į					1 1	
8.00"	200.00		100%	100.0%	0.0%		90%				+++	1						┿	90.
6.00"	150.00		100%	100.0%	0.0%									<i>Y</i> .				1 1	
4.00"	100.00		100%	100.0%	0.0%									i				1 1	80.0
3.00"	75.00		100%	100.0%	0.0%		80%							1				1	80.0
2.50"	63.00		100%	100.0%	0.0%									1				1	
2.00"	50.00	100%	100%	100.0%	0.0%		70%				Ш			1			Ш	1	70.
1.75"	45.00		100%	100.0%	0.0%														
1.50"	37.50		100%	100.0%	0.0%		ł								<b>.</b>			1 1	
1.25"	31.50		100%	100.0%	0.0%		60%							-	1			++	60.0
1.00"	25.00	100%	100%	100.0%	0.0%	9									N.			1 1	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing													50.
5/8"	16.00		100%	100.0%	0.0%	96	50%								*			1 1	50.
1/2"	12.50	100%	100%	100.0%	0.0%										ΠÏ			1	
3/8"	9.50	100%	100%	100.0%	0.0%		40%				444				ШЦ			11	40.
1/4"	6.30		100%	100.0%	0.0%													1 1	
#4	4.75	100%	100%	100.0%	0.0%										·	( II II		1 1	
#8	2.36		99%	100.0%	0.0%		30%				+++	-				<del>\</del>		┿	30.0
#10	2.00	99%	99%	100.0%	0.0%											*		1 1	
#16	1.18		99%	100.0%	0.0%													1 1	
#20	0.850		99%	100.0%	0.0%		20%				$^{\dagger\dagger\dagger}$		Ш				mm	1 1	20.0
#30	0.600		99%	100.0%	0.0%														
#40	0.425	99%	99%	100.0%	0.0%		10%				444				ШШ		$\lambda$	11	10.0
#50	0.300		92%	100.0%	0.0%														
#60	0.250		89%	100.0%	0.0%		ŀ											*_]	
#80	0.180		85%	100.0%	0.0%		0%	والمرودة	-	10.000	والماطاط	1.000		0.10	سلللظ	0.010	шШ		0.09
#100	0.150	84%	84%	100.0%	0.0%			100.00	,	10.000		1.000	J	0.10	IU	0.010	J	0.00	Л
#140	0.106	0170	72%	100.0%	0.0%					Po	rticle Size	(mm)							
#170	0.090		67%	100.0%	0.0%														
#200	0.075	63.3%	63.3%	100.0%	0.0%		<ul> <li>Sieve Sizes</li> </ul>			- Max Sp	acs.			n Specs			Sieve Resu	te	
#200 Copyright		1	U.	100.070	0.070	II	<ul> <li>31646 21562</li> </ul>			- wax sp	503		- M	11.3hqC2			weve Resu	13	



## **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Project #: 21B233 Sandy Silt with Clay Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT2-GB-16-19 ft Tested By: C. Kriss brown Sample#: B21-1546 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 2.54 Sp Gr: Sieve Analysis Sample Weight: 75.85 **Grain Size Distribution** Hydroscopic Moist.: 6.24% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 71.39 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 38 7% 0.0494 mm 100% 25.000 mm 27 1.0" 33.7% 0.0358 mm 3/4" 100% 19.000 mm 2 23.5 20.5 29 4%  $0.0231\ mm$ 5/8" 100% 16.000 mm 15 14.5 20.8% 0.0138 mm 1/2" 100% 12.500 mm 30 16.5% 0.0099 mm 3/8" 100% 9.500 mm 0.0071 mm 60 12.9% 1/4" 100% 6.300 mm 240 4.5 6.4% 0.0036 mm 100% 4.750 mm #4 #10  $2.000\ mm$ 1440 2.1%  $0.0015 \ mm$ 99% 99% #20 0.850 mm Liquid Limit: n/a % Gravel: 0.3% #40 99%  $0.425 \, mm$ % Sand: 36.4% Plastic Limit: n/a #100 84% 0.150 mm % Silt: 54.3% Plasticity Index: n/a #200 63.3%  $0.075 \ mm$ 62.3% 0.074 mm % Clay: 9.0% Silts 47.6% 0.050 mm 0.020 mm 26.5% 0.005 mm 9.0% Clays 3.1%  $0.002\ mm$ Colloids 1.4%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Environmental ● Geotechnical Engineering ● Special Inspection ● Non-Destructive Testing ● Materials Testing

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Reviewed by:

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1546
Sample Date:	7/9/2021
Test Date:	9/27/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT2-GB-16-19 ft

 Visual Soil Description:
 brown sandy silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

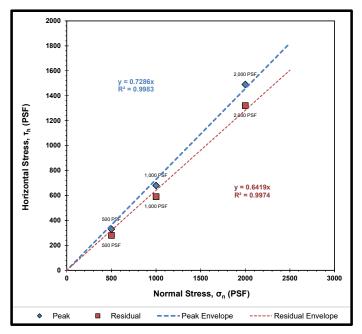
Specimen Height (in): 1
Rate of Strain (in/min): 0.0042
Estimated Specific Gravity of Solids: 2.65

Summary of Samp	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%): 38.6		
	Initial	Post-Consolidation
Dry Density (PCF):	100.0	106.5
Void Ratio:	0.684	0.581
Porosity (%):	40.6	36.8
Degree of Saturation (%):	saturated	saturated

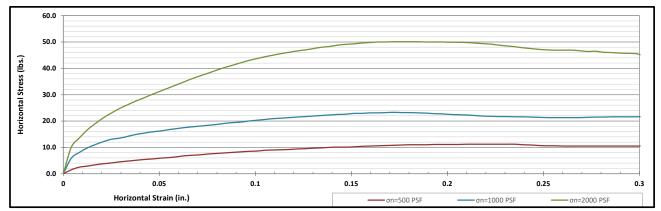
Summary of Sample	σ <sub>n</sub> =1000 PSF	
Initial Moisture Content (%):	36.2	
	Initial	Post-Consolidation
Dry Density (PCF):	101.4	111.3
Void Ratio:	0.661	0.514
Porosity (%):	39.8	34.0
Degree of Saturation (%):	saturated	saturated

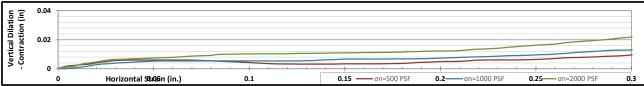
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%): 34.6		
	Initial	Post-Consolidation
Dry Density (PCF):	102.5	110.5
Void Ratio:	0.643	0.525
Porosity (%):	39.1	34.4
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS				
PEAK RESIDUAL				
Angle of Internal Friction, φ (°):	36	33		
Cohesion (PSF):	0	0		



Failure Envelope Test Values:				
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000	
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	330	680	1490	
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	280	590	1320	





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# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification **Project #:** 21B233 Sampled By: Client Silty Sand Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT1-GB-0-10 ft Tested By: C. Kriss brown Sample #: B21-1549 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Liquid limit cannot be established Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: Number of Blows: Plastic Limit Determination Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Plastic limit cannot be determined Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 100% 70.0 % 90% 80% A" Line 60.0 % Plasticity Index 50.0 % 60% 40.0 % 50% 30.0 % CL Or OL 20.0 % 30% MH or OH 20% 10.0 % 10% ML or OL 100% 80% 0% -**Liquid Limit** Number of Blows, "N

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding or reports is reserved pending our writer approval.

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#80

#100

#140

#170

#200

**Comments:** 

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

Source: LDW21-GT1-GB-10-20 ft Sample#: B21-1551

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 1-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown

= 33/98



### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.013 \\ D_{(10)} = 0.037 \\ D_{(15)} = 0.059 \\ D_{(30)} = 0.072 \\ \end{array}$ % Gravel = 0.5% % Sand = 66.2% mm % Silt & Clay = 33.4% mm Liquid Limit = n/a mm  $D_{(50)} = 0.106$   $D_{(60)} = 0.125$   $D_{(90)} = 0.327$ mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.11$ Coeff. of Uniformity,  $C_U = 3.34$ Fineness Modulus = 0.42

Plastic Limit = n/a Moisture %, as sampled = 57.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)}$
						ust Ratio
		Actual	Interpolated	AS	TM C136, AS	TM D691
			e Cumulative			ľ
Sieve	C!	Percent	Percent	C	C	-
US	Metric	Passing	Passing	Specs Max	Specs Min	
12.00"	300.00	rassing	100%	100.0%	0.0%	
10.00"	250.00		100%	100.0%	0.0%	
8.00"	200.00		100%	100.0%	0.0%	
6.00"	150.00		100%	100.0%	0.0%	
4.00"	100.00		100%	100.0%	0.0%	
3.00"	75.00		100%	100.0%	0.0%	
2.50"	63.00		100%	100.0%	0.0%	
2.00"	50.00	100%	100%	100.0%	0.0%	
1.75"	45.00	10070	100%	100.0%	0.0%	
1.50"	37.50		100%	100.0%	0.0%	
1.25"	31.50		100%	100.0%	0.0%	
1.00"	25.00	100%	100%	100.0%	0.0%	o o
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing
5/8"	16.00	10070	100%	100.0%	0.0%	96
1/2"	12.50	100%	100%	100.0%	0.0%	
3/8"	9.50	100%	100%	100.0%	0.0%	
1/4"	6.30		100%	100.0%	0.0%	
#4	4.75	100%	100%	100.0%	0.0%	
#8	2.36		99%	100.0%	0.0%	
#10	2.00	99%	99%	100.0%	0.0%	
#16	1.18		99%	100.0%	0.0%	
#20	0.850		99%	100.0%	0.0%	
#30	0.600		99%	100.0%	0.0%	
#40	0.425	99%	99%	100.0%	0.0%	
#50	0.300		87%	100.0%	0.0%	
#60	0.250		83%	100.0%	0.0%	

76%

73%

50%

41%

33.4%

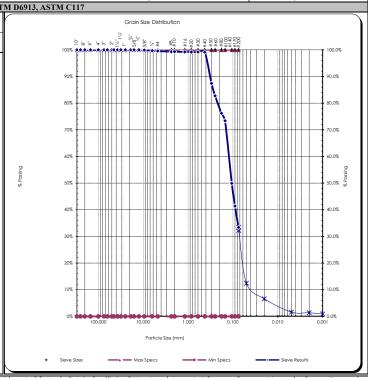
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Reviewed by:

73%

33.4%



## **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT1-GB-10-20 ft Tested By: C. Kriss brown Sample#: B21-1551 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 2.53 Sp Gr: Sieve Analysis Sample Weight: 75.48 **Grain Size Distribution** Hydroscopic Moist.: 2.34% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 73.75 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0554 mm 100% 25.000 mm 11.1% 1.0" 0.0394 mm 3/4" 100% 19.000 mm 2 7.5 10.4% 0.0252 mm 5.5 7.6%5/8" 100% 16.000 mm 15 5.5%  $0.0146 \, \text{mm}$ 1/2" 100% 12.500 mm 30 4.2% 0.0104 mm 3/8" 100% 9.500 mm 0.0074 mm 60 1.5 2.1% 1/4" 100% 6.300 mm 240 1.4% 0.0037 mm 100% 4.750 mm #4 #10  $2.000\ mm$ 1440 1.4%  $0.0015 \ mm$ 99% 99% #20  $0.850 \ mm$ Liquid Limit: n/a % Gravel: 0.5% #40 99%  $0.425 \, mm$ % Sand: 66.2% Plastic Limit: n/a #100 73% 0.150 mm % Silt: Plasticity Index: n/a #200 33.4%  $0.075 \ mm$ 32.2% 0.074 mm % Clay: 1.6% Silts 12.5% 0.050 mm 0.020 mm 6.6% 1.6% 0.005 mm Clays 1.4%  $0.002\ mm$ Colloids 0.9%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by: Meghan Blodgett-Carrillo

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1551
Sample Date:	7/9/2021
Test Date:	9/23/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT1-GB-10-20 ft

 Visual Soil Description:
 brown silty sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

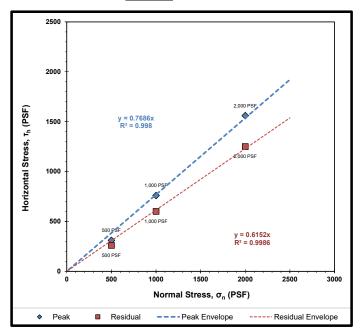
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%): 30.0		
	Initial	Post-Consolidation
Dry Density (PCF):	106.5	108.9
Void Ratio:	0.581	0.547
Porosity (%):	36.8	35.4
Degree of Saturation (%):	saturated	saturated

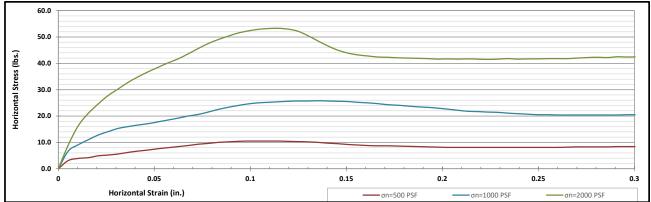
Summary of Sample	σ <sub>n</sub> =1000 PSF	
Initial Moisture Content (%):	29.7	
	Initial	Post-Consolidation
Dry Density (PCF):	598.3	612.5
Void Ratio:	-0.718	-0.725
Porosity (%):	-255.1	-263.6
Degree of Saturation (%):	-111.5	saturated

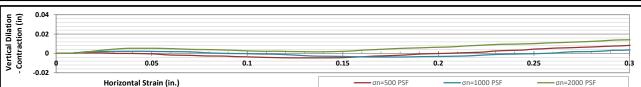
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%): 29.8		
	Initial	Post-Consolidation
Dry Density (PCF):	107.6	113.2
Void Ratio:	0.566	0.488
Porosity (%):	36.1	32.8
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS				
PEAK RESIDUAL				
Angle of Internal Friction, φ (°):	38	32		
Cohesion (PSF):	0	0		



Failure Envelope Test Values:									
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000						
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	310	760	1560						
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	260	600	1250						





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Client:	Anchor QEA	Date:	October 1, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1563-1577
Revised on:		Date sampled:	7-12-21 & 7-13-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



## **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	<u> </u>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 3, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1563	LDW21-GT13-GB-0-1.5 ft	229.0	1015.9	773.9	242.0	544.9	44.4%
B21-1564	LDW21-GT13-GB-0-11 ft	221.0	537.3	449.8	87.5	228.8	38.2%
B21-1565	LDW21-GT13-GB-11-12.5 ft	217.1	1140.1	930.2	209.9	713.1	29.4%
B21-1566	LDW21-GT13-GB-11-21 ft	233.4	922.3	739.9	182.4	506.5	36.0%
B21-1567	LDW21-GT13-GB-21-22.5 ft	222.0	1231.9	1002.3	229.6	780.3	29.4%
B21-1568	LDW21-GT13-GB-21-31 ft	222.1	758.0	621.0	137.0	398.9	34.3%
B21-1569	LDW21-GT13-GB-31-32.5 ft	208.7	1100.3	893.6	206.7	684.9	30.2%
B21-1570	LDW21-GT19-GB-0-1.5 ft	234.8	863.2	678.6	184.6	443.8	41.6%
B21-1571	LDW21-GT19-GB-0-6.9 ft	222.1	761.3	524.7	236.6	302.6	78.2%
B21-1572	LDW21-GT19-GB-6.9-8.5 ft	233.1	1713.9	1391.1	322.8	1158.0	27.9%
B21-1573	LDW21-GT19-GB-8.5-10 ft	220.2	954.0	779.7	174.3	559.5	31.2%
B21-1574	LDW21-GT19-GB-8.5-18.5 ft	224.3	805.4	688.5	116.9	464.2	25.2%
B21-1575	LDW21-GT19-GB-18.5-20 ft	229.6	1121.9	927.8	194.1	698.2	27.8%
B21-1576	LDW21-GT19-GB-18.5-28.5 ft	215.7	1329.2	1088.0	241.2	872.3	27.7%
B21-1577	LDW21-GT19-GB-28.5-30 ft	225.2	725.0	616.3	108.7	391.1	27.8%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



## **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 1, 2021	Tested by: A. Eifrig

B21-1571 LDW21-GT19-GB-0-6.9 ft 429.62 462.35 32.7 TSA-014 192.3 499.5 0.99752 710.77 690.55 23.1 2.6160217 0.99931	Sample # B21-1564 B21-1568	Location LDW21-GT13-GB-0-11 ft LDW21-GT13-GB-21-31 ft	Tare 378.85 394.06	Dry Soil + Tare 431.72 438.75	Mass of Dry Soil 52.9 44.7	Pycno ID TSA-016 TSA-012	Mass of Pycno 197.2 180.4	Volume of Pycno 499.5 499.5	Density of Water @ Tx 0.99747 0.99752	Mass of Pycno filled w/ water & soils 728.02 706.18	Mass of	Water, 0.1 *C 23.3	SpG of Soils 2.6087558	Factor	SpG 2.6068253
B21-1574 LDW21-GT19-GB-8.5-18.5 ft 415.36 464.91 49.6 TSA-013 184.0 499.7 0.99754 712.79 682.43 23.0 2.5819681 0.99933	B21-1571	LDW21-GT19-GB-0-6.9 ft	429.62	462.35	32.7	TSA-014	192.3	499.5	0.99752	710.77	690.55				2.6142167
	B21-1574	LDW21-GT19-GB-8.5-18.5 ft	415.36	464.91	49.6	TSA-013	184.0	499.7	0.99754	712.79	682.43	23.0	2.5819681	0.99933	2.5802382
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					<del>                                     </del>				<del>                                     </del>	<del>                                     </del>					
			1												

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT13-GB-0-11 ft Sample#: B21-1564

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 1-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.008 \\ \textbf{D}_{(10)} = 0.019 \\ \textbf{D}_{(15)} = 0.053 \\ \textbf{D}_{(30)} = 0.121 \\ \textbf{D}_{(50)} = 0.244 \\ \textbf{D}_{(60)} = 0.301 \\ \textbf{D}_{(90)} = 1.175 \\ \textbf{Partia} = 26/87 \\ \end{array}$ % Gravel = 0.4% % Sand = 75.2% mm % Silt & Clay = 24.4% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 2.52$ Coeff. of Uniformity,  $C_U = 15.71$ Fineness Modulus = 1.34

Plastic Limit = 0.0% Moisture %, as sampled = 38.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

recquiracture 70, 11 acc -	
Req'd Fracture %, 2+ Faces =	

						ust Ratio = 26/87		Fracture %	6, 2+ Fa	ces = n	/a	R	leq'd Fr	racture	%, 2+	Faces =	=
ASTM C136, ASTM D6913, ASTM C117																	
			Interpolated					Grain Siz	e Distribut	tion							
~	a.	1	Cumulative			-		ŧ .									
Sieve		Percent	Percent	Specs	Specs		2 60 60 € 60 60 °		7 4 9	8 2 9	8 4 8 8	88458					
US	Metric	Passing	Passing	Max	Min	100%		*****	Trivit Tri	4	+++	** ***	ППТ	Т	ППТ	T 10	0.0%
12.00"	300.00		100%	100.0%	0.0%		<u> </u>			<b>N</b> III							
10.00"	250.00		100%	100.0%	0.0%		[			1 \						1 1	. 007
8.00"	200.00		100%	100.0%	0.0%	90%										70	1.0%
6.00"	150.00		100%	100.0%	0.0%					l N							
4.00"	100.00		100%	100.0%	0.0%	80%			Ш.	1					Ш	80	1.0%
3.00"	75.00		100%	100.0%	0.0%						111					1 1	
2.50"	63.00		100%	100.0%	0.0%						111						
2.00"	50.00	100%	100%	100.0%	0.0%	70%				+			╫╫┼		+++	70	.0%
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1.50"	37.50		100%	100.0%	0.0%											1 1	
1.25"	31.50		100%	100.0%	0.0%	60%			****	1 111	## <b>!</b>		###		mm		1.0%
1.00"	25.00	100%	100%	100.0%	0.0%	D C					1111						in g
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5/8"	16.00		100%	100.0%	0.0%	P6 2070	l				11111					"	86
1/2"	12.50	100%	100%	100.0%	0.0%		[				11111					1 1	
3/8"	9.50	100%	100%	100.0%	0.0%	40%				1		<u> </u>			+++	40	.0%
1/4"	6.30		100%	100.0%	0.0%							Ĭ III					
#4	4.75	100%	100%	100.0%	0.0%							1					
#8	2.36		99%	100.0%	0.0%	30%			****	1		<b>\</b>	###		+++	30	1.0%
#10	2.00	99%	99%	100.0%	0.0%		t I IIIIII					1				1 1	
#16	1.18		90%	100.0%	0.0%	20%										<u> </u>	1.0%
#20	0.850		86%	100.0%	0.0%	20/6							<b>VIII</b>			ΤŦ°	1.076
#30	0.600		84%	100.0%	0.0%								*			1 1	
#40	0.425	82%	82%	100.0%	0.0%	10%							$\boxplus >$	<b>K</b> -	+++	10	1.0%
#50	0.300		60%	100.0%	0.0%												
#60	0.250		51%	100.0%	0.0%										*		
#80	0.180		39%	100.0%	0.0%	0%	100.000	10.00	111 bi i.i.	1.000	<del>0 0 00</del> -	0.100		0.010	ш	0.001	0%
#100	0.150	34%	34%	100.0%	0.0%		100.000	.0.00		1.000		0.100		0.010		0.001	
#140	0.106	-	28%	100.0%	0.0%			1	Particle Size	(mm)							
#170	0.090		26%	100.0%	0.0%												
#200	0.075	24.4%	24.4%	100.0%	0.0%	+ Sieve S	izes —	—▲ — Max S	specs		- Min S	Specs	_	Sie	eve Resul	ts	
		hnical Services PS, 1996-9															
				and ourselves, all reports are	submitted as the confide	ntial property of clients, and autho	rization for public	ation of stateme	ents, conclu	sions or ext	racts from	or regardi	ng our repo	orts is rese	rved pen	ing our writ	tten appro



## **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT13-GB-0-11 ft Tested By: C. Kriss brown Sample#: B21-1564 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.61 Sieve Analysis Sample Weight: 100.15 **Grain Size Distribution** Hydroscopic Moist.: 0.83% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 99.33 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0519 mm 100% 25.000 mm 14 5 14 6% 1.0" 3/4" 100% 19.000 mm 2 13 13.1% 0.0369 mm 11.5 11.6%  $0.0236\ mm$ 5/8" 100% 16.000 mm 15 8.1% 0.0139 mm 1/2" 100% 12.500 mm 30 6.5 6.6% 0.0099 mm 3/8" 100% 9.500 mm 0.0071 mm 60 4.0% 1/4" 100% 6.300 mm 240 1.0% 0.0036 mm 100% 4.750 mm #4 #10  $2.000\ mm$ 1440 1.0%  $0.0015 \ mm$ 99% #20 86% 0.850 mm Liquid Limit: 0.0 % % Gravel: 0.4% #40 82%  $0.425 \, mm$ % Sand: 75.2% Plastic Limit: 0.0 % #100 34% 0.150 mm % Silt: 22.2% Plasticity Index: 0.0 % #200 24.4%  $0.075 \ mm$ 24.0% 0.074 mm % Clay: Silts 14.6% 0.050 mm 10.3% 0.020 mm 2.2% 0.005 mm Clays 1.0%  $0.002\ mm$ Colloids 0.7%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Loamy Sand All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by: Meghan Blodgett-Carrillo

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1564
Sample Date:	7/12/2021
Test Date:	9/20/2021
Technician:	M. Carrillo

Sample Source: LDW21-GT13-GB-0-11 ft

Visual Soil Description: brown sand with silt

Type of Specimen: Remolded Cylindrical Shear Box

Specimen Diameter (in): 2.5

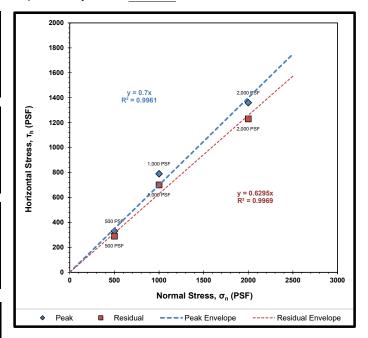
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	32.6	
	Initial	Post-Consolidation
Dry Density (PCF):	104.7	106.1
Void Ratio:	0.608	0.589
Porosity (%):	37.8	37.0
Degree of Saturation (%):	saturated	saturated

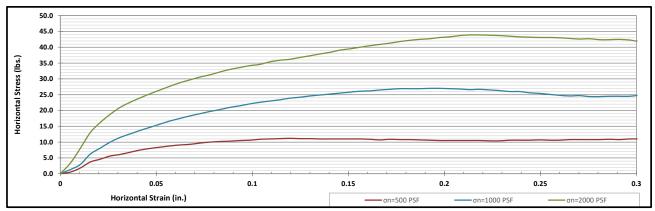
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	30.5	
	Initial	Post-Consolidation
Dry Density (PCF):	105.5	108.0
Void Ratio:	0.597	0.560
Porosity (%):	37.4	35.9
Degree of Saturation (%):	saturated	saturated

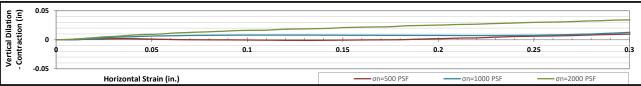
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF					
Initial Moisture Content (%):	31.4						
	Initial	Post-Consolidation					
Dry Density (PCF):	105.7	113.8					
Void Ratio:	0.595	0.481					
Porosity (%):	37.3	32.5					
Degree of Saturation (%):	saturated	saturated					

ESTIMATED STRENGTH PARAMETERS									
	PEAK	RESIDUAL							
Angle of Internal Friction, φ (°):	35	32							
Cohesion (PSF):	0	0							



Failure Envelope Test Values:								
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000					
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	330	790	1360					
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	700	1230					





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT13-GB-11-21 ft Sample#: B21-1566

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.020 \\ \textbf{D}_{(10)} = 0.040 \\ \textbf{D}_{(15)} = 0.060 \\ \textbf{D}_{(30)} = 0.107 \\ \textbf{D}_{(50)} = 0.177 \\ \textbf{D}_{(60)} = 0.230 \\ \textbf{D}_{(90)} = 0.388 \\ \textbf{D}_{(90)} = 0.388 \end{array}$ % Gravel = 0.3% % Sand = 81.0% mm % Silt & Clay = 18.7% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 1.25$ Coeff. of Uniformity,  $C_U = 5.74$ Fineness Modulus = 0.87 Plastic Limit = n/a

Moisture %, as sampled = 36.0% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

					Di	$D_{(90)} = 0.388$ ust Ratio = 17/88	mm	Fracture %, 1 Face = r		q a Fracture %, 1 d Fracture %, 2+ I	
				AS		TM D6913, ASTM	C117	Tractare 78, 2 · Taces 1	, a red	3 1 1 detaile 7 6, 2 - 1	uees
			Interpolated Cumulative		Í			Grain Size Distribution			
Sieve	Size	Percent	Percent	Specs	Specs			3". 2". 11%". 1". 1\". 1\". 55(8\". 8\". 84. #4. #16.			
US	Metric	Passing	Passing	Max	Min	10	oi⊆ eeean	3,8 2,7 1 2,7 1 2,1 1 2,	8 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		<del></del> 100.0%
12.00"	300.00		100%	100.0%	0.0%	1	Ē		##		100.0,0
10.00"	250.00		100%	100.0%	0.0%		H				1
8.00"	200.00		100%	100.0%	0.0%	9	0%	$\cdots$		+	90.0%
6.00"	150.00		100%	100.0%	0.0%		F				- 1
4.00"	100.00		100%	100.0%	0.0%						00.00
3.00"	75.00		100%	100.0%	0.0%	8	0%				80.0%
2.50"	63.00		100%	100.0%	0.0%						- 1
2.00"	50.00	100%	100%	100.0%	0.0%	7	0%				70.0%
1.75"	45.00		100%	100.0%	0.0%						1
1.50"	37.50		100%	100.0%	0.0%				1 1		1
1.25"	31.50		100%	100.0%	0.0%	6	0%		HH <b>\</b> - HH		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	D L					50.0%
3/4"	19.00	100%	100%	100.0%	0.0%	Possing 2	0%				50.0%
5/8"	16.00		100%	100.0%	0.0%	86	" F T				30.0/8 8
1/2"	12.50	100%	100%	100.0%	0.0%				11111		1
3/8"	9.50	100%	100%	100.0%	0.0%	4	0%				40.0%
1/4"	6.30		100%	100.0%	0.0%						1
#4	4.75	100%	100%	100.0%	0.0%						1
#8	2.36		99%	100.0%	0.0%	3	0%		******		30.0%
#10	2.00	99%	99%	100.0%	0.0%						1
#16	1.18		98%	100.0%	0.0%		0%		ili i i i i i i i i i i i i i i i i i i		20.0%
#20	0.850		98%	100.0%	0.0%		" F T				20.0%
#30	0.600		97%	100.0%	0.0%						1
#40	0.425	97%	97%	100.0%	0.0%	1	0%			<del>                                     </del>	10.0%
#50	0.300		73%	100.0%	0.0%						- 1
#60	0.250		64%	100.0%	0.0%						- 1
#80	0.180		51%	100.0%	0.0%		0%	100 10.000 1.000	0.100	0.010	0.0%
#100	0.150	45%	45%	100.0%	0.0%						
#140	0.106		30%	100.0%	0.0%			Particle Size (mm)			
#170	0.090		24%	100.0%	0.0%						
#200	0.075	18.7%	18.7%	100.0%	0.0%	+ Sie	ve Sizes	—▲ — Max Specs —	- Min Specs	Sieve Results	
Copyright	Spears Engineering & Tec	hnical Services PS, 1996-9	8								



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT13-GB-21-31 ft Sample#: B21-1568

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.021 \\ \textbf{D}_{(10)} = 0.042 \\ \textbf{D}_{(15)} = 0.063 \\ \textbf{D}_{(30)} = 0.109 \\ \textbf{D}_{(50)} = 0.177 \\ \textbf{D}_{(60)} = 0.229 \\ \textbf{D}_{(90)} = 0.385 \\ \textbf{Ratio} = 13/71 \\ \end{array}$ % Gravel = 0.1% % Sand = 82.1% mm % Silt & Clay = 17.9% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 1.23$ Coeff. of Uniformity,  $C_U = 5.46$ Fineness Modulus = 0.85

Plastic Limit = n/a Moisture %, as sampled = 34.3% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

						ust Ratio = 13			Fract	ure %,	2+ Fa	ices =	n/a		Re	q'd Fr	acture	e %, 2	+ Fac	es =
			T. 1. 2	AS	TM C136, AS	TM D6913, AS	STM C11	1												
		Actual	Interpolated			ľ			G	rain Size	Distribu	rtion								
		1	Cumulative	-					E+											
Sieve		Percent	Percent	Specs	Specs		<u>.</u> 6	90 ft ft 60 ft	2.8	5/8%	- 2	22 29	8 8 8	8888	828					
US	Metric	Passing	Passing	Max	Min								1414	1111	+	П		ПП		T 100.0%
12.00"	300.00		100%	100.0%	0.0%								TT 1							}
10.00"	250.00		100%	100.0%	0.0%		-													1
8.00"	200.00		100%	100.0%	0.0%		90%								-1111			1111		90.0%
6.00"	150.00		100%	100.0%	0.0%		t													1
4.00"	100.00		100%	100.0%	0.0%		80%								ЩЩ	Ш		Ш		80.0%
3.00"	75.00		100%	100.0%	0.0%															1
2.50"	63.00		100%	100.0%	0.0%									1						}
2.00"	50.00	100%	100%	100.0%	0.0%		70%					-		-				-		70.0%
1.75"	45.00		100%	100.0%	0.0%									1						1
1.50"	37.50		100%	100.0%	0.0%									ì						1
1.25"	31.50		100%	100.0%	0.0%		60%					-	####	+	-11111			***		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0	ŀ							1						2.0
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50%													50.0%
5/8"	16.00		100%	100.0%	0.0%	PG	30% F							1				Ш		T 30.0% 88
1/2"	12.50	100%	100%	100.0%	0.0%									1						1
3/8"	9.50	100%	100%	100.0%	0.0%		40%					4		+		-		₩.	_	40.0%
1/4"	6.30		100%	100.0%	0.0%															1
#4	4.75	100%	100%	100.0%	0.0%		t								1					1
#8	2.36		100%	100.0%	0.0%		30%			-		-	####	++-	•	-		+++		30.0%
#10	2.00	100%	100%	100.0%	0.0%		ŀ								NII.					}
#16	1.18		99%	100.0%	0.0%		20%								1					20.0%
#20	0.850		98%	100.0%	0.0%		20%											Ш		20.0%
#30	0.600		98%	100.0%	0.0%		-													1
#40	0.425	98%	98%	100.0%	0.0%		10%		444-				Ш.			Ш.		Ш.	_	10.0%
#50	0.300		74%	100.0%	0.0%		ŀ													1
#60	0.250		64%	100.0%	0.0%		t													1
#80	0.180		51%	100.0%	0.0%		0%	100.000	debbo	10.000		1.00		40-00	0.100	ш	0.010	ш.	<del>-</del>	<b>↓</b> 0.0% .001
#100	0.150	45%	45%	100.0%	0.0%			100.000		10.000		1.00		,	2.700		0.010	,	U	
#140	0.106		29%	100.0%	0.0%					Po	article Size	e (mm)								
#170	0.090		23%	100.0%	0.0%															
#200	0.075	17.9%	17.9%	100.0%	0.0%		Sieve Size	5		■ Max Sp	ecs	_	<b>-</b>	Min Spec	s	_		iieve Res	ults	
		hnical Services PS, 1996-9		100.070	0.070	<u> </u>	2.310 0120		_						-					



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT19-GB-0-6.9 ft

Sample#: B21-1571

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

ML, Silt with Sand Sample Color:

brown

## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{AS | M | D431} \\ \textbf{D}_{(5)} = 0.004 \\ \textbf{D}_{(10)} = 0.007 \\ \textbf{D}_{(15)} = 0.009 \\ \textbf{D}_{(30)} = 0.019 \\ \textbf{D}_{(50)} = 0.051 \\ \textbf{D}_{(60)} = 0.062 \\ \textbf{D}_{(90)} = 0.186 \end{array}$ % Gravel = 1.2% % Sand = 27.1% mm % Silt & Clay = 71.7% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a mm

Coeff. of Curvature,  $C_C = 0.88$ Coeff. of Uniformity,  $C_U = 9.46$ Fineness Modulus = 0.29

Plastic Limit = 0.0% Moisture %, as sampled = 78.2% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

					D	$D_{(90)} = 0.186$ ust Ratio = 59/79	mm	Fracture %, 1 Face = n/a Req'd Fracture %, 1 Fac Fracture %, 2+ Faces = n/a Req'd Fracture %, 2+ Face	
				AS	TM C136, AS	ГМ D6913, ASTM С	117		
		Actual	Interpolated					Grain Size Distribution	
		Cumulative	Cumulative					±.	
	Size	Percent	Percent	Specs	Specs		b	25.55 27.77 27.77 27.78 27.78 28.88 28	
US	Metric	Passing	Passing	Max	Min				100.0%
12.00"	300.00		100%	100.0%	0.0%				
10.00"	250.00		100%	100.0%	0.0%				
8.00"	200.00		100%	100.0%	0.0%	90%	1		90.0%
6.00"	150.00		100%	100.0%	0.0%				
4.00"	100.00		100%	100.0%	0.0%	80%	·		80.0%
3.00"	75.00		100%	100.0%	0.0%	00,0			00.070
2.50"	63.00		100%	100.0%	0.0%		F		
2.00"	50.00	100%	100%	100.0%	0.0%	70%	: ∔		70.0%
1.75"	45.00		100%	100.0%	0.0%				
1.50"	37.50		100%	100.0%	0.0%				
1.25"	31.50		100%	100.0%	0.0%	60%	: <del>    -</del>		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	2	ł I		- 50.0%
3/4"	19.00	100%	100%	100.0%	0.0%	50% 500 800 800 800 800 800 800 800 800 800	.		50.007 S
5/8"	16.00		100%	100.0%	0.0%	P6 20%	T		30.0%
1/2"	12.50	100%	100%	100.0%	0.0%				
3/8"	9.50	100%	100%	100.0%	0.0%	40%	; ‡‡		40.0%
1/4"	6.30		99%	100.0%	0.0%				
#4	4.75	99%	99%	100.0%	0.0%				
#8	2.36		98%	100.0%	0.0%	30%	; <del>[                                    </del>	<del></del>	30.0%
#10	2.00	98%	98%	100.0%	0.0%		+		
#16	1.18		97%	100.0%	0.0%			_	
#20	0.850		96%	100.0%	0.0%	20%	T		20.0%
#30	0.600		96%	100.0%	0.0%			-	
#40	0.425	96%	96%	100.0%	0.0%	10%	; 📙		10.0%
#50	0.300		93%	100.0%	0.0%				
#60	0.250		92%	100.0%	0.0%		H		
#80	0.180		90%	100.0%	0.0%	0%		100,000 10,000 1,000 0,100 0,010 0,0	0.0%
#100	0.150	89%	89%	100.0%	0.0%			10.000 10.000 1.000 0.100 0.010 0.0	UI
#140	0.106	03.0	79%	100.0%	0.0%			Particle Size (mm)	
#170	0.090		75%	100.0%	0.0%				
#200	0.075	71.7%	71.7%	100.0%	0.0%	+ Sieve	Sizes	→ Max Specs	
	t Spears Engineering & Tec	,	,	100.070	0.070	1 3,040	JEC3	——————————————————————————————————————	
				and ourselves, all reports are	submitted as the confide	ntial property of clients, and auth	orization	n for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our	written an



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client ML, Silt with Sand Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT19-GB-0-6.9 ft Tested By: C. Kriss brown Sample#: B21-1571 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.61 Sieve Analysis Sample Weight: 50.97 **Grain Size Distribution** Hydroscopic Moist.: 2.35% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 49.80 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0488 mm 100% 25.000 mm 24.5 48 4% 1.0" 38.6% 0.0356 mm 3/4" 100% 19.000 mm 2 19.5 17.5 34.6%  $0.0228\ mm$ 5/8" 100% 16.000 mm 15 23.7%  $0.0135 \ mm$ 1/2" 100% 12.500 mm 30 17.8% 0.0097 mm 3/8" 100% 9.500 mm 0.0070 mm 60 5.5 10.9% 1/4" 99% 6.300 mm 240 2.5 4.9% 0.0036 mm 99% 4.750 mm #4 2.0% #10  $2.000\ mm$ 1440  $0.0015 \ mm$ 98% #20 96% 0.850 mm Liquid Limit: 0.0 % % Gravel: 1.2% #40 96%  $0.425 \, mm$ % Sand: 27.1% Plastic Limit: 0.0 % #100 89% 0.150 mm % Silt: 64.3% Plasticity Index: 0.0 % #200 71.7%  $0.075 \ mm$ 70.8% 0.074 mm % Clay: Silts 56.9% 0.050 mm 31.3% 0.020 mm 7.4% 0.005 mm Clays 2.7%  $0.002\ mm$ Colloids 1.3%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway
Project #: 21B233 Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 ML. Silt with Sand Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT19-GB-0-6.9 ft Tested By: C. Kriss Sample #: B21-1571 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Liquid limit cannot be established Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A Plasticity Index, I<sub>P</sub>: % Moisture: N/A Number of Blows: Weight of Wet Soils + Pan: Plastic limit cannot be determined Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 80.0 % 100% 70.0 % 90% 60.0 % A" Line Plasticity Index 50.0 % 40.0 % 50% 30.0 % CL or OL MH or OH 20% 10.0 % 10% ML or OL 0.0 % 50% 10 100 **Liquid Limit** Copyright Spears Engineering & Technical Services PS, 1996-98

Au results apply only to extent accurates and materiast tested. As a mutual protection to citeris, the puote and ourserves, an reports are summitted as the continental property of citeris, and authorization for punication of statements, concussors of extracts from or regarding our reports is reserved pending our written approval.

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT19-GB-6.9-8.5 ft Sample#: B21-1572

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

mm

brown



### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{ASIN D43} \\ \textbf{D}_{(5)} = 0.068 \\ \textbf{D}_{(10)} = 0.168 \\ \textbf{D}_{(15)} = 0.215 \\ \textbf{D}_{(30)} = 0.356 \\ \textbf{D}_{(50)} = 0.749 \\ \textbf{D}_{(60)} = 1.076 \\ \textbf{D}_{(90)} = 1.777 \\ \textbf{Partia} = 0.061 \end{array}$ % Gravel = 0.3% % Sand = 94.2% mm % Silt & Clay = 5.5% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 0.75$ Coeff. of Uniformity,  $C_U = 5.98$ Fineness Modulus = 2.59

Plastic Limit = n/a Moisture %, as sampled = 27.9% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

	•	Actual Cumulative	Interpolated Cumulative	•						ain Size Dis								
Sieve	Size	Percent	Percent	Specs	Specs		h .		7. 1.7. % 1.7.1.7. %	io <sup>is</sup> in :	. <sub>m</sub> o	202	2888	88 88				
US	Metric	Passing	Passing	Max	Min		100% ♣♠.	v <b>o 4</b> ‰	• <b>• • .•</b> .•	કે કે કે • <b>ભ</b> ્રામ•	**	# # 2	* * * *	## ## T				<b>T</b> 100.0
12.00"	300.00		100%	100.0%	0.0%		T				Ti	III						1
10.00"	250.00		100%	100.0%	0.0%		ŀ				111							1
8.00"	200.00		100%	100.0%	0.0%		90%		+++-+		+++		++-+-					90.0%
6.00"	150.00		100%	100.0%	0.0%		-				111							1
4.00"	100.00		100%	100.0%	0.0%													1
3.00"	75.00		100%	100.0%	0.0%		80%											80.0%
2.50"	63.00		100%	100.0%	0.0%							<b>\</b>						1
2.00"	50.00	100%	100%	100.0%	0.0%		70%											70.0%
1.75"	45.00		100%	100.0%	0.0%							1						
1.50"	37.50		100%	100.0%	0.0%		ł					1						1
1.25"	31.50		100%	100.0%	0.0%		60%		++++		+++	-1			+++		+++	60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	D	}					N.						1
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing						ì						50.0%
5/8"	16.00		100%	100.0%	0.0%	Pic	50%				$\Box$	1			T			50.0%
1/2"	12.50	100%	100%	100.0%	0.0%		ļ.					1						1
3/8"	9.50	100%	100%	100.0%	0.0%		40%						Ш					40.0%
1/4"	6.30		100%	100.0%	0.0%		ŀ											1
#4	4.75	100%	100%	100.0%	0.0%		ŀ						<b>N</b>					1
#8	2.36		99%	100.0%	0.0%		30%		+++-+		╁┼┼		+		++-		+++	30.0%
#10	2.00	99%	99%	100.0%	0.0%		-						Ĭ					1
#16	1.18		67%	100.0%	0.0%								Ĭ					20.0%
#20	0.850		54%	100.0%	0.0%		20%				T		1					20.0%
#30	0.600		44%	100.0%	0.0%								<b> </b>					1
#40	0.425	37%	37%	100.0%	0.0%		10%	ЩЩ	++++		444		1		$\Box$		444	10.0%
#50	0.300		24%	100.0%	0.0%		ŀ											1
#60	0.250		19%	100.0%	0.0%		ł							111				1
#80	0.180		11%	100.0%	0.0%		0%	100.000		10.000	i io	1.000	0-00-0	0.100		0.010		0.0%
#100	0.150	8%	8%	100.0%	0.0%			100.000		.0.000		1.000		5.100		0.010		0.001
#140	0.106		7%	100.0%	0.0%					Partic	le Size (mr	n)						
#170	0.090		6%	100.0%	0.0%													
#200	0.075	5.5%	5.5%	100.0%	0.0%		<ul> <li>Sieve Sizes</li> </ul>			Max Specs			— Min Spe	ecs	_	Sieve	Results	
Copyright		1		100.070	0.070	<b>I</b> k .				,								

Comments:		
Reviewed by:	Mayh Blaket and lo	
	Meghan Blodgett-Carrillo	



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT19-GB-8.5-18.5 ft

Sample#: B21-1574

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 1-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

2.36

2.00

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#10 #16

#20

#30

#40

#50

#60

#80 #100

#140

#170

#200

Sample Meets Specs ? N/A

 $\begin{array}{c} D_{(5)} = 0.103 \\ D_{(10)} = 0.155 \\ D_{(15)} = 0.177 \\ D_{(30)} = 0.242 \\ D_{(30)} = 0.232 \end{array}$ % Gravel = 0.0%% Sand = 97.3% mm % Silt & Clay = 2.7% mm Liquid Limit = n/a mm  $D_{(50)} = 0.328$ mm Plasticity Index = n/a  $D_{(60)} = 0.372$ mm Sand Equivalent = n/a  $D_{(90)} = 1.435$ Oust Ratio = 2/53

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

Coeff. of Curvature,  $C_C = 1.01$ Coeff. of Uniformity,  $C_U = 2.40$ Fineness Modulus = 1.87

Plastic Limit = n/a Moisture %, as sampled = 25.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					Dι
				AS	TM C136, AST
		Actual Cumulative	Interpolated Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%

100%

100%

86%

80%

75%

72%

43%

32%

16%

5%

4%

2.7%

72%

100.0%

100.0%

100.0%

100.0%

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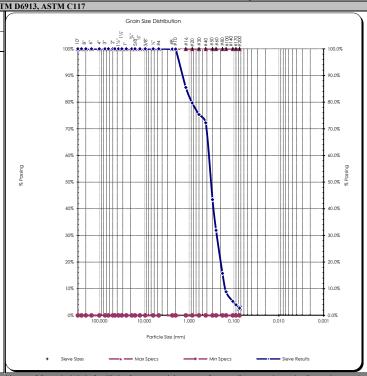
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Reviewed by: Meghan Blodgett-Carrillo

## **Direct Shear Test Results:**

#### ASTM D-3080



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1574
Sample Date:	7/13/2021
Test Date:	9/21/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT19-GB-8.5-18.5 ft

 Visual Soil Description:
 brown sand with silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

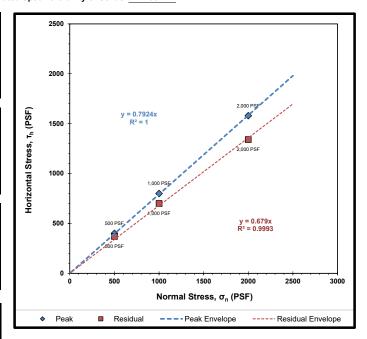
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	27.5	
	Initial	Post-Consolidation
Dry Density (PCF):	106.2	107.3
Void Ratio:	0.586	0.570
Porosity (%):	37.0	36.3
Degree of Saturation (%):	saturated	saturated

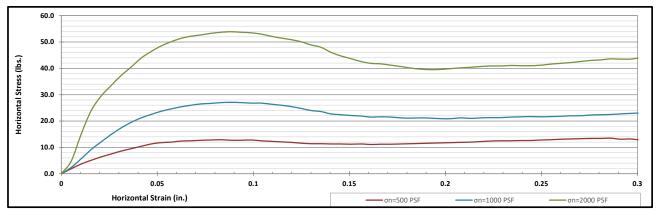
Summary of Samp	σ <sub>n</sub> =1000 PSF	
Initial Moisture Content (%):	tial Moisture Content (%): 26.1	
	Initial	Post-Consolidation
Dry Density (PCF):	108.0	109.7
Void Ratio:	0.560	0.536
Porosity (%):	35.9	34.9
Degree of Saturation (%):	saturated	saturated

Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	24.7	
	Initial	Post-Consolidation
Dry Density (PCF):	109.2	111.5
Void Ratio:	0.543	0.511
Porosity (%):	35.2	33.8
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS				
	PEAK	RESIDUAL		
Angle of Internal Friction, φ (°):	38	34		
Cohesion (PSF):	0	0		



Failure Envelope Test Values:					
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000		
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	400	800	1580		
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	370	700	1340		





Corporate • 777 Chrysler Drive • Burlington, WA 98233 • Phone 360.755.1990 • Fax 360.755.1980 SW Region • 2118 Black Lake Blvd. S.W.• Olympia, WA 98512 • Phone 360.534.9777 • Fax 360.534.9779 NW Region • 805 Dupont, Suite #5 • Bellingham, WA 98225 • Phone 360.647.6061 • Fax 360.647.8111 Kitsap Region • 5451 N.W. Newberry Hill Road, Suite 101 • Silverdale, WA 98383 • Phone/Fax 360.698.6787



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT19-GB-18.5-28.5 ft Sample#: B21-1576

Sample Meets Specs? N/A

Specifications

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

No Specs

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 1-Sep-21

Tested By: C. Kriss

SP-SM, Poorly graded Sand with Silt Sample Color:

mm

brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

 $D_{(5)} = 0.058$   $D_{(10)} = 0.092$   $D_{(15)} = 0.117$   $D_{(30)} = 0.185$ % Gravel = 0.0%% Sand = 93.6% mm % Silt & Clay = 6.4% mm Liquid Limit = n/a mm  $D_{(50)} = 0.271$ mm  $D_{(60)} = 0.314$ mm

Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Moisture %, as sampled = 27.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Coeff. of Curvature,  $C_C = 1.18$ Coeff. of Uniformity,  $C_U = 3.40$ 

Fineness Modulus = 1.41

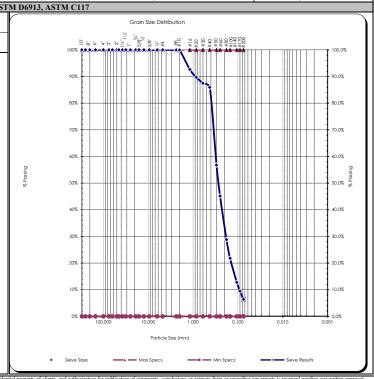
Plastic Limit = n/a

 $D_{(90)} = 0.882$ Dust Ratio = 5/67

Unified Soil Classification System, ASTM-2487

Reg'd Fracture %, 2+ Faces =

					D
		Actual Cumulativ	Interpolated Cumulative	AS	STM C136, AS
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		93%	100.0%	0.0%
#20	0.850		90%	100.0%	0.0%
#30	0.600		87%	100.0%	0.0%
#40	0.425	86%	86%	100.0%	0.0%



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Reviewed by: Meghan Blodgett-Carrillo

57%

45%

29%

22%

13%

10%

6.4%



Client:	Anchor QEA	Date:	October 5, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1693-1706
Revised on:		Date sampled:	July 14, 2021

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 13, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1693	LDW21-GT37-GB-0-1.5 ft	233.7	583.3	440.8	142.5	207.1	68.8%
B21-1694	LDW21-GT37-GB-10-11.5 ft	302.0	688.9	534.6	154.3	232.6	66.3%
B21-1695	LDW21-GT37-GB-10-20 ft	234.3	678.9	534.1	144.8	299.8	48.3%
B21-1696	LDW21-GT37-GB-20-21.5 ft	341.8	864.9	644.8	220.1	303.0	72.6%
B21-1697	LDW21-GT37-GB-20-30 ft	316.0	945.0	766.3	178.7	450.3	39.7%
B21-1698	LDW21-GT37-GB-30-31.5 ft	346.9	1041.2	892.0	149.2	545.1	27.4%
B21-1699	LDW21-GT18-GB-0-1.5 ft	360.3	577.1	507.3	69.8	147.0	47.5%
B21-1700	LDW21-GT18-GB-0-6.5 ft	233.5	726.8	590.5	136.3	357.0	38.2%
B21-1701	LDW21-GT18-GB-6.5-8 ft	357.0	752.8	656.6	96.2	299.6	32.1%
B21-1702	LDW21-GT18-GB-6.5-16.5 ft	217.3	795.2	684.7	110.5	467.4	23.6%
B21-1703	LDW21-GT18-GB-16.5-18 ft	354.3	1016.0	893.3	122.7	539.0	22.8%
B21-1704	LDW21-GT18-GB-16.5-21.4 ft	10.2	159.2	118.5	40.7	108.3	37.6%
B21-1705	LDW21-GT18-GB-21.4-26.5 ft	690.5	1366.5	1179.1	187.4	488.6	38.4%
B21-1706	LDW21-GT18-GB-26.5-28 ft	359.5	929.9	801.2	128.7	441.7	29.1%
+							

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 13, 2021	Tested by: A. Eifrig

									Mass of Pycno filled		Temp of		Temp.	
			Dry Soil +	Mass of Dry		Mass of	Volume of	Density of	w/ water &				Correction	Corrected
Sample #	Location	Tare	Tare	Soil	Pycno ID	Pycno	Pycno	Water @ Tx		w/ water	*C	Soils	Factor	SpG
B21-1695	LDW21-GT37-GB-10-20 ft	493.21	568.13	74.9	TSA-013	184.0	499.7	0.99756	728.81	682.44	22.9	2.6240964	0.99936	
B21-1697	LDW21-GT37-GB-20-30 ft	497.94	575.45	77.5	TSA-011	190.3	499.5	0.99752	736.61	688.63	23.1	2.624687	0.99931	2.6228759
B21-1700	LDW21-GT18-GB-0-6.5 ft	600.24	700.15	99.9	TSA-020	195.0	499.5	0.99752	753.52	693.28	23.1	2.5184539	0.99931	2.5167161
B21-1702	LDW21-GT18-GB-6.5-16.5 ft	510.32	612.20	101.9	TSA-010	180.3	499.5	0.99754	742.28	678.62		2.6655395		2.6637535
B21-1705	LDW21-GT18-GB-21.4-26.5 ft	501.27	576.59	75.3	TSA-021	183.4	499.4	0.99745	727.11	681.56	23.4	2.5303609	0.99924	2.5284379
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#10

#16

#20

#30

#40 #50

#60

#80 #100

#140

#170

#200

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

93%

Source: LDW21-GT37-GB-10-20 ft Sample#: B21-1695

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 13-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.003$   $D_{(10)} = 0.007$   $D_{(15)} = 0.016$ % Gravel = 0.5%% Sand = 57.8% mm % Silt & Clay = 41.7% mm  $D_{(30)} = 0.057$ Liquid Limit = 0.0% mm  $D_{(50)} = 0.097$ mm Plasticity Index = 0.0%  $D_{(60)} = 0.124$ mm Sand Equivalent = n/a  $D_{(90)} = 0.386$ mm Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 3.61$ Coeff. of Uniformity,  $C_U = 17.03$ Fineness Modulus = 0.59

Plastic Limit = 0.0% Moisture %, as sampled = 48.3% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

Dust Ratio =	21/47	Fract
136, ASTM D6913,	ASTM C117	

					Dı
				A	STM C136, AST
		Actual Cumulativ	Interpolated e Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	99%	99%	100.0%	0.0%
#8	2.36		99%	100.0%	0.0%

99%

96%

95%

94%

93%

83%

78%

72%

69%

53%

47%

41.7%

100.0%

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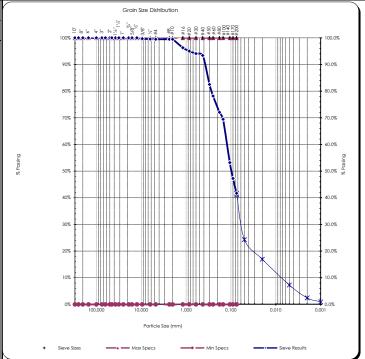
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**Comments:** Reviewed by: Meghan Blodgett-Carrillo



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 13-Sep-21 Sample Color Source: LDW21-GT37-GB-10-20  $\operatorname{ft}$ Tested By: C. Kriss brown Sample#: B21-1695 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.62 Sieve Analysis Sample Weight: 74.76 **Grain Size Distribution** Hydroscopic Moist.: 2.84% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 72.70 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 25.6% 0.0505 mm 100% 25.000 mm 18.5 1.0" 3/4" 100% 19.000 mm 2 15.5 21.4% 0.0364 mm 13.5 18.7%  $0.0234\ mm$ 5/8" 100% 16.000 mm 15 13.8%  $0.0137 \ mm$ 1/2" 100% 12.500 mm 30 12.4% 0.0097 mm 3/8" 100% 9.500 mm 0.0070 mm 60 9.7% 1/4" 100% 6.300 mm 240 5.5% 0.0035 mm 99% 4.750 mm #4 1.4% #10 99%  $2.000 \ mm$ 1440  $0.0015 \ mm$ #20 95% 0.850 mm Liquid Limit: 0.0 % % Gravel: 0.5% #40 93%  $0.425 \, mm$ % Sand: 57.8% Plastic Limit: 0.0 % #100 69% 0.150 mm % Silt: 34.4% Plasticity Index: 0.0 % #200 41.7%  $0.075 \ mm$ 41.1% 0.074 mm % Clay: 7.3% Silts 24.3% 0.050 mm 0.020 mm 17.0% 7.3% 0.005 mm Clays 2.5%  $0.002\ mm$ Colloids 0.9% $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Loamy Sand All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1695
Sample Date:	7/14/2021
Test Date:	9/16/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT37-GB-10-20 ft

 Visual Soil Description:
 brown silty sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

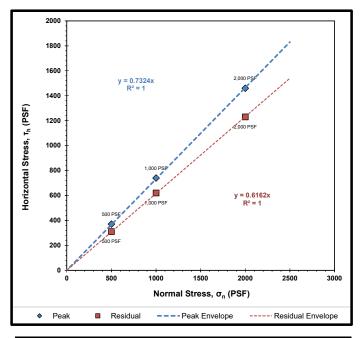
 Specimen Diameter (in):
 2.5

Summary of Sample	σ <sub>n</sub> =500 PSF	
nitial Moisture Content (%): 35.3		
	Initial	Post-Consolidation
Dry Density (PCF):	100.7	102.8
Void Ratio:	0.673	0.639
Porosity (%):	40.2	39.0
Degree of Saturation (%):	saturated	saturated

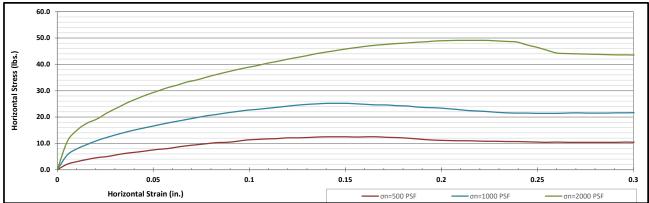
Summary of Sample Data:		σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	36.0	
	Initial	Post-Consolidation
Dry Density (PCF):	100.9	110.5
Void Ratio:	0.670	0.525
Porosity (%):	40.1	34.4
Degree of Saturation (%):	saturated	saturated

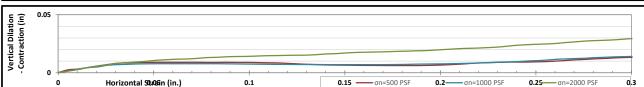
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	35.4	
	Initial	Post-Consolidation
Dry Density (PCF):	101.4	114.5
Void Ratio:	0.662	0.471
Porosity (%):	39.8	32.0
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS							
PEAK RESIDUAL							
Angle of Internal Friction, φ (°):	36	32					
Cohesion (PSF):	0	0					



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	370	740	1460				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	310	620	1230				





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT37-GB-20-30 ft

Sample#: B21-1697

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 13-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.013 \\ \textbf{D}_{(10)} = 0.025 \\ \textbf{D}_{(15)} = 0.038 \\ \textbf{D}_{(30)} = 0.077 \\ \textbf{D}_{(50)} = 0.165 \\ \textbf{D}_{(60)} = 0.234 \\ \textbf{D}_{(90)} = 0.767 \end{array}$ % Gravel = 0.2% % Sand = 70.3% mm % Silt & Clay = 29.5% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a  $\sqrt{6}$ , 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.00$ Coeff. of Uniformity,  $C_U = 9.20$ Fineness Modulus = 1.03

Plastic Limit = 0.0% Moisture %, as sampled = 39.7% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.7$	67 mm		Fract	ure
						ust Ratio = 1			Fractur	e %
				A	STM C136, AS	ΓM D6913, AS	STM C117			
		Actual Cumulative	Interpolated Cumulative						Grain	
Sieve	Size	Percent	Percent	Specs	Specs		ъ.	6 44 V		. ×.
US	Metric	Passing	Passing	Max	Min		100%	~~~*\****		
12.00"	300.00		100%	100.0%	0.0%		11			
10.00"	250.00		100%	100.0%	0.0%		11			
8.00"	200.00		100%	100.0%	0.0%		90%			-#
6.00"	150.00		100%	100.0%	0.0%		ł I			
4.00"	100.00		100%	100.0%	0.0%		80%			
3.00"	75.00		100%	100.0%	0.0%		00% FT			
2.50"	63.00		100%	100.0%	0.0%		1.1			
2.00"	50.00	100%	100%	100.0%	0.0%		70%			-#
1.75"	45.00		100%	100.0%	0.0%		<b>!</b>			
1.50"	37.50		100%	100.0%	0.0%		<u> </u>			
1.25"	31.50		100%	100.0%	0.0%		60%		++-+-	$\dashv$
1.00"	25.00	100%	100%	100.0%	0.0%	0	<u> </u>			
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%			
5/8"	16.00		100%	100.0%	0.0%	96	50%			
1/2"	12.50	100%	100%	100.0%	0.0%		F			
3/8"	9.50	100%	100%	100.0%	0.0%		40%			-#
1/4"	6.30		100%	100.0%	0.0%		11			
#4	4.75	100%	100%	100.0%	0.0%		11			
#8	2.36		98%	100.0%	0.0%		30%		++-+-	-#
#10	2.00	98%	98%	100.0%	0.0%		ł l			
#16	1.18		93%	100.0%	0.0%		20%			
#20	0.850		91%	100.0%	0.0%		20%			
#30	0.600		89%	100.0%	0.0%		F 1			
#40	0.425	88%	88%	100.0%	0.0%		10%		++-	$-\!$
#50	0.300		70%	100.0%	0.0%					
#60	0.250		62%	100.0%	0.0%					
#80	0.180		52%	100.0%	0.0%		0%	100,000	1000-00	10.000
#100	0.150	48%	48%	100.0%	0.0%					

100.0%

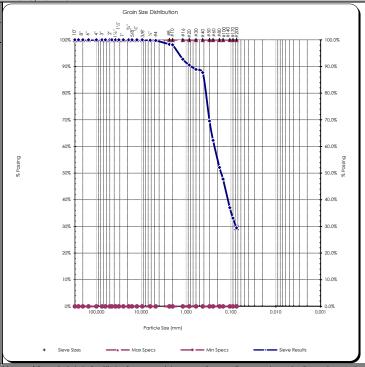
100.0%

100.0%

37%

33%

29.5%



**Comments:** 

0.0%

0.0%

0.0%

Meghan Blodgett-Carrillo

29.5%

0.106

0.090

0.075

#140

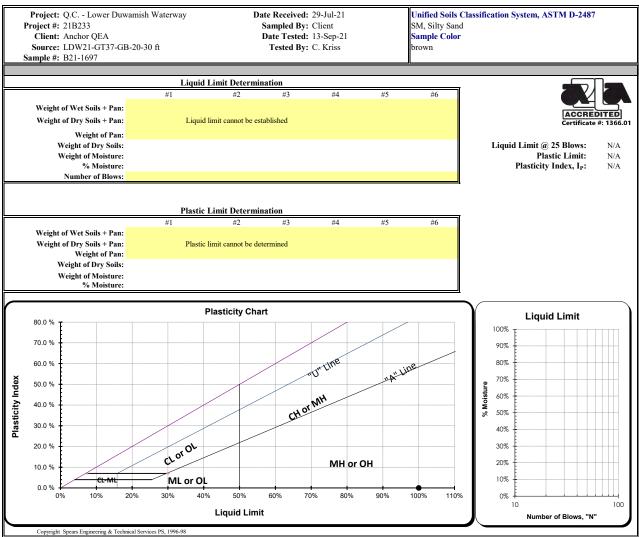
#170

#200

Reviewed by:



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



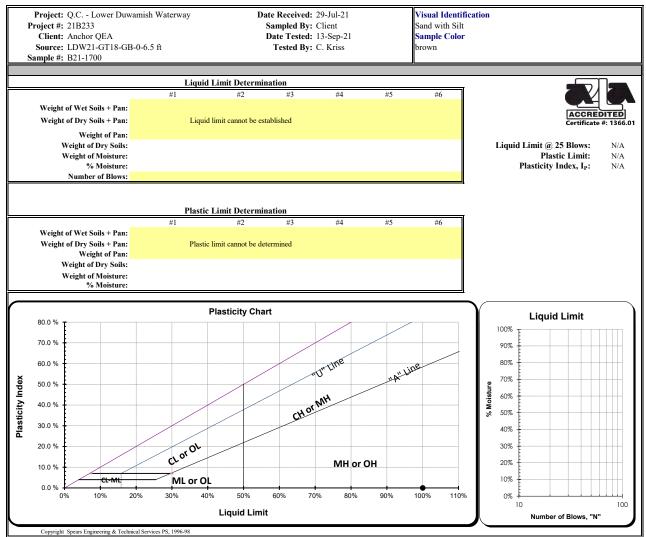
All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT18-GB-6.5-16.5 ft

Sample#: B21-1702

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 13-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



Coeff. of Curvature,  $C_C = 1.00$ Coeff. of Uniformity,  $C_U = 2.29$ 

Fineness Modulus = 1.97

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

#140

#170

#200

**Comments:** 

Sample Meets Specs? N/A

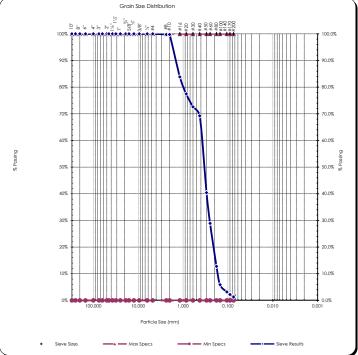
 $D_{(5)} = 0.136$   $D_{(10)} = 0.168$   $D_{(15)} = 0.190$   $D_{(30)} = 0.255$ % Gravel = 0.0%% Sand = 98.7% mm % Silt & Clay = 1.3% mm Liquid Limit = n/a mm  $D_{(50)} = 0.342$ mm Plasticity Index = n/a  $D_{(60)} = 0.385$ mm Sand Equivalent = n/a  $D_{(90)} = 1.497$ Dust Ratio = 1/54 Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

Plastic Limit = n/a Moisture %, as sampled = 23.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

ASTM C136, ASTM D6913, ASTM C117

Specs	Specs	
Max	Min	
100.0%	0.0%	

				AS	1 WI C130, AS
		Actual	Interpolated		
		Cumulative	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		84%	100.0%	0.0%
#20	0.850		77%	100.0%	0.0%
#30	0.600		73%	100.0%	0.0%
#40	0.425	69%	69%	100.0%	0.0%
#50	0.300		40%	100.0%	0.0%
#60	0.250		29%	100.0%	0.0%
#80	0.180		13%	100.0%	0.0%



0.0%

0.0%

0.0%

0.0%

Reviewed by:

1.3%

6%

3%

2%

1.3%

100.0%

100.0%

100.0%

100.0%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT18-GB-16.5-21.4 ft

Sample#: B21-1704

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 13-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.005$   $D_{(10)} = 0.014$   $D_{(15)} = 0.038$   $D_{(30)} = 0.081$   $D_{(50)} = 0.122$ % Gravel = 0.0%% Sand = 72.8% mm % Silt & Clay = 27.2% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0%  $D_{(60)} = 0.142$ mm Sand Equivalent = n/a

Coeff. of Curvature,  $C_C = 3.31$ Coeff. of Uniformity,  $C_U = 10.24$ Fineness Modulus = 0.53

Plastic Limit = 0.0% Moisture %, as sampled = 37.6% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.351$	mm	F	racture %,	1 Face	= n/a	
					Dı	ust Ratio = 3/11		Fra	cture %, 2-	+ Faces	= n/a	
				AS	STM C136, AST	TM D6913, ASTM	I C117					
		Actual	Interpolated						Grain Size Dis	stribution		
		7	Cumulative									
Sieve		Percent	Percent	Specs	Specs		b 1, 1	<u>2</u> . با با با با با	3/8"	, ∞2 ;	288	\$ 8 s
US	Metric	Passing	Passing	Max	Min		100%			-	• <b>*</b> •*•*	**
12.00"	300.00		100%	100.0%	0.0%							1
10.00"	250.00		100%	100.0%	0.0%		11					1
8.00"	200.00		100%	100.0%	0.0%		90%			_	-11111	1
6.00"	150.00		100%	100.0%	0.0%		ł I					
4.00"	100.00		100%	100.0%	0.0%		80%					li
3.00"	75.00		100%	100.0%	0.0%		00%					
2.50"	63.00		100%	100.0%	0.0%							
2.00"	50.00	100%	100%	100.0%	0.0%		70%					Ж
1.75"	45.00		100%	100.0%	0.0%							
1.50"	37.50		100%	100.0%	0.0%		<u> </u>					
1.25"	31.50		100%	100.0%	0.0%		60%			++-+-		++
1.00"	25.00	100%	100%	100.0%	0.0%	2	H					
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50%					
5/8"	16.00		100%	100.0%	0.0%	P6	30%					П
1/2"	12.50	100%	100%	100.0%	0.0%		11					
3/8"	9.50	100%	100%	100.0%	0.0%		40%					Щ.
1/4"	6.30		100%	100.0%	0.0%							
#4	4.75	100%	100%	100.0%	0.0%		<u> </u>					
#8	2.36		100%	100.0%	0.0%		30%			+++-		#
#10	2.00	100%	100%	100.0%	0.0%		H					
#16	1.18		100%	100.0%	0.0%		20%					
#20	0.850		100%	100.0%	0.0%		20%					m
#30	0.600		100%	100.0%	0.0%		11					
#40	0.425	100%	100%	100.0%	0.0%		10%	_####		444-		4
#50	0.300		83%	100.0%	0.0%		<b>!</b>					Ш
#60	0.250		77%	100.0%	0.0%		ł I					
#80	0.180		68%	100.0%	0.0%		0%	100.000	10.000	<del>                                     </del>	1.000	-01
#100	0.150	64%	64%	100.0%	0.0%			100.000	10.000	'	.000	
			2.770	2.2.510.70	2.070	II						

100.0%

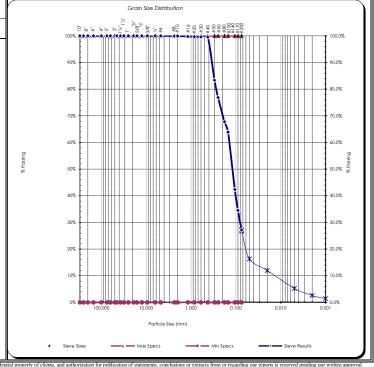
100.0%

100.0%

42%

35%

27.2%



0.0%

0.0%

0.0%

Comments:			
-			
1 . 00	n 10-11		

Reviewed by: Meghan Blodgett-Carrillo

0.106

0.090

0.075

27.2%

#140

#170

#200



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 1-Sep-21 Sample Color Source: LDW21-GT18-GB-16.5-21.4 ft Tested By: C. Kriss brown Sample#: B21-1704 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.53 Sieve Analysis Sample Weight: 99.41 **Grain Size Distribution** Hydroscopic Moist.: 2.98% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 96.53 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0526 mm 100% 25.000 mm 17 18 1% 1.0" 14.9% 0.0379 mm 3/4" 100% 19.000 mm 2 14 12.5 13.3%  $0.0242 \ mm$ 5/8" 100% 16.000 mm 15 9.5 10.1% 0.0142 mm 1/2" 100% 12.500 mm 30 8.5% 0.0101 mm 3/8" 100% 9.500 mm 60 6.5 6.9% 0.0072 mm 1/4" 100% 6.300 mm 240 4.3% 0.0036 mm 100% 4.750 mm #4 #10 100%  $2.000\ mm$ 1440 2.1%  $0.0015 \ mm$ #20 100% 0.850 mm Liquid Limit: 0.0 % % Gravel: 0.0% #40 100%  $0.425 \, mm$ % Sand: 72.8% Plastic Limit: 0.0 % #100 64% 0.150 mm % Silt: 21.9% Plasticity Index: 0.0 % #200 27.2%  $0.075 \ mm$ 26.8% 0.074 mm % Clay: 5.3% Silts 16.4% 0.050 mm 0.020 mm 12.0% 5.3% 0.005 mm Clays 2.6%  $0.002\ mm$ Colloids 1.4%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Loamy Sand All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1704
Sample Date:	7/14/2021
Test Date:	9/17/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT18-GB-16.5-21.4 ft

 Visual Soil Description:
 brown silty sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

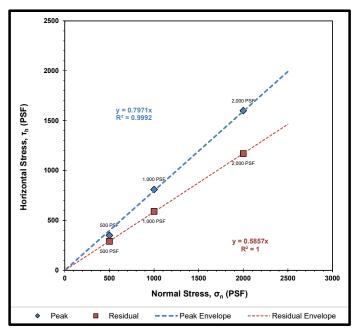
 Specimen Diameter (in):
 2.5

Summary of Sampl	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	29.4	
	Initial	Post-Consolidation
Dry Density (PCF):	107.0	107.9
Void Ratio:	0.575	0.562
Porosity (%):	36.5	36.0
Degree of Saturation (%):	saturated	saturated

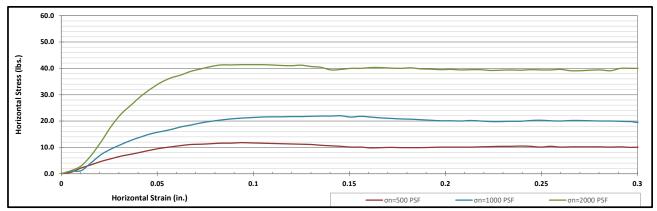
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	28.3	
	Initial	Post-Consolidation
Dry Density (PCF):	107.4	109.9
Void Ratio:	0.569	0.533
Porosity (%):	36.3	34.8
Degree of Saturation (%):	saturated	saturated

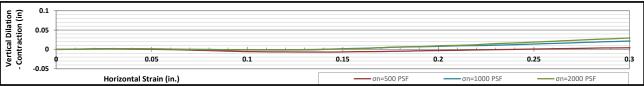
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	29.0	
	Initial	Post-Consolidation
Dry Density (PCF):	106.9	110.5
Void Ratio:	0.576	0.525
Porosity (%):	36.5	34.4
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRI	ENGTH PARA	METERS
	PEAK	RESIDUAL
Angle of Internal Friction, φ (°):	39	30
Cohesion (PSF):	0	0



Failure Envelope Test	Values:		
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	350	810	1600
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	590	1170





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT18-GB-21.4-26.5 ft

Sample#: B21-1705

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 13-Sep-21

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

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0.0%

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#8

#10 #16

#20

#30

#40

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

99%

94%

29.7%

Sample Meets Specs? N/A

 $D_{(5)} = 0.013$   $D_{(10)} = 0.025$ % Gravel = 0.7% % Sand = 69.6% mm  $D_{(15)} = 0.038$ % Silt & Clay = 29.7% mm  $D_{(30)} = 0.076$ Liquid Limit = n/a mm  $D_{(50)} = 0.128$ mm Plasticity Index = n/a  $D_{(60)} = 0.162$ mm Sand Equivalent = n/a  $D_{(90)} = 0.393$ mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.41$ Coeff. of Uniformity,  $C_U = 6.40$ Fineness Modulus = 0.74 Plastic Limit = n/a

Moisture %, as sampled = 38.4% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

D(90) 0.575						
st Ratio = 23/73		1.0				
M D6913, ASTM	IM C136, ASI	AS	T . 1 . 1			
			Interpolated	Actual		
			Cumulative			
	Specs	Specs	Percent	Percent		Sieve
1	Min	Max	Passing	Passing	Metric	US
	0.0%	100.0%	100%		300.00	12.00"
	0.0%	100.0%	100%		250.00	10.00"
	0.0%	100.0%	100%		200.00	8.00"
	0.0%	100.0%	100%		150.00	6.00"
	0.0%	100.0%	100%		100.00	4.00"
	0.0%	100.0%	100%		75.00	3.00"
	0.0%	100.0%	100%		63.00	2.50"
	0.0%	100.0%	100%	100%	50.00	2.00"
	0.0%	100.0%	100%		45.00	1.75"
	0.0%	100.0%	100%		37.50	1.50"
	0.0%	100.0%	100%		31.50	1.25"
p p	0.0%	100.0%	100%	100%	25.00	1.00"
% Possing	0.0%	100.0%	100%	100%	19.00	3/4"
96	0.0%	100.0%	100%		16.00	5/8"
	0.0%	100.0%	100%	100%	12.50	1/2"
	0.0%	100.0%	100%	100%	9.50	3/8"
	0.0%	100.0%	100%		6.30	1/4"

99%

99%

99%

96%

95%

95%

94%

78%

71%

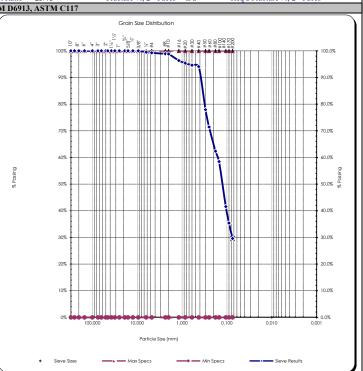
62%

58%

42%

35%

29.7%



Reviewed by: Meghan Blodgett-Carrillo



Client:	Anchor QEA	Date:	October 6, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1787-1803
Revised on:		Date sampled:	7-12-21 & 7-14-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 20, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1787	LDW21-GT15-GB-0-7.5 ft	233.4	1016.2	787.2	229.0	553.8	41.4%
B21-1788	LDW21-GT15-GB-7.5-9 ft	306.7	450.8	422.5	28.3	115.8	24.4%
B21-1789	LDW21-GT15-GB-7.5-15 ft	236.2	1288.2	1043.0	245.2	806.8	30.4%
B21-1790	LDW21-GT15-GB-15-17.5 ft	303.3	997.2	810.9	186.3	507.6	36.7%
B21-1791	LDW21-GT15-GB-17.5-19 ft	311.1	465.1	434.0	31.1	122.9	25.3%
B21-1792	LDW21-GT15-GB-17.5-25.4 ft	270.2	882.6	747.4	135.2	477.2	28.3%
B21-1793	LDW21-GT15-GB-25.4-27.5 ft	260.6	1270.0	1036.1	233.9	775.5	30.2%
B21-1794	LDW21-GT15-GB-27.5-29 ft	222.9	616.1	520.8	95.3	297.9	32.0%
B21-1795	LDW21-GT29-GB-0-1.5 ft	225.1	949.8	644.5	305.3	419.4	72.8%
B21-1796	LDW21-GT29-GB-0-10.6 ft	221.7	746.6	548.6	198.0	326.9	60.6%
B21-1797	LDW21-GT29-GB-11-12.5 ft	221.4	1082.5	801.0	281.5	579.6	48.6%
B21-1798	LDW21-GT29-GB-11-21 ft	224.4	738.0	646.6	91.4	422.2	21.6%
B21-1799	LDW21-GT29-GB-21-22.5 ft	222.3	408.6	349.3	59.3	127.0	46.7%
B21-1800	LDW21-GT29-GB-21-26 ft	233.8	1031.7	903.6	128.1	669.8	19.1%
B21-1801	LDW21-GT29-GB-26-28.9 ft	229.1	776.5	629.0	147.5	399.9	36.9%
B21-1802	LDW21-GT29-GB-28.9-31 ft	188.4	1285.9	988.6	297.3	800.2	37.2%
B21-1803	LDW21-GT29-GB-31-32.5 ft	225.3	925.7	756.5	169.2	531.2	31.9%
<del></del>							

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 20, 2021	Tested by: A. Eifrig

		Ī							Mass of Pycno filled	Mass of	Tamm of		Temp.	1
			Dry Soil +	Mass of Dry		Mass of	Volume of	Density of	w/ water &					Corrected
Sample #	Location	Tare	Tare	Soil	Pycno ID	Pycno	Pycno	Water @ Tx		w/ water	*C	Soils	Factor	SpG
B21-1787	LDW21-GT15-GB-0-7.5 ft	584.26	658.50	74.2	TSA-014	192.3	499.5	0.99749	735.04	690.54	23.2	2.4966051		2.4948325
B21-1792	LDW21-GT15-GB-17.5-25.4 ft	493.62	594.11	100.5	TSA-016	197.2	499.5	0.99754	757.82	695.45		2.6360571		2.634291
B21-1793	LDW21-GT15-GB-25.4-27.5 ft	500.82	575.98	75.2	TSA-022	198.0	499.5	0.99749	740.87	696.19		2.4661721		2.4644211
B21-1796	LDW21-GT29-GB-0-10.6 ft	600.79	675.86	75.1	TSA-012	180.4	499.5	0.99752	722.04	678.65	23.1	2.3695318	0.99931	2.3678968
B21-1798	LDW21-GT29-GB-11-21 ft	584.33	685.35	101.0	TSA-017	187.9	499.4	0.99749	749.71	686.04	23.2	2.7049457	0.99929	2.7030252
		1		<del></del>				<b>-</b>	1		-		1	
		1						1	1					
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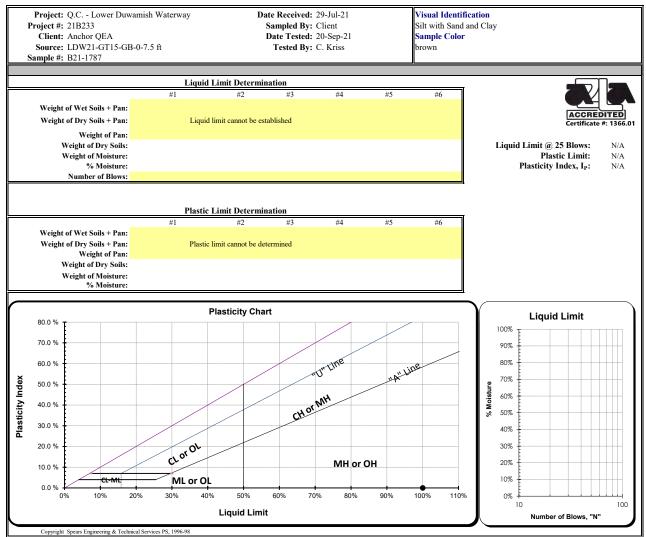
All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our

Comments: Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit cup without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT15-GB-7.5-15 ft Sample#: B21-1789

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



80 0%

70.0%

30.0%

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.076$   $D_{(10)} = 0.113$   $D_{(15)} = 0.150$   $D_{(30)} = 0.220$ % Gravel = 1.6% % Sand = 93.6% mm % Silt & Clay = 4.8% mm Liquid Limit = n/a mm  $D_{(50)} = 0.313$   $D_{(60)} = 0.359$   $D_{(90)} = 1.522$ mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 1.19$ Coeff. of Uniformity,  $C_U = 3.17$ Fineness Modulus = 1.81 Plastic Limit = n/a Moisture %, as sampled = 30.4%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						2(90) 1.52					
						oust Ratio = 2/		Frac	ture %, 2+ F	aces = n/a	
			1	AS	STM C136, AS	TM D6913, AS	FM C117				
		Actual	Interpolated					(	Grain Size Distrib	ution	
			Cumulative					Ę.,	_		
Sieve		Percent	Percent	Specs	Specs		9	4 % 2 % T	5/8′′′′ 3/8′′′′′′′′′′′′′′′′′′′′′′′′′′′′′′	<sup>85</sup> 5 5 8 8 8 8 8 8 8	8848
US	Metric	Passing	Passing	Max	Min	4			4	4 4 4 4 4 4	
12.00"	300.00		100%	100.0%	0.0%		<b> </b>			" <b>\</b>	
10.00"	250.00		100%	100.0%	0.0%		90%			<b>\</b>	
8.00"	200.00		100%	100.0%	0.0%		90%				
6.00"	150.00		100%	100.0%	0.0%		1 1			\ \ \	
4.00"	100.00		100%	100.0%	0.0%		80%			<u>\</u>	1
3.00"	75.00		100%	100.0%	0.0%		<u> </u>				
2.50"	63.00		100%	100.0%	0.0%		ł I				
2.00"	50.00	100%	100%	100.0%	0.0%		70%				╁═╌╫
1.75"	45.00		100%	100.0%	0.0%		FI				
1.50"	37.50		100%	100.0%	0.0%		11				
1.25"	31.50		100%	100.0%	0.0%		60%				111
1.00"	25.00	100%	100%	100.0%	0.0%	D	<u> </u>				
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				
5/8"	16.00		99%	100.0%	0.0%	96	55%				
1/2"	12.50	99%	99%	100.0%	0.0%		F				
3/8"	9.50	99%	99%	100.0%	0.0%		40%				
1/4"	6.30		99%	100.0%	0.0%		<b>!</b>			<b>}</b>	
#4	4.75	98%	98%	100.0%	0.0%		ļ			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
#8	2.36		97%	100.0%	0.0%		30%				
#10	2.00	97%	97%	100.0%	0.0%		ł I				1
#16	1.18		85%	100.0%	0.0%		20%				<b>\</b>
#20	0.850		80%	100.0%	0.0%		20% F				
#30	0.600		77%	100.0%	0.0%		F				
#40	0.425	74%	74%	100.0%	0.0%		10%				$\perp \downarrow \parallel$
#50	0.300		47%	100.0%	0.0%						1
#60	0.250		37%	100.0%	0.0%		<u> </u>				
#80	0.180		21%	100.0%	0.0%		0%	00.000	10.000	- <del>00 -0101010 00</del>	0.100
#100	0.150	15%	15%	100.0%	0.0%			00.000	10.000	1.000	0.100
#140	0.106		9%	100.0%	0.0%				Particle Siz	:e (mm)	

100.0%

100.0%

0.0%

0.0%

#170

#200

Reviewed by:

Meghan Blodgett-Carrillo

4.8%

7%

4.8%

0.090

0.075

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1789
Sample Date:	7/12/2021
Test Date:	9/28/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT15-GB-7.5-15 ft

 Visual Soil Description:
 brown sand with silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

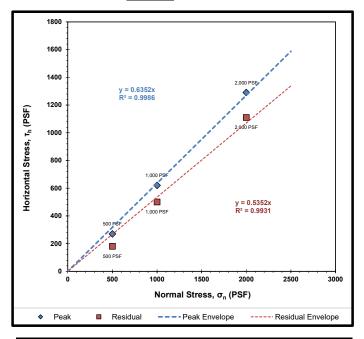
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	26.1	
	Initial	Post-Consolidation
Dry Density (PCF):	109.2	110.2
Void Ratio:	0.543	0.528
Porosity (%):	35.2	34.6
Degree of Saturation (%):	saturated	saturated

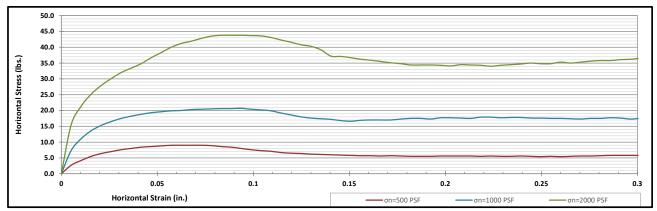
Summary of Samp	le Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	25.9	
	Initial	Post-Consolidation
Dry Density (PCF):	108.7	110.2
Void Ratio:	0.550	0.529
Porosity (%):	35.5	34.6
Degree of Saturation (%):	saturated	saturated

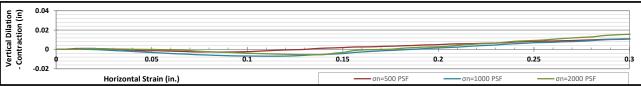
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	25.9	
	Initial	Post-Consolidation
Dry Density (PCF):	110.0	114.4
Void Ratio:	0.532	0.473
Porosity (%):	34.7	32.1
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS						
	PEAK	RESIDUAL				
Angle of Internal Friction, φ (°):	32	28				
Cohesion (PSF):	0	0				



Failure Envelope Test Values:					
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000		
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	270	620	1290		
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	180	500	1110		





Corporate • 777 Chrysler Drive • Burlington, WA 98233 • Phone 360.755.1990 • Fax 360.755.1980 SW Region • 2118 Black Lake Blvd. S.W.• Olympia, WA 98512 • Phone 360.534.9777 • Fax 360.534.9779 NW Region • 805 Dupont, Suite #5 • Bellingham, WA 98225 • Phone 360.647.6061 • Fax 360.647.8111 Kitsap Region • 5451 N.W. Newberry Hill Road, Suite 101 • Silverdale, WA 98383 • Phone/Fax 360.698.6787



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT15-GB-15-17.5 ft

Sample#: B21-1790

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21 Tested By: C. Kriss

Visual Identification Sandy Silt with Clay Sample Color: brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.004 \\ \textbf{D}_{(10)} = 0.006 \\ \textbf{D}_{(10)} = 0.012 \\ \textbf{D}_{(30)} = 0.039 \\ \textbf{D}_{(50)} = 0.067 \\ \textbf{D}_{(60)} = 0.082 \\ \textbf{D}_{(90)} = 0.193 \\ \textbf{Ratio} = 47/80 \end{array}$ mm mm mm mm mm mm

Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a

% Gravel = 1.3% % Sand = 41.6%

% Silt & Clay = 57.1%

Coeff. of Curvature,  $C_C = 2.92$ Coeff. of Uniformity,  $C_U = 12.63$ Fineness Modulus = 0.29

Plastic Limit = n/a Moisture %, as sampled = 36.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Req'd	Fracture	%,	2+	Faces	=

						Oust Ratio = 47/80 Fracture %, 2+ Faces = n/a Req'd Fracture %, 2+ Faces =
				AS	TM C136, AST	STM D6913, ASTM C117
			Interpolated			Grain Size Distribution
		,	Cumulative			
Sieve	Size	Percent	Percent	Specs	Specs	7
US	Metric	Passing	Passing	Max	Min	
12.00"	300.00		100%	100.0%	0.0%	
10.00"	250.00		100%	100.0%	0.0%	
8.00"	200.00		100%	100.0%	0.0%	90%
6.00"	150.00		100%	100.0%	0.0%	<u> </u>
4.00"	100.00		100%	100.0%	0.0%	80%
3.00"	75.00		100%	100.0%	0.0%	0.0.0
2.50"	63.00		100%	100.0%	0.0%	<u> </u>
2.00"	50.00	100%	100%	100.0%	0.0%	70.5
1.75"	45.00		100%	100.0%	0.0%	1
1.50"	37.50		100%	100.0%	0.0%	
1.25"	31.50		100%	100.0%	0.0%	60%
1.00"	25.00	100%	100%	100.0%	0.0%	ge
3/4"	19.00	99%	99%	100.0%	0.0%	0.5 50.5 44 50%
5/8"	16.00		99%	100.0%	0.0%	96 20% B6
1/2"	12.50	99%	99%	100.0%	0.0%	
3/8"	9.50	99%	99%	100.0%	0.0%	40.0%
1/4"	6.30		99%	100.0%	0.0%	
#4	4.75	99%	99%	100.0%	0.0%	<u> </u>
#8	2.36		98%	100.0%	0.0%	30%
#10	2.00	98%	98%	100.0%	0.0%	<b>I</b>
#16	1.18		97%	100.0%	0.0%	20.0%
#20	0.850		97%	100.0%	0.0%	20%
#30	0.600		97%	100.0%	0.0%	
#40	0.425	97%	97%	100.0%	0.0%	10%
#50	0.300		93%	100.0%	0.0%	
#60	0.250		92%	100.0%	0.0%	
#80	0.180		90%	100.0%	0.0%	0% 000 0 000 000 000 000 000 000 000
#100	0.150	89%	89%	100.0%	0.0%	100,000 10,000 1,000 0,100 0,010 0,001
#140	0.106	03.0	70%	100.0%	0.0%	Particle Size (mm)
#170	0.090		63%	100.0%	0.0%	
#200	0.075	57.1%	57.1%	100.0%	0.0%	+ Sieve Sizes → Max Specs → Min Specs → Sieve Results
	Spears Engineering & Tec	1	ļ	100.070	0.070	
11.0					1 20 1 0 01	dential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approve

Reviewed by:



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Sandy Silt with Clay Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 20-Sep-21 Sample Color Source: LDW21-GT15-GB-15-17.5 ft Tested By: C. Kriss brown Sample#: B21-1790 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 75.02 **Grain Size Distribution** 1.96% Soils Particle Hydroscopic Moist .: Sieve Percent ACCREDITED Adj. Sample Wgt: 73.58 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 31.500 mm Minutes Reading Passing 100% Diameter 0.0477 mm 33.8% 100% 25.000 mm 25.5 1.0" 27.8% 0.0347 mm 3/4" 19.000 mm 2 21 99% 17 22.5%  $0.0224\ mm$ 5/8" 99% 16.000 mm 15 15.9% 0.0133 mm 1/2" 99% 12.500 mm 30 10 13.3% 0.0096 mm 3/8" 99% 9.500 mm 60 10.6% 0.0068 mm 1/4" 99% 6.300 mm 240 4.6% 0.0035 mm 99% 4.750 mm 3.5 #4 2.7% #10 98%  $2.000\ mm$ 1440  $0.0014\ mm$ #20 97%  $0.850 \ mm$ Liquid Limit: n/a % Gravel: 1.3% #40 97% 0.425 mm % Sand: 41.6% Plastic Limit: n/a #100 89% 0.150 mm % Silt: 49.7% Plasticity Index: n/a #200 57.1%  $0.075 \ mm$ 56.2% 0.074 mm % Clay: 7.3% Silts 42.6% 0.050 mm 0.020 mm 20.8% 7.3% 0.005 mm Clays 3.2%  $0.002\ mm$ Colloids 1.8%  $0.001\ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

<b>Comments:</b>			
	Mayh Bargot and b		
Reviewed by:	Meghan Blodgett-Carrillo		



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#20

#30

#40 #50

#60

#80 #100

#140

#170

#200

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

68%

15.5%

Source: LDW21-GT15-GB-17.5-19 ft Sample#: B21-1791

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21 Tested By: C. Kriss

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.007$   $D_{(10)} = 0.056$   $D_{(15)} = 0.073$ % Gravel = 2.2% % Sand = 82.3% mm % Silt & Clay = 15.5% mm  $D_{(30)} = 0.142$ mm  $D_{(50)} = 0.287$ mm  $D_{(60)} = 0.362$ mm  $D_{(90)} = 1.662$ Oust Ratio = 22/97

mm

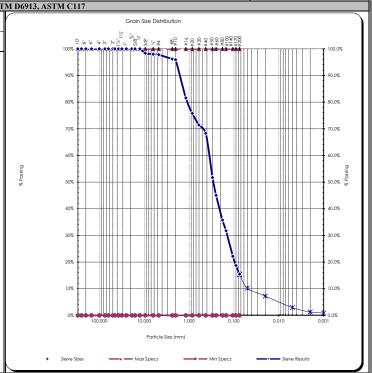
Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 0.98$ Coeff. of Uniformity,  $C_U = 6.42$ Fineness Modulus = 1.71 Plastic Limit = n/a

Moisture %, as sampled = 25.3% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				46	TM C126
		Actual Cumulative	Interpolated Cumulative	AS	TM C136,
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	98%	98%	100.0%	0.0%
1/4"	6.30		98%	100.0%	0.0%
#4	4.75	98%	98%	100.0%	0.0%
#8	2.36		96%	100.0%	0.0%
#10	2.00	96%	96%	100.0%	0.0%
#16	1.18		82%	100.0%	0.0%
		I			1



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0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

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32%

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15.5%

100.0%

100.0%

100.0%

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100.0%

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100.0%

100.0%



# **Hydrometer Report**

Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 Project: Q.C. - Lower Duwamish Waterway SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 20-Sep-21 Sample Color **Source:** LDW21-GT15-GB-17.5-19 ft Tested By: C. Kriss brown Sample#: B21-1791 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 74.97 **Grain Size Distribution** Hydroscopic Moist.: Soils Particle 1.06% Sieve Percent ACCREDITED Adj. Sample Wgt: 74.18 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Percent Soils Particle 1.5" 100% 37.500 mm Corrected 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0532 mm 100% 25.000 mm 9.1% 1.0" 3/4" 100% 19.000 mm 2 9.1% 0.0376 mm 5 6 7.8% 0.0239 mm 5/8" 100% 16.000 mm 15 6.5% 0.0139 mm 1/2" 100% 12.500 mm 30 4.5 5.8% 0.0098 mm 3/8" 98% 9.500 mm 60 5.2% 0.0070 mm 1/4" 98% 6.300 mm 240 1.3% 0.0035 mm 98% 4.750 mm #4 0.0014 mm 2.000 mm 1440 1.3% #10 96% #20 76%  $0.850\ mm$ Liquid Limit: n/a % Gravel: 2.2% #40 68% 0.425 mm % Sand: 82.3% Plastic Limit: n/a #100 32% 0.150 mm % Silt: 12.6% Plasticity Index: n/a #200 15.5% 0.075 mm 15.2% 0.074 mm % Clay: 3.0% Silts 10.2% 0.050 mm 0.020 mm 7.3% 3.0% 0.005 mm Clays 1.3%  $0.002\ mm$ Colloids 0.9%  $0.001\ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval. Comments:

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#100

#140

#170

#200

0.150

0.106

0.090

0.075

Source: LDW21-GT15-GB-17.5-25.4 ft Sample#: B21-1792

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: brown

7/34

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.023$   $D_{(10)} = 0.046$   $D_{(15)} = 0.069$ % Gravel = 8.2% % Sand = 75.4% mm % Silt & Clay = 16.4% mm  $D_{(30)} = 0.125$ Liquid Limit = n/a mm  $D_{(50)} = 0.234$ mm Plasticity Index = n/a  $D_{(60)} = 0.299$ mm Sand Equivalent = n/a  $D_{(90)} = 1.927$ mm

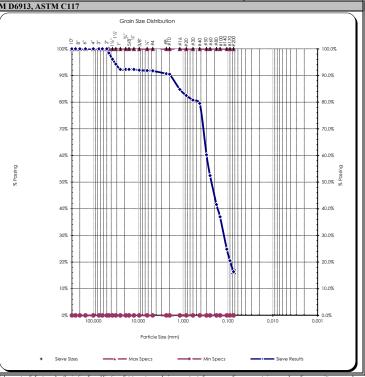
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.13$ Coeff. of Uniformity,  $C_U = 6.52$ Fineness Modulus = 1.71 Plastic Limit = n/a

Moisture %, as sampled = 28.3% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					_	D(90
				AC	TM C136, AS	ust Ratio
		Actual	Interpolated	AS	1 WI C130, AS	I MI DOS
		Cumulative	Cumulative			
Sieve	Size	Percent	Percent	Specs	Specs	1
US	Metric	Passing	Passing	Max	Min	
12.00"	300.00		100%	100.0%	0.0%	
10.00"	250.00		100%	100.0%	0.0%	
8.00"	200.00		100%	100.0%	0.0%	
6.00"	150.00		100%	100.0%	0.0%	
4.00"	100.00		100%	100.0%	0.0%	
3.00"	75.00		100%	100.0%	0.0%	
2.50"	63.00		100%	100.0%	0.0%	
2.00"	50.00	100%	100%	100.0%	0.0%	
1.75"	45.00		98%	100.0%	0.0%	
1.50"	37.50		96%	100.0%	0.0%	
1.25"	31.50		94%	100.0%	0.0%	
1.00"	25.00	92%	92%	100.0%	0.0%	2
3/4"	19.00	92%	92%	100.0%	0.0%	% Possing
5/8"	16.00		92%	100.0%	0.0%	96
1/2"	12.50	92%	92%	100.0%	0.0%	
3/8"	9.50	92%	92%	100.0%	0.0%	
1/4"	6.30		92%	100.0%	0.0%	
#4	4.75	92%	92%	100.0%	0.0%	
#8	2.36		91%	100.0%	0.0%	
#10	2.00	91%	91%	100.0%	0.0%	
#16	1.18		85%	100.0%	0.0%	
#20	0.850		83%	100.0%	0.0%	
#30	0.600		81%	100.0%	0.0%	
#40	0.425	80%	80%	100.0%	0.0%	
#50	0.300		60%	100.0%	0.0%	
#60	0.250		52%	100.0%	0.0%	
#80	0.180		42%	100.0%	0.0%	
	1		1			



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**Comments:** Reviewed by: Meghan Blodgett-Carrillo

37%

25%

20%

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100.0%

100.0%

100.0%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

Sample#: B21-1793

Source: LDW21-GT15-GB-25.4-27.5 ft

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21 Tested By: C. Kriss

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.006$   $D_{(10)} = 0.010$   $D_{(15)} = 0.022$ mm mm  $D_{(30)} = 0.066$ mm  $D_{(50)} = 0.104$ mm  $D_{(60)} = 0.125$ 

 $D_{(90)} = 0.331$ 

Dust Ratio = 29/79

Liquid Limit = n/a Plasticity Index = n/a mm Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

% Gravel = 0.0%

% Silt & Clay = 36.4%

% Sand = 63.6%

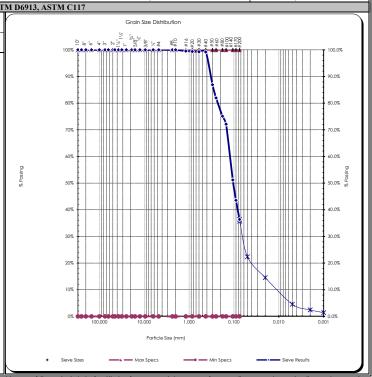
Coeff. of Curvature,  $C_C = 3.56$ Coeff. of Uniformity,  $C_U = 12.70$ Fineness Modulus = 0.42 Plastic Limit = n/a

Moisture %, as sampled = 30.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	IM C130, AS1
		Actual Cumulativ	Interpolated ve Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
2.00"	300.00		100%	100.0%	0.0%
0.00"	250.00		100%	100.0%	0.0%
.00"	200.00		100%	100.0%	0.0%
.00"	150.00		100%	100.0%	0.0%
.00"	100.00		100%	100.0%	0.0%
.00"	75.00		100%	100.0%	0.0%
.50"	63.00		100%	100.0%	0.0%
.00"	50.00	100%	100%	100.0%	0.0%
.75"	45.00		100%	100.0%	0.0%
.50"	37.50		100%	100.0%	0.0%
.25"	31.50		100%	100.0%	0.0%

	Cumulative Cumulative								
Sieve	Size	Percent	Percent	Specs	Specs				
US	Metric	Passing	Passing	Max	Min				
12.00"	300.00		100%	100.0%	0.0%				
10.00"	250.00		100%	100.0%	0.0%				
8.00"	200.00		100%	100.0%	0.0%				
6.00"	150.00		100%	100.0%	0.0%				
4.00"	100.00		100%	100.0%	0.0%				
3.00"	75.00		100%	100.0%	0.0%				
2.50"	63.00		100%	100.0%	0.0%				
2.00"	50.00	100%	100%	100.0%	0.0%				
1.75"	45.00		100%	100.0%	0.0%				
1.50"	37.50		100%	100.0%	0.0%				
1.25"	31.50		100%	100.0%	0.0%				
1.00"	25.00	100%	100%	100.0%	0.0%				
3/4"	19.00	100%	100%	100.0%	0.0%				
5/8"	16.00		100%	100.0%	0.0%				
1/2"	12.50	100%	100%	100.0%	0.0%				
3/8"	9.50	100%	100%	100.0%	0.0%				
1/4"	6.30		100%	100.0%	0.0%				
#4	4.75	100%	100%	100.0%	0.0%				
#8	2.36		100%	100.0%	0.0%				
#10	2.00	100%	100%	100.0%	0.0%				
#16	1.18		100%	100.0%	0.0%				
#20	0.850		99%	100.0%	0.0%				
#30	0.600		99%	100.0%	0.0%				
#40	0.425	99%	99%	100.0%	0.0%				
#50	0.300		87%	100.0%	0.0%				
#60	0.250		82%	100.0%	0.0%				
#80	0.180		75%	100.0%	0.0%				
#100	0.150	72%	72%	100.0%	0.0%				
		1	1		1				



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**Comments:** Reviewed by: Meghan Blodgett-Carrillo

36.4%

51%

44%

36.4%

100.0%

100.0%

100.0%



# **Hydrometer Report**

Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 Project: Q.C. - Lower Duwamish Waterway SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 20-Sep-21 Sample Color Source: LDW21-GT15-GB-25.4-27.5 ft Tested By: C. Kriss brown Sample#: B21-1793 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.46 Sieve Analysis Sample Weight: 76.16 **Grain Size Distribution** Hydroscopic Moist.: 4.72% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 72.73 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Percent Soils Particle 1.5" 100% 37.500 mm Corrected 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0541 mm 21.7% 100% 25.000 mm 15 1.0" 19.5% 0.0388 mm 3/4" 100% 19.000 mm 2 13.5 5 11 15.9% 0.0248 mm 5/8" 100% 16.000 mm 15 9 13.0% 0.0145 mm 1/2" 100% 12.500 mm 30 7.5 10.8% 0.0104 mm 3/8" 100% 9.500 mm 0.0074 mm 60 4.5 6.5% 1/4" 100% 6.300 mm 240 3.6% 0.0038 mm 100% 4.750 mm 2.5 #4 100% 2.000 mm 1440 2.2% 0.0015 mm #10 #20 99%  $0.850\ mm$ Liquid Limit: n/a % Gravel: 0.0% #40 99% 0.425 mm % Sand: 63.6% Plastic Limit: n/a #100 72% 0.150 mm % Silt: 31.8% Plasticity Index: n/a #200 36.4% 0.075 mm 35.7% 0.074 mm % Clay: 4.6% Silts 22.4% 0.050 mm 0.020 mm 14.5% 4.6% 0.005 mm Clays 2.5%  $0.002\ mm$ Colloids 1.4%  $0.001\ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Loamy Sand All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval Comments:

Environmental • Geotechnical Engineering • Special Inspection • Non-Destructive Testing • Materials Testing

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360.755.1990

www.mtc-inc.net

Reviewed by:

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C Lower Duwamish Waterway Project #: 21B233 Client: Anchor QEA Source: LDW21-GT29-0-10.6 ft Sample #: B21-1796				ate Received: Sampled By: Date Tested: Tested By:	Client 21-Sep-21		Visual Identific Silt Sample Color brown	cation
		Liqui	d Limit Determ	ination				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	32.74	33.79	36.07				
	Weight of Dry Soils + Pan:	28.61	29.18	30.52				
	Weight of Pan:	19.91	19.73	19.61				
	Weight of Dry Soils:	8.70	9.45	10.91				Liquid Limit @ 25 Blows: 47 %
	Weight of Moisture:	4.13	4.61	5.55				Plastic Limit: N/A
	% Moisture:	47.5 %	48.8 %	50.9 %				Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:	25	16	11				
	Plastic Limit Determination #1 #2 #3 #4 #5 #6							
	Weight of Wet Soils + Pan:		2	5				
	Weight of Dry Soils + Pan:	Plastic	limit cannot be de	termined				
	Weight of Pan:							
	Weight of Dry Soils:							ACCREDITED
	Weight of Moisture: % Moisture:							Certificate #: 1366.01, 1366.02 & 1366.04
_	70 111013141101							
	70.0/		Plasticity Cha	art				Liquid Limit
	70 %							60% T
	60 %			_/	ine			
				, we	Line	عمند		50%
	50 %				or OH			
ě	40 %			CH	or o			₽ 40% -
Ě	40 %			<u> </u>				ist
Plasticity Index	30 %	/						40%
sti			.					°
뮵	20 %	1, or 0,		R 4				20%
	10 %	CL or OL		IVI	H or OH			
	CL-ML	ML or C						10%
	0%		-			_		
	0% 10% 20%	30% 40	% 50%	60% 70	% 80%	90%	100% 110%	0% 10 100
			Liquid Lim	it				Number of Blows, "N"
	Copyright Spears Engineering & Technica							

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding

Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

 $Corporate \sim 777\ Chrysler\ Drive \quad \bullet \quad Burlington,\ WA\ 98233 \quad \bullet \quad Phone\ (360)\ 755-1990 \quad \bullet \quad Fax\ (360)\ 755-1980$ 

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Visit our website: www.mtc-inc.net



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT29-GB-11-21 ft

Sample#: B21-1798

#170

#200

0.090

0.075

2.0%

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 20-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.156 \\ \textbf{D}_{(10)} = 0.197 \\ \textbf{D}_{(15)} = 0.237 \\ \textbf{D}_{(30)} = 0.358 \\ \textbf{D}_{(50)} = 0.737 \\ \textbf{D}_{(60)} = 1.003 \\ \textbf{D}_{(90)} = 1.801 \\ \end{array}$ % Gravel = 0.5% % Sand = 97.4% mm % Silt & Clay = 2.0% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 0.65$ Coeff. of Uniformity,  $C_U = 5.10$ Fineness Modulus = 2.64 Plastic Limit = n/a

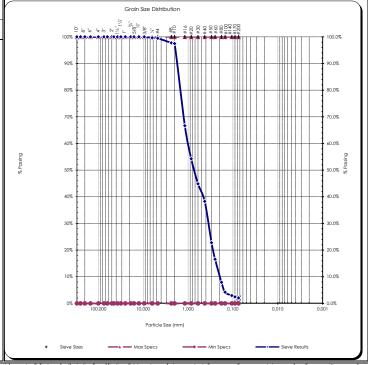
Moisture %, as sampled = 21.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 1.801$	mm		Fracture			
						Oust Ratio = 3/56		Fra	acture %	, 2+ I	Faces	= n
				AS	STM C136, AS	TM D6913, ASTM	I C117					
		Actual	Interpolated						Grain Size	e Distrik	bution	
		7	Cumulative					E.				
Sieve		Percent	Percent	Specs	Specs		io io :	. <u>7</u> . 4 4 ¢ . 7. 4 4 ¢	. %%	7.4	eo_0 ##	8 =
US 12.00"	Metric	Passing	Passing 100%	Max	Min	4	100%	<u> • • • • • • • • • • • • • • • • • • </u>		***	-	4
	300.00			100.0%	0.0%		ł I				ľ	
10.00"	250.00		100%	100.0%	0.0%		90%				1	
8.00"	200.00		100%	100.0%	0.0%		70%			Ш		Ш
6.00"	150.00		100%	100.0%	0.0%							
4.00"	100.00	1	100%	100.0%	0.0%		80%		$\sqcup \sqcup \sqcup$	₩	++	-111
3.00"	75.00		100%	100.0%	0.0%							
2.50"	63.00		100%	100.0%	0.0%		1					
2.00"	50.00	100%	100%	100.0%	0.0%		70%			HH	++-	ш
1.75"	45.00		100%	100.0%	0.0%		- [ ]					ì
1.50"	37.50		100%	100.0%	0.0%							1
1.25"	31.50		100%	100.0%	0.0%		60%			m	+	1
1.00"	25.00	100%	100%	100.0%	0.0%	oug Oug						Ì
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%			ШШ		\
5/8"	16.00		100%	100.0%	0.0%	84						- 1)
1/2"	12.50	100%	100%	100.0%	0.0%		- [ ]					
3/8"	9.50	100%	100%	100.0%	0.0%		40%		$\mathbb{H} = \mathbb{H}$	₩	++-	-##
1/4"	6.30		100%	100.0%	0.0%		- 11					
#4	4.75	99%	99%	100.0%	0.0%							
#8	2.36		98%	100.0%	0.0%		30%			###	++-	-#
#10	2.00	97%	97%	100.0%	0.0%		ł I					
#16	1.18		67%	100.0%	0.0%		20%					
#20	0.850		54%	100.0%	0.0%		<sup>2070</sup> F T			Ш	П	T
#30	0.600		45%	100.0%	0.0%							
#40	0.425	38%	38%	100.0%	0.0%		10%	-	$\square$	₩	₩	-11
#50	0.300		23%	100.0%	0.0%							
#60	0.250		17%	100.0%	0.0%							
#80	0.180		8%	100.0%	0.0%		0%	100.000	10.000	4	400-	1.000
#100	0.150	4%	4%	100.0%	0.0%			100.000	10.000			1.000
#140	0.106	1	3%	100.0%	0.0%				P	article S	Size (mm)	)
		1	1 227			ll .						

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100.0%



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0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

2%

2.0%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT29-GB-21-26 ft

Sample#: B21-1800

#16

#20

#30

#40

#50

#60

#80

#100

#140

#170

#200

**Comments:** 

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21

Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand Sample Color:

gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.153$   $D_{(10)} = 0.185$   $D_{(15)} = 0.218$ % Gravel = 4.9% % Sand = 93.3% mm % Silt & Clay = 1.8% mm  $D_{(30)} = 0.314$ Liquid Limit = n/a mm  $D_{(50)} = 0.527$ mm Plasticity Index = n/a  $D_{(60)} = 0.883$ mm Sand Equivalent = n/a  $D_{(90)} = 1.952$ Oust Ratio = 3/80 mm

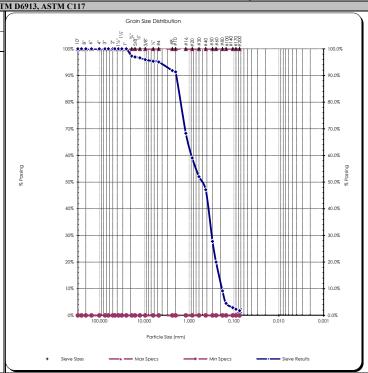
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 0.60$ Coeff. of Uniformity,  $C_U = 4.77$ Fineness Modulus = 2.67 Plastic Limit = n/a

Moisture %, as sampled = 18.8% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					D
		Actual Cumulative	Interpolated Cumulative	AS	STM C136, AS
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	97%	97%	100.0%	0.0%
5/8"	16.00		97%	100.0%	0.0%
1/2"	12.50	97%	97%	100.0%	0.0%
3/8"	9.50	96%	96%	100.0%	0.0%
1/4"	6.30		95%	100.0%	0.0%
#4	4.75	95%	95%	100.0%	0.0%
#8	2.36		92%	100.0%	0.0%
#10	2.00	91%	91%	100.0%	0.0%



0.0%

0.0%

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0.0%

0.0%

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Reviewed by:

68%

59%

52%

47%

28%

20%

9%

5%

3%

2%

1.8%

47%

1.8%

100.0%

100.0%

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100.0%

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#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1800
Sample Date:	7/14/2021
Test Date:	9/29/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT29-GB-21-26 ft

 Visual Soil Description:
 gray sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

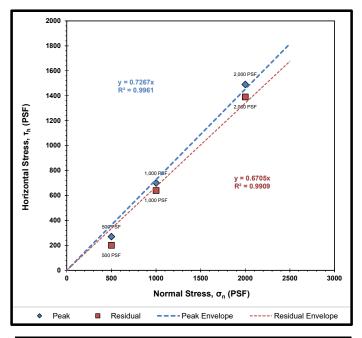
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%):	23.0	
	Initial	Post-Consolidation
Dry Density (PCF):	107.5	108.1
Void Ratio:	0.567	0.558
Porosity (%):	36.2	35.8
Degree of Saturation (%):	saturated	saturated

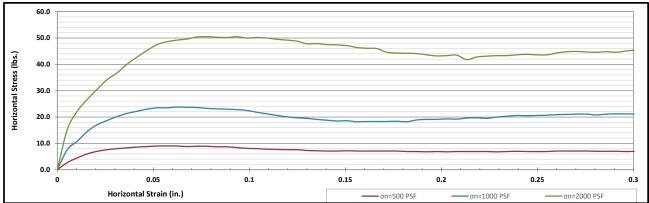
Summary of Sample	σ <sub>n</sub> =1000 PSF	
Initial Moisture Content (%):	22.3	
	Initial	Post-Consolidation
Dry Density (PCF):	107.1	108.5
Void Ratio:	0.572	0.552
Porosity (%):	36.4	35.6
Degree of Saturation (%):	saturated	saturated

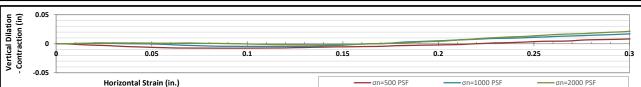
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	21.8	
	Initial	Post-Consolidation
Dry Density (PCF):	108.8	110.9
Void Ratio:	0.548	0.519
Porosity (%):	35.4	34.2
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS			
	PEAK	RESIDUAL	
Angle of Internal Friction, φ (°):	36	34	
Cohesion (PSF):	0	0	



Failure Envelope Test Values:					
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000		
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	270	700	1490		
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	200	640	1390		





Corporate • 777 Chrysler Drive • Burlington, WA 98233 • Phone 360.755.1990 • Fax 360.755.1980 SW Region • 2118 Black Lake Blvd. S.W.• Olympia, WA 98512 • Phone 360.534.9777 • Fax 360.534.9779 NW Region • 805 Dupont, Suite #5 • Bellingham, WA 98225 • Phone 360.647.6061 • Fax 360.647.8111 Kitsap Region • 5451 N.W. Newberry Hill Road, Suite 101 • Silverdale, WA 98383 • Phone/Fax 360.698.6787



Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

**Source:** LDW21-GT29-GB-26-28.9 ft **Sample#:** B21-1801

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

Tested By: C. Kriss

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#50

#60

#80

#140

#170

#200

**Comments:** 

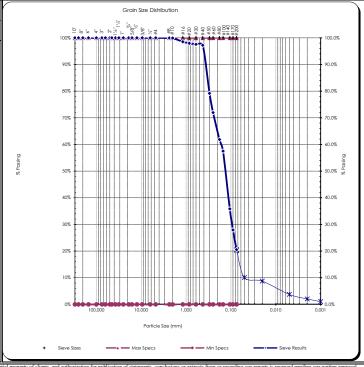
Sample Meets Specs ? N/A

 $D_{(5)} = 0.008$   $D_{(10)} = 0.040$   $D_{(15)} = 0.061$ % Gravel = 0.0%% Sand = 79.4% mm % Silt & Clay = 20.6% mm  $D_{(30)} = 0.094$ Liquid Limit = n/a mm  $D_{(50)} = 0.135$ mm Plasticity Index = n/a  $D_{(60)} = 0.167$ mm Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a  $D_{(90)} = 0.375$ mm

Coeff. of Curvature,  $C_C = 1.33$ Coeff. of Uniformity,  $C_U = 4.18$ Fineness Modulus = 0.67 Plastic Limit = n/a Moisture %, as sampled = 36.9%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						$D_{(90)} - 0$ .	
				4.6		ust Ratio = 1	
			Interpolated	AS	TM C136, AS	1 M D6913, A	SIM CII7
Sieve	Siza	Cumulative Percent	Percent	Specs	Specs	-	
US	Metric	Passing	Passing	Max	Min		io i ⊆ ••••• 2001
12.00"	300.00	1 4551115	100%	100.0%	0.0%	1	100%
0.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		90%
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		80%
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		70%
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		ł I
.25"	31.50		100%	100.0%	0.0%		60%
.00"	25.00	100%	100%	100.0%	0.0%	9	1
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%
5/8"	16.00		100%	100.0%	0.0%	₽€	30%
1/2"	12.50	100%	100%	100.0%	0.0%		[ ]
3/8"	9.50	100%	100%	100.0%	0.0%		40%
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		100%	100.0%	0.0%		30%
#10	2.00	100%	100%	100.0%	0.0%		<u> </u>
#16	1.18		99%	100.0%	0.0%		20%
#20	0.850		98%	100.0%	0.0%		-0% E T
#30	0.600		98%	100.0%	0.0%		F
#40	0.425	97%	97%	100.0%	0.0%		10%



Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval

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Reviewed by:

Meghan Blodgett-Carrillo

20.6%

79%

72%

62%

58%

36%

28%

20.6%



# **Hydrometer Report**

Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 Project: Q.C. - Lower Duwamish Waterway SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 20-Sep-21 Sample Color Source: LDW21-GT29-GB-26-28.9 ft Tested By: C. Kriss brown Sample#: B21-1801 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 100.10 **Grain Size Distribution** Hydroscopic Moist.: 1.34% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 98.78Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Percent Soils Particle 1.5" 100% 37.500 mm Corrected 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 11.6% 0.0520 mm 100% 25.000 mm 11.5 1.0" 3/4" 100% 19.000 mm 2 9.5 9.6% 0.0371 mm 5 9 9.1% 0.0235 mm 5/8" 100% 16.000 mm 15 8.1%0.0137 mm 1/2" 100% 12.500 mm 30 6.1% 0.0097 mm 3/8" 100% 9.500 mm 6 0.0070 mm 60 4.0% 1/4" 100% 6.300 mm 240 3.5% 0.0035 mm 100% 4.750 mm 3.5 #4 0.0014 mm 100% 2.000 mm 1440 1.5% #10 #20 98%  $0.850\ mm$ Liquid Limit: n/a 97% % Gravel: 0.0% #40 0.425 mm % Sand: 79.4% Plastic Limit: n/a #100 58% 0.150 mm % Silt: Plasticity Index: n/a #200 20.6% 0.075 mm 20.2% 0.074 mm % Clay: 3.8% Silts 10.1% 0.050 mm 0.020 mm 8.7% 3.8% 0.005 mm Clays 2.1%  $0.002\ mm$ Colloids 1.1%  $0.001\ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval. Comments:

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT29-GB-28.9-31 ft Sample#: B21-1802

0.250

0.180

0.150

0.106

0.090

0.075

#60

#80

#140

#170

#200

**Comments:** 

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 20-Sep-21 Tested By: C. Kriss

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

mm

brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

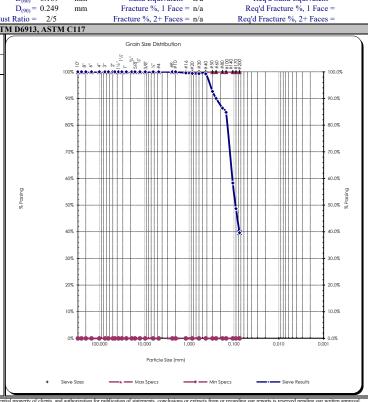
Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.009 \\ D_{(10)} = 0.019 \\ D_{(15)} = 0.028 \\ D_{(30)} = 0.057 \\ D_{(30)} = 0.003 \end{array}$ % Gravel = 0.0%% Sand = 60.4% mm % Silt & Clay = 39.6% mm Liquid Limit = n/a mm  $D_{(50)} = 0.092$ mm Plasticity Index = n/a  $D_{(60)} = 0.109$ mm Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.57$ Coeff. of Uniformity,  $C_U = 5.75$ Fineness Modulus = 0.24 Plastic Limit = n/a Moisture %, as sampled = 37.2%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

				4.0	TM C126
		Actual Cumulative	Interpolated Cumulative	AS	TM C136,
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		100%	100.0%	0.0%
#20	0.850		99%	100.0%	0.0%
#30	0.600		99%	100.0%	0.0%
#40	0.425	99%	99%	100.0%	0.0%
#50	0.300		93%	100.0%	0.0%



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Reviewed by: \_ Meghan Blodgett-Carrillo

85%

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90%

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85%

58%

49%

39.6%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%



Client:	Anchor QEA	Date:	October 14, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1812 - 1832
Revised on:		Date sampled:	July 15, 2021

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	<u> </u>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 23, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1812	LDW21-GT25-GB-0-1.5 ft	233.7	903.3	628.8	274.5	395.1	69.5%
B21-1813	LDW21-GT25-GB-0-8.5 ft	260.6	578.9	450.1	128.8	189.5	68.0%
B21-1814	LDW21-GT25-GB-8.5-10 ft	306.5	1244.3	1034.1	210.2	727.6	28.9%
B21-1815	LDW21-GT25-GB-8.5-16.2 ft	234.4	975.8	829.1	146.7	594.7	24.7%
B21-1816	LDW21-GT25-GB-16.2-18.5 ft	301.0	1029.3	834.6	194.7	533.6	36.5%
B21-1817	LDW21-GT25-GB-18.5-20 ft	311.0	1016.3	872.1	144.2	561.1	25.7%
B21-1818	LDW21-GT25-GB-18.5-24.4 ft	182.5	963.7	746.1	217.6	563.6	38.6%
B21-1819	LDW21-GT25-GB-24.4-26ft	268.9	846.8	702.0	144.8	433.1	33.4%
B21-1820	LDW21-GT25-GB-26-28.5 ft	229.0	653.6	545.0	108.6	316.0	34.4%
B21-1821	LDW21-GT25-GB-28.5-30 ft	221.8	847.9	689.3	158.6	467.5	33.9%
B21-1822	LDW21-GT33-GB-0-1.5 ft	223.1	962.3	671.6	290.7	448.5	64.8%
B21-1823	LDW21-GT33-GB-0-10.4 ft	225.2	643.8	515.2	128.6	290.0	44.3%
B21-1824	LDW21-GT33-GB-11-12.5 ft	221.3	1042.8	776.6	266.2	555.3	47.9%
B21-1825	LDW21-GT33-GB-11-18.5 ft	225.3	614.1	543.5	70.6	318.2	22.2%
B21-1826	LDW21-GT33-GB-18.3-21 ft	215.8	753.3	613.6	139.7	397.8	35.1%
B21-1827	LDW21-GT33-GB-21-22.5 ft	220.8	673.2	554.6	118.6	333.8	35.5%
B21-1828	LDW21-GT33-GB-21-26.8 ft	217.3	766.4	626.0	140.4	408.7	34.4%
B21-1829	LDW21-GT33-GB-26.8-28.8 ft	233.1	799.7	630.2	169.5	397.1	42.7%
B21-1830	LDW21-GT33-GB-28.8-29.5 ft	223.1	1026.1	824.1	202.0	601.0	33.6%
B21-1831	LDW21-GT33-GB-29.5-31 ft	221.8	989.1	767.9	221.2	546.1	40.5%
B21-1832	LDW21-GT33-GB-31-32.5 ft	208.9	577.5	479.9	97.6	271.0	36.0%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	<u> </u>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 20, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Tare	Mass of Dry Soil	Pycno ID		Volume of Pycno	Water @ Tx		Mass of Pycno filled w/ water	Water, 0.1 *C	SpG of Soils	Factor	SpG
B21-1813	LDW21-GT25-GB-0-8.5 ft	498.19	565.01	66.8	TSA-022	198.0	499.5	0.99759	737.17	696.24				2.5796852
B21-1820	LDW21-GT25-GB-26-28.5 ft	510.35	585.58	75.2	TSA-015	187.6	499.5	0.99780	732.43	686.00	21.9		0.99959	
B21-1825	LDW21-GT33-GB-11-18.5 ft	502.55	602.33	99.8	TSA-023	163.9	498.7	0.99786	723.74	661.59	21.6	2.6514178	0.99966	2.6505163
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Visual Identification Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Project #: 21B233 Sampled By: Client Silt with Clay Client: Anchor QEA, LLC Date Tested: 25-Sep-21 Sample Color Source: LDW21-GT25-GB-0-8.5 ft Tested By: K. Mendez orown Sample #: B21-1813 **Liquid Limit Determination** Weight of Wet Soils + Pan: 29 60 25.42 26.01 21.62 21.93 Weight of Dry Soils + Pan: 25.96 Weight of Pan: 19.65 15.20 15.00 Weight of Dry Soils: 6.31 6.42 6.93 Liquid Limit @ 25 Blows: Weight of Moisture: 3.64 3.80 4.08 Plastic Limit: 45 % % Moisture: 57.7 % 59.2 % 58.9 % Plasticity Index, I<sub>P</sub>: 13 % Number of Blows: **Plastic Limit Determination** Weight of Wet Soils + Pan: 35.15 34.29 Weight of Dry Soils + Pan: 33.00 32.39 28.27 28.20 Weight of Pan: Weight of Dry Soils: 4.73 4.19 Weight of Moisture: % Moisture: 45.4 % **Plasticity Chart Liquid Limit** 70% 60 % 60% CH or OH 50 % 50% Plasticity Index 40 % 40% 30 % CLorOL 30% 20 % MH or OH 20% 10 % 10% ML or OL CL-M 30% 60% 70% 80% 90% 100% 10 100 **Liquid Limit** Number of Blows, "N Copyright Spears Engineering & Technical Services PS, 1996-9

Comments:

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT25-GB-8.5-16.2 ft Sample#: B21-1815

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 25-Sep-21

Tested By: K. Mendez

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

mm

Sample Color:

brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

11%

1.9%

#40

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{ASTM D4S} \\ \textbf{D}_{(5)} = 0.216 \\ \textbf{D}_{(10)} = 0.395 \\ \textbf{D}_{(15)} = 0.501 \\ \textbf{D}_{(30)} = 0.773 \\ \textbf{D}_{(50)} = 1.137 \\ \textbf{D}_{(60)} = 1.318 \\ \textbf{D}_{(90)} = 1.864 \end{array}$ % Gravel = 1.1% % Sand = 97.0% mm % Silt & Clay = 1.9% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 1.15$ Coeff. of Uniformity,  $C_U = 3.34$ Fineness Modulus = 3.20 Plastic Limit = n/a

Moisture %, as sampled = 24.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 1$	1.804
						ust Ratio =	
		Actual Cumulative	Interpolated Cumulative	AS	STM C136, AS	FM D6913,	ASTM C
Sieve	Size	Percent	Percent	Specs	Specs	1	
US	Metric	Passing	Passing	Max	Min		1009
12.00"	300.00		100%	100.0%	0.0%	1	
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		909
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		809
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		709
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		609
1.00"	25.00	100%	100%	100.0%	0.0%	p <sub>0</sub>	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	
5/8"	16.00		100%	100.0%	0.0%	96	509
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		405
1/4"	6.30		99%	100.0%	0.0%		
#4	4.75	99%	99%	100.0%	0.0%		
#8	2.36		98%	100.0%	0.0%		309
#10	2.00	97%	97%	100.0%	0.0%		
#16	1.18		52%	100.0%	0.0%		209
#20	0.850		34%	100.0%	0.0%		20
#30	0.600		20%	100.0%	0.0%		

11%

7% 6%

4%

3%

2%

2%

1.9%

100.0%

100.0%

100.0%

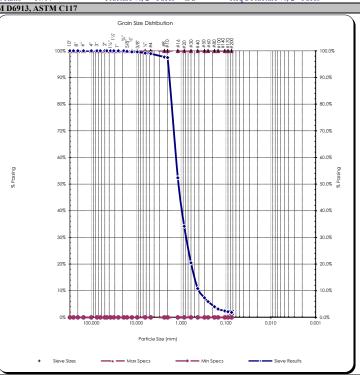
100.0%

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Reviewed by: \_ Meghan Blodgett-Carrillo

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1815
Sample Date:	7/15/2021
Test Date:	9/30/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT25-GB-8.5-16.2 ft

 Visual Soil Description:
 brown sand with silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

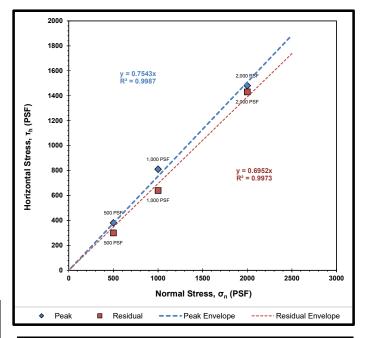
 Specimen Diameter (in):
 2.5

Summary of Sampl	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	25.1	
	Initial	Post-Consolidation
Dry Density (PCF):	108.7	109.7
Void Ratio:	0.550	0.536
Porosity (%):	35.5	34.9
Degree of Saturation (%):	saturated	saturated

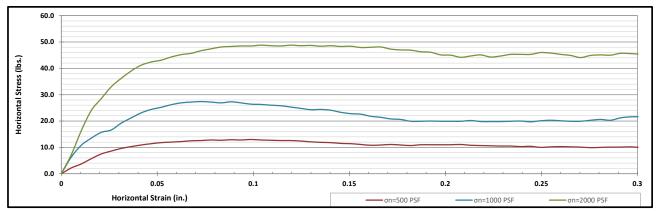
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF						
Initial Moisture Content (%):	24.7							
	Initial	Post-Consolidation						
Dry Density (PCF):	107.3	108.8						
Void Ratio:	0.571	0.549						
Porosity (%):	36.3	35.4						
Degree of Saturation (%):	saturated	saturated						

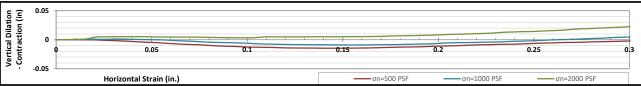
Summary of Sampl	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	25.6	
	Initial	Post-Consolidation
Dry Density (PCF):	107.7	110.3
Void Ratio:	0.564	0.527
Porosity (%):	36.0	34.5
Degree of Saturation (%):	saturated	saturated

ESTIMATED STR	ENGTH PARA	METERS
	PEAK	RESIDUAL
Angle of Internal Friction, φ (°):	37	35
Cohesion (PSF):	0	0



Failure Envelope Test	Values:		
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	380	810	1480
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	300	640	1430





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#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duw roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT25-Gl ample #: B21-1816	C .	5	te Received: Sampled By: Date Tested: Tested By:	Client 25-Sep-21		Visual Identific Sand Sample Color grayish-brown	ation
		Liquid Lir	nit Determina	tion				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan:	Unable	to esablish liqui	d limit				
	Weight of Pan: Weight of Dry Soils:							Liquid Limit @ 25 Blows: N/A
	Weight of Moisture:							Plastic Limit: N/A
	% Moisture: Number of Blows:							Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:							
		Plastic I is	nit Determina	tion				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan: Weight of Pan:	Cannot	letermined plast	ic limit				
	Weight of Dry Soils:							ACCREDITED
	Weight of Moisture: % Moisture:							Certificate #: 1366.01, 1366.02 & 1366.04
	/ 0 112013tu1C1							
	70 % <b>T</b>	Plas	sticity Chart					Liquid Limit
					4			100%
	60 %			1	Line	" Lipe		90%
IJ	50 %		$\prec$		.OH _			80%
Plasticity Index	40 %	/		CA	or OH			1 ts 60%
<u>₹</u>								60%
stici	30 %							% 40% 40%
Pla	20 %	CLorOL	$\overline{}$	N 4	H or OH			30%
	10 %			IVI	n or UH			20%
	CL-ML	ML or OL						10%
	0 % 10%	20% 30% 40%	50%	50% 70%	80%	90% 1	100% 110%	0%
		L	iquid Limit					10 100 Number of Blows, "N"
	Copyright Spears Engineering & Tech	nical Services PS, 1996-98						

Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duwa roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT25-GB- ample #: B21-1818	•	Date Received: 29-Jul-21 Sampled By: Client Date Tested: 25-Sep-21 Tested By: K. Mende:	San San	nal Identification d nple Color vish-brown		
		Liquid Limit De	etermination				
			#2 #3 #4	#5	#6		
	Weight of Wet Soils + Pan:						
	Weight of Dry Soils + Pan:	Unable to esal	blish liquid limit				
	Weight of Pan:						
	Weight of Dry Soils: Weight of Moisture:				L	iquid Limit @ 25 Blows: N/A Plastic Limit: N/A	
	% Moisture:					Plasticity Index, I <sub>P</sub> : N/A	
	Number of Blows:					•	
		Plastic Limit De	etermination #2 #3 #4	#5	#6		
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan:		ined plastic limit	πJ	#0		
	Weight of Dry Soils: Weight of Moisture:  Moisture:					ACCREDITED  Certificate #: 1366.01, 1366.02 & 1366.04	
	70 % <b>T</b>	Plasticity	/ Chart		)(	Liquid Limit	
	60 %		TOT LINE	MAN LINE		90%	
Plasticity Index	40 %		CHOTOH		oisture	60%	
tici	30 %					40%	
Plas	20 %	ClorOL	MH or Oh			30%	
	10 %		ivin or Of	1		20%	
	CL-ML	ML or OL				10%	
	0 % 10% 20	0% 30% 40% 50	% 60% 70% 80%	90% 100%	110%	0%	ı
		Liquid	Limit			10 Number of Blows, "N"	
	Copyright Spears Engineering & Technic						_
	apply only to actual locations and materials is reserved pending our written approval.	tested. As a mutual protection to clients, the pu	one and ourselves, all reports are submitted as the	confidential property of clients, a	ing autnorization for publication	on of statements, conclusions or extracts from or regardi	.ng

Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

60.9%

Source: LDW21-GT25-GB-26-28.5 ft Sample#: B21-1820

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 25-Sep-21 Tested By: K. Mendez

Visual Identification Sandy Silt with Clay Sample Color: brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D43} \\ \textbf{D}_{(5)} = 0.003 \\ \textbf{D}_{(10)} = 0.008 \\ \textbf{D}_{(15)} = 0.013 \\ \textbf{D}_{(30)} = 0.043 \\ \textbf{D}_{(50)} = 0.065 \\ \textbf{D}_{(60)} = 0.074 \\ \textbf{D}_{(90)} = 0.167 \end{array}$ % Gravel = 0.0%% Sand = 39.1% mm % Silt & Clay = 60.9% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a aces = n/a Coeff. of Curvature,  $C_C = 3.28$ Coeff. of Uniformity,  $C_U = 9.69$ Fineness Modulus = 0.16 Plastic Limit = n/a

Moisture %, as sampled = 34.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

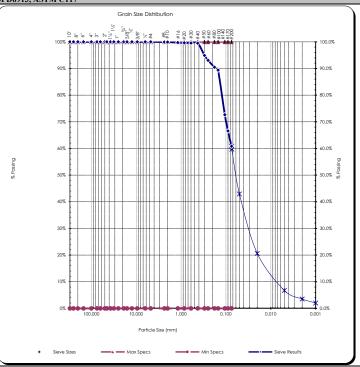
Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.167$	mm		Fractu		
						ust Ratio = 11/18		Fı	racture	%, 2+	- Fac
				AS	STM C136, AS	TM D6913, ASTN	I C117				
		Actual Cumulative	Interpolated Cumulative							Size Dist	
Sieve	Size	Percent	Percent	Specs	Specs		ъ.:	4 to 6/2	~ \$ <sub>36</sub> %	io =	. ∞⊆
US	Metric	Passing	Passing	Max	Min		100%			∂ ≥ ≟ ototot	. #±
12.00"	300.00		100%	100.0%	0.0%		- 11				
10.00"	250.00		100%	100.0%	0.0%						
8.00"	200.00		100%	100.0%	0.0%		90%			###	++-
6.00"	150.00		100%	100.0%	0.0%						
4.00"	100.00		100%	100.0%	0.0%		80%				
3.00"	75.00		100%	100.0%	0.0%		00% F				
2.50"	63.00		100%	100.0%	0.0%						
2.00"	50.00	100%	100%	100.0%	0.0%		70%			ЩЩ.	4
1.75"	45.00		100%	100.0%	0.0%						
1.50"	37.50		100%	100.0%	0.0%						
1.25"	31.50		100%	100.0%	0.0%		60%			###	++-
1.00"	25.00	100%	100%	100.0%	0.0%	D C					
3/4"	19.00	100%	100%	100.0%	0.0%	% Pasing	50%				
5/8"	16.00		100%	100.0%	0.0%	96	50% F				
1/2"	12.50	100%	100%	100.0%	0.0%						
3/8"	9.50	100%	100%	100.0%	0.0%		40%				444
1/4"	6.30		100%	100.0%	0.0%						
#4	4.75	100%	100%	100.0%	0.0%						
#8	2.36		100%	100.0%	0.0%		30%		-	###	+++
#10	2.00	100%	100%	100.0%	0.0%		11				
#16	1.18		100%	100.0%	0.0%		20%				
#20	0.850		100%	100.0%	0.0%		1000				
#30	0.600		100%	100.0%	0.0%						
#40	0.425	100%	100%	100.0%	0.0%		10%		+	###	+
#50	0.300		95%	100.0%	0.0%						
#60	0.250		93%	100.0%	0.0%						
#80	0.180		90%	100.0%	0.0%		0%	100.000	10	0.000	-
#100	0.150	89%	89%	100.0%	0.0%						
	1	1	1	1	1	1					

100.0%

100.0%

100.0%



0.0%

0.0%

0.0%

Comments:		
Reviewed by:	Alagh Bhotget aribo	
Reviewed by:	Meghan Blodgett-Carrillo	

73%

67%

60.9%



### **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Project #: 21B233 Sandy Silt with Clay Sampled By: Client Client: Anchor QEA Date Tested: 25-Sep-21 Sample Color Source: LDW21-GT25-GB-26-28.5 ft Tested By: K. Mendez brown Sample#: B21-1820 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr: 2.61 Sieve Analysis Sample Weight: 75.00 **Grain Size Distribution** Hydroscopic Moist.: 10.50% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 67.87 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 32.7% 0.0494 mm 100% 25.000 mm 22 1.0" 26.8% 0.0357 mm 3/4" 100% 19.000 mm 2 18 15.5 23.0%  $0.0230\ mm$ 5/8" 100% 16.000 mm 15 10.5 15.6%  $0.0137 \ mm$ 1/2" 100% 12.500 mm 30 13.4% 0.0097 mm 3/8" 100% 9.500 mm 0.0070 mm 60 8.9% 1/4" 100% 6.300 mm 240 5.2% 0.0036 mm 100% 4.750 mm 3.5 #4 #10 100%  $2.000\ mm$ 1440 3.0%  $0.0015 \ mm$ #20 100% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 100%  $0.425 \, mm$ % Sand: 39.1% Plastic Limit: n/a #100 89% 0.150 mm % Silt: 54.1% Plasticity Index: n/a #200 60.9%  $0.075 \ mm$ 59.8% 0.074 mm % Clay: 6.8% Silts 42.9% 0.050 mm 0.020 mm 20.6% 0.005 mm 6.8% Clays 3.5%  $0.002\ mm$ Colloids 2.0%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:

| Meghan Blodgett-Carrillo



#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Visual Identification Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Project #: 21B233 Sampled By: Client Silt with Clay Client: Anchor QEA, LLC Date Tested: 25-Sep-21 Sample Color Source: LDW21-GT33-GB-0-10.4 ft Tested By: K. Mendez orown Sample #: B21-1823 **Liquid Limit Determination** Weight of Wet Soils + Pan: 28 38 32 44 32.76 28.74 Weight of Dry Soils + Pan: 24.50 28.64 Weight of Pan: 15.01 19.79 19.63 Weight of Dry Soils: 8.85 9.11 Liquid Limit @ 25 Blows: Weight of Moisture: 3.88 3.80 4.02 Plastic Limit: 32 % % Moisture: 40.9 % 42.9 % 44.1 % Plasticity Index, I<sub>P</sub>: 10 % Number of Blows: **Plastic Limit Determination** Weight of Wet Soils + Pan: 35.43 35.12 Weight of Dry Soils + Pan: 33.78 33.45 28.27 Weight of Pan: 28.65 Weight of Dry Soils: 5.13 5.18 Weight of Moisture: 1.65 % Moisture: **Plasticity Chart Liquid Limit** 50% 60 % 45% CH or OH 40% 50 % 35% Plasticity Index 40 % 30% 25% 30 % 20% 20 % 15% MH or OH 10% 10 % ML or OL CL-M 5% 30% 60% 70% 80% 90% 100% 0% 10 100 **Liquid Limit** Number of Blows, "N' Copyright Spears Engineering & Technical Services PS, 1996-9

Comments: Reviewed by: Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT33-GB-11-18.5 ft

Sample#: B21-1825

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 25-Sep-21 Tested By: K. Mendez Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} D_{(5)} = 0.128 \\ D_{(10)} = 0.189 \\ D_{(15)} = 0.234 \\ D_{(30)} = 0.368 \\ D_{(50)} = 0.772 \\ D_{(60)} = 1.025 \\ D_{(90)} = 1.786 \\ \end{array}$ % Gravel = 0.1% % Sand = 96.5% mm % Silt & Clay = 3.4% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 0.70$ Coeff. of Uniformity,  $C_U = 5.43$ Fineness Modulus = 2.64

Plastic Limit = n/a Moisture %, as sampled = 22.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

						ust Ratio =			Fract	ure %, 2+	Faces	= n/a		Red	ı'd Frac	cture %	6, 2+ F	aces =
				AS	TM C136, AS	ΓM D6913,	ASTM C1	17										
			Interpolated						G	rain Size Dis	tribution							
		1	Cumulative		1	_												
	Size	Percent	Percent	Specs	Specs		Ě	in in i	1200	, 50 . 4 	<sub>82</sub> 2	2885	\$ 88 8 8	3458				
US	Metric	Passing	Passing	Max	Min	_	100%			**************************************			+++		ттт		ПТТ	T 100.0%
12.00"	300.00		100%	100.0%	0.0%													1
10.00"	250.00		100%	100.0%	0.0%						1 1							1
8.00"	200.00		100%	100.0%	0.0%		90% -		*****		111	-11111	ttt		$^{\dagger\dagger}$	-##		90.0%
6.00"	150.00		100%	100.0%	0.0%													1
4.00"	100.00		100%	100.0%	0.0%		80% -											80.0%
3.00"	75.00		100%	100.0%	0.0%													1
2.50"	63.00		100%	100.0%	0.0%													1
2.00"	50.00	100%	100%	100.0%	0.0%		70% -	-	++++-			++++	+++		+++		+++	70.0%
1.75"	45.00		100%	100.0%	0.0%							•						1
1.50"	37.50		100%	100.0%	0.0%							VIIII						1
1.25"	31.50		100%	100.0%	0.0%		60% -					₩	ttt		TT:T:			60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0						1						ju Bu
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50% -					l i						50.0% No.
5/8"	16.00		100%	100.0%	0.0%	96	50,0	-				1						1 00.0%
1/2"	12.50	100%	100%	100.0%	0.0%							N.						1
3/8"	9.50	100%	100%	100.0%	0.0%		40% -	<u> </u>				\			+++	-##	HHH	40.0%
1/4"	6.30		100%	100.0%	0.0%							1						1
#4	4.75	100%	100%	100.0%	0.0%								1					1
#8	2.36		99%	100.0%	0.0%		30% -				††††		₩		***	-##		30.0%
#10	2.00	98%	98%	100.0%	0.0%								N					1
#16	1.18		66%	100.0%	0.0%		20% -											20.0%
#20	0.850		53%	100.0%	0.0%		20/0						1			ШП		10.0,0
#30	0.600		43%	100.0%	0.0%			-					11					1
#40	0.425	36%	36%	100.0%	0.0%		10% -				++-		++-}-		+++		+++	10.0%
#50	0.300		22%	100.0%	0.0%								\					-1
#60	0.250		17%	100.0%	0.0%									**				1
#80	0.180		9%	100.0%	0.0%		0%	100	000	10.000		1.000	9-00-00	0.100		0.010		0.0%
#100	0.150	6%	6%	100.0%	0.0%													
#140	0.106		4%	100.0%	0.0%					Particl	e Size (mm	)						
#170	0.090		4%	100.0%	0.0%													
#200	0.075	3.4%	3.4%	100.0%	0.0%		+ Sieve Siz	zes		Max Specs		<b></b> -	Min Spe	cs	_	Siev	e Results	
Copyrigh	Spears Engineering & Tec	hnical Services PS, 1996-9	8															
results apply only to		s tested. As a mutual prote	etion to cliente the public			21	1' - 1 - 1		11' 4' (	-1-1			ſ	-		_	-	

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1825
Sample Date:	7/15/2021
Test Date:	10/1/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT33-GB-11-18.5 ft

 Visual Soil Description:
 brown sand with silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

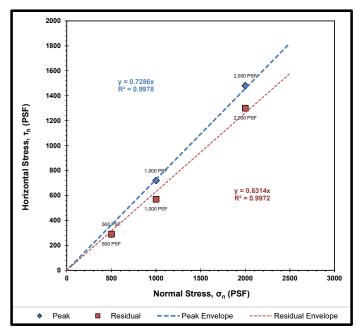
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	le Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	27.4	
	Initial	Post-Consolidation
Dry Density (PCF):	105.9	106.9
Void Ratio:	0.591	0.577
Porosity (%):	37.2	36.6
Degree of Saturation (%):	saturated	saturated

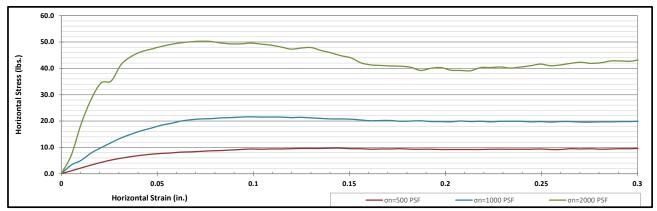
Summary of Samp	le Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	27.4	
	Initial	Post-Consolidation
Dry Density (PCF):	106.2	107.7
Void Ratio:	0.586	0.564
Porosity (%):	36.9	36.1
Degree of Saturation (%):	saturated	saturated

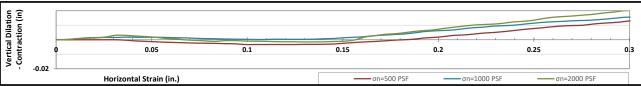
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	26.6	
	Initial	Post-Consolidation
Dry Density (PCF):	106.1	108.6
Void Ratio:	0.589	0.551
Porosity (%):	37.0	35.5
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS									
PEAK RESIDUAL									
Angle of Internal Friction, φ (°):	38	32							
Cohesion (PSF):	0	0							



Failure Envelope Test Values:										
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000							
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	290	720	1480							
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	570	1300							

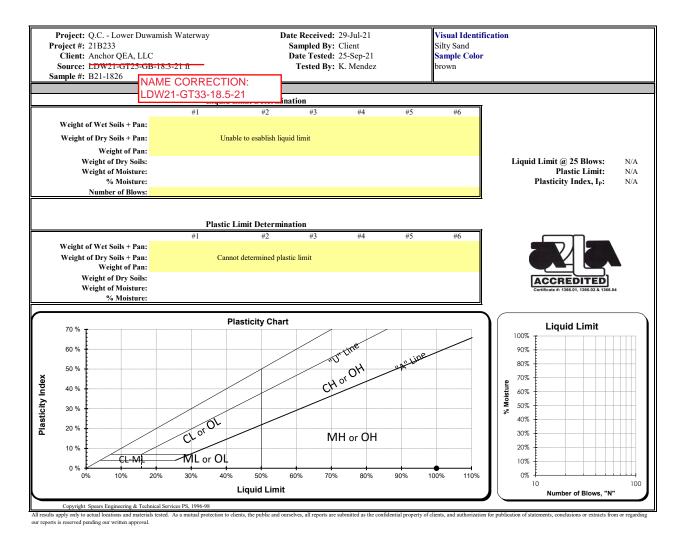




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### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



Comments: Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT33-GB-21-26.8 ft Sample#: B21-1828

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 25-Sep-21 Tested By: K. Mendez Unified Soils Classification System, ASTM D-2487

ML, Sandy Silt Sample Color:

mm

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.004 \\ \textbf{D}_{(10)} = 0.007 \\ \textbf{D}_{(15)} = 0.010 \\ \textbf{D}_{(30)} = 0.036 \\ \textbf{D}_{(50)} = 0.064 \\ \textbf{D}_{(60)} = 0.074 \\ \textbf{D}_{(90)} = 0.141 \\ \textbf{Partice} = 43/70 \\ \textbf{D}_{(10)} = 43/$ % Gravel = 0.0%% Sand = 38.9% mm % Silt & Clay = 61.1% mm Liquid Limit = 0.0% mm mm Plasticity Index = 0.0% mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 2.51$ Coeff. of Uniformity,  $C_U = 10.39$ Fineness Modulus = 0.10

Plastic Limit = 0.0% Moisture %, as sampled = 34.4% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

						st Ratio = 43/70		1	racture	%, 2-	+ Fac	es = n/	a		Req'd	Fract	ıre %	2+ Fa	ces =
				AS	STM C136, AST	M D6913, ASTM	C117												
		Actual Cumulative	Interpolated			r			Grain	Size Dis	tributio	n							
Sieve	C:	,		C	C				ž										
US	Metric Metric	Percent Passing	Percent Passing	Specs Max	Specs Min		9 9 9	4 % %	7. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	3/8	<b>∞</b> Ω	128	988	884	82				
12.00"	300.00	rassing	100%	100.0%	0.0%	100	%	****		m		<b>-</b> • • • • •	TÎN!	**	+	П	TTTTT		100.0%
10.00"	250.00		100%	100.0%	0.0%								100	•.					1
8.00"	200.00		100%	100.0%	0.0%	9	<sub>%</sub>						Ш	Ĺ			ШШ		90.0%
6.00"	150.00		100%	100.0%	0.0%		~							1					70.0%
4.00"	100.00		100%	100.0%	0.0%									1					1
						81	% <del> </del>	-###		-###	++-+			+					80.0%
3.00"	75.00		100%	100.0%	0.0%									1					1
2.50" 2.00"	63.00	1000/	100%	100.0% 100.0%	0.0% 0.0%									i					1
	50.00	100%	100%			70	% <del>     </del>	-11111					###				###		70.0%
1.75"	45.00		100%	100.0%	0.0%														1
1.50"	37.50		100%	100.0%	0.0%	4	<sub>%</sub>												60.0%
1.25"	31.50	1000/	100%	100.0%	0.0%										TIII				
1.00"	25.00	100%	100%	100.0%	0.0%	Possing									\				3 sing
3/4"	19.00	100%	100%	100.0%	0.0%	E 50	% <del> </del>							-					50.0% %
5/8"	16.00		100%	100.0%	0.0%	-									II \				1
1/2"	12.50	100%	100%	100.0%	0.0%										*				1
3/8"	9.50	100%	100%	100.0%	0.0%	40	7%	-11111	++-+-		+++		+++-		###\	$\vdash$	-		40.0%
1/4"	6.30		100%	100.0%	0.0%		H								III I \				1
#4	4.75	100%	100%	100.0%	0.0%	24	%								۱ ۱۱۱۱۱۱	<b>(</b>			30.0%
#8	2.36		100%	100.0%	0.0%	3	<sup>70</sup> [ ]						III			\			30.0%
#10	2.00	100%	100%	100.0%	0.0%											М.			1
#16	1.18		100%	100.0%	0.0%	21	% <del>  </del>				444		444-	1		<u> </u>	Ш		20.0%
#20	0.850		100%	100.0%	0.0%											$  \   \  $			1
#30	0.600		100%	100.0%	0.0%											l I '	VIII.		1
#40	0.425	99%	99%	100.0%	0.0%	10	%	-###	++-		+++		++-	$+-\parallel$	+++	$\vdash\vdash$	₩	$\vdash$	10.0%
#50	0.300		97%	100.0%	0.0%														1
#60	0.250		96%	100.0%	0.0%		_ []_	ШШ					Ш					*	*
#80	0.180		94%	100.0%	0.0%	· '	)% <b>000-0</b>	00.000		0.000		1.000		0.10	10	0.	010		→ 0.0% 0.001
#100	0.150	94%	94%	100.0%	0.0%														
#140	0.106		75%	100.0%	0.0%					Partic	le Size (n	nm)							
#170	0.090		68%	100.0%	0.0%														
#200	0.075	61.1%	61.1%	100.0%	0.0%	+ Siev	e Sizes	_	<b>—</b> M	ax Specs		-	- Min	Specs			- Sieve	Results	
Copyright	Spears Engineering & Tec	hnical Services PS, 1996-9	3																

Reviewed by:



#### **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 ML, Sandy Silt Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 25-Sep-21 Sample Color Source: LDW21-GT33-GB-21-26.8 ft Tested By: K. Mendez brown Sample#: B21-1828 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 75.85 **Grain Size Distribution** 3.68% Soils Particle Hydroscopic Moist .: Sieve Percent ACCREDITED Adj. Sample Wgt: 73.16 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0477 mm 100% 25.000 mm 25 34 2% 1.0" 0.0347 mm 3/4" 100% 19.000 mm 2 21.5 29 4% 17.5 23.9%  $0.0224\ mm$ 5/8" 100% 16.000 mm 15 12.5 17.1% 0.0133 mm 1/2" 100% 12.500 mm 30 14.4% 0.0096 mm 3/8" 100% 9.500 mm 60 9.6% 0.0069 mm 1/4" 100% 6.300 mm 240 3.5 4.8% 0.0035 mm 100% 4.750 mm #4 #10  $2.000\ mm$ 1440 3.4%  $0.0014\ mm$ 100% #20 100% 0.850 mm Liquid Limit: 0.0 % % Gravel: 0.0% #40 99%  $0.425 \, mm$ % Sand: 38.9% Plastic Limit: 0.0 % #100 94% 0.150 mm % Silt: 54.2% Plasticity Index: 0.0 % #200 61.1%  $0.075 \ mm$ 0.074 mm % Clay: 6.9% Silts 60.1% 44.4% 0.050 mm 0.020 mm 22.1% 6.9% 0.005 mm Clays 3.8%  $0.002\ mm$ Colloids 2.4%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:

Meghan Blodgett-Carrillo



#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duw roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT33-GI ample #: B21-1828	D		te Received: Sampled By: Date Tested: Tested By:	Client 25-Sep-21		Unified Soils Cl ML, Sandy Silt Sample Color brown	lassification System, ASTM D-2487
			nit Determina					
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan:	Unable	to esablish liqu	d limit				
	Weight of Pan: Weight of Dry Soils:							Liquid Limit @ 25 Blows: N/A
	Weight of Moisture:							Plastic Limit: N/A
	% Moisture: Number of Blows:							<b>Plasticity Index, I<sub>P</sub>:</b> N/A
	Number of Blows:							
		DI di Ti	** TS					
		#1	mit Determina #2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:		2	","		5		
	Weight of Dry Soils + Pan:	Cannot	determined plast	ic limit				
	Weight of Pan: Weight of Dry Soils:							ACCREDITED
	Weight of Moisture:							Certificate #: 1366.01, 1366.02 & 1366.04
	% Moisture:							
$\bigcap$	70 % <b>T</b>	Plas	sticity Chart					Liquid Limit
	/0 % <b>[</b>							100%
	60 %				Line	" Line		90%
	50 %			T,	, al	MA"LLITTE		80%
ĕ				-14	or OH			9 70% E
Plasticity Index	40 %			- Cr				an to 60%
city	30 %							S 50%
asti		OL OL						40%
ä	20 %	CLorOL		М	H or OH			30%
	10 %							20%
	0 % CL-ML	ML or OL						10%
		20% 30% 40%		60% 70%	80%	90% 1	100% 110%	0%
		L	iquid Limit					Number of Blows, "N"
	Copyright Spears Engineering & Tech	nical Services PS, 1996-98						

Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without

tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Pi	Project: Q.C Lower Duw roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT33-GF ample #: B21-1829	2	5	te Received: Sampled By: Date Tested: Tested By:	Client 25-Sep-21		Visual Identific Silty Sand Sample Color brown	cation
	<u> </u>		mit Determina				1	·
	w	#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	** 11	. 1818	110 5				
	Weight of Dry Soils + Pan: Weight of Pan:	Unable	e to esablish liqui	d limit				
	Weight of Dry Soils:							Liquid Limit @ 25 Blows: N/A
	Weight of Moisture:							Plastic Limit: N/A
	% Moisture: Number of Blows:							Plasticity Index, I <sub>P</sub> : N/A
		Plastic Li	mit Determina #2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan:	Cannot	determined plast	ic limit				
	Weight of Dry Soils: Weight of Moisture: % Moisture:							ACCREDITED  Certificate #: 1366.01, 1366.02 & 1366.04
	70.0/	Pla	sticity Chart					Liquid Limit
	70 %				, tine	المناهدات المناهدات		100%
L L	50 %				or OH	THE THIE		80%
Plasticity Index	40 %			Ch	or			70%
city	30 %							50%
astic		OL OL						40%
ā	20 %	CLorOL		М	H or OH			30%
	10 %							20%
	0 % CL-ML	ML or OL					-	10%
	0% 10%	20% 30% 40%		60% 70%	80%	90% 1	00% 110%	0% <del> </del> 10 100
			iquid Limit					Number of Blows, "N"
	Copyright Spears Engineering & Tech	nical Services PS, 1996-98						

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Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

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Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

**Source:** LDW21-GT33-GB-28.8-29.5 ft **Sample#:** B21-1830

Sample Meets Specs? N/A

Specifications

No Specs

#16

#20

#30

#40

#50

#60

#80 #100

#140

#170

#200

Comments:

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 25-Sep-21

Tested By: K. Mendez

Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color: brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Coeff. of Curvature,  $C_C = 0.90$ Coeff. of Uniformity,  $C_U = 4.50$ Fineness Modulus = 0.78 Plastic Limit = n/a

Moisture %, as sampled = 33.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

ASIM	C136, ASTM D6913, ASTM C1	. /

					D
				AS	STM C136, AS
		Actual	Interpolated		
		Cumulative	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%

99%

99%

99%

99%

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100.0%

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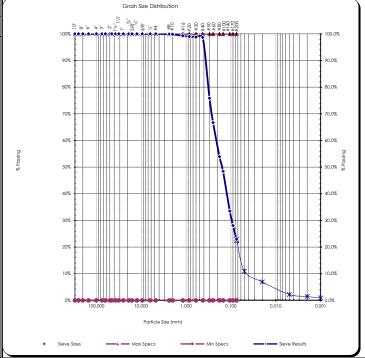
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99%

23.0%



### **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soils Classification System, ASTM D-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 25-Sep-21 Sample Color Source: LDW21-GT33-GB-28.8-29.5 ft Tested By: K. Mendez brown Sample#: B21-1830 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 80.02 **Grain Size Distribution** 4.80% Soils Particle Hydroscopic Moist .: Sieve Percent ACCREDITED Adj. Sample Wgt: 76.35 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 10.5% 0.0529 mm 100% 25.000 mm 1.0" 3/4" 100% 19.000 mm 2 9.2% 0.0376 mm 5.5 7.2%  $0.0240 \ mm$ 5/8" 100% 16.000 mm 15 6.5% 0.0139 mm 1/2" 100% 12.500 mm 30 5.2% 0.0098 mm 3/8" 100% 9.500 mm 60 2.6% 0.0070 mm 1/4" 100% 6.300 mm 240 2.0% 0.0035 mm 100% 4.750 mm 1.5 #4 #10 100%  $2.000\ mm$ 1440 1.3%  $0.0014\ mm$ #20 99% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 99%  $0.425 \, mm$ % Sand: 77.0% Plastic Limit: n/a #100 48% 0.150 mm % Silt: 20.8% Plasticity Index: n/a #200 23.0%  $0.075 \ mm$ 22.4% 0.074 mm % Clay: 2.2% Silts 10.9% 0.050 mm 0.020 mm 6.9% 2.2% 0.005 mm Clays 1.5%  $0.002\ mm$ Colloids 0.9% $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by: Meghan Blodgett-Carrillo



#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duw roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT33-GI ample #: B21-1831	D	:	te Received: Sampled By: Date Tested: Tested By:	Client 25-Sep-21		Visual Identific Sandy Silt Sample Color brown	ation
		Liquid Lin	mit Determina	ntion				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:							
	Weight of Dry Soils + Pan:	Unable	to esablish liqui	id limit				
	Weight of Pan:							1: :11: :4 \( \alpha \)
	Weight of Dry Soils: Weight of Moisture:							Liquid Limit @ 25 Blows: N/A Plastic Limit: N/A
	% Moisture:							Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:							
		#1	mit Determina #2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	#1	#2	#3	#4	#3	#0	
	Weight of Dry Soils + Pan:	Cannot	determined plast	ic limit				
	Weight of Pan: Weight of Dry Soils:							
	Weight of Moisture:							Certificate #: 1366.01, 1366.02 & 1366.04
	% Moisture:							
$\overline{}$	70 % <b>T</b>	Plas	sticity Chart					Liquid Limit
	70 % [							100%
	60 %				tine	" Line		90%
	50 %			T.	, oH	MA"LALLE		80%
ĕ				٠,١	or OH			<u>e</u> 70%
Plasticity Index	40 %			- G,				60%
city	30 % =							<b>50%</b> 50%
asti	20 %	OL						40%
ਾ	20%	CLorOL		М	H or OH			30%
	10 %							20%
	0 % CL-ML	ML or OL					<u> </u>	10%
	0% 10%	20% 30% 40%		60% 70%	80%	90% 1	100% 110%	0% + 10 100
		L	iquid Limit					Number of Blows, "N"
	Copyright Spears Engineering & Tech	nical Services PS, 1996-98						

Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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Client:	Anchor QEA	Date:	October 19, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-1948 - 1965
Revised on:		Date sampled:	July 16, 2021

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor	Trease see Tituenea Reports		Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 1, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-1948	LDW21-GT39-GB-0-1.5 ft	182.2	359.3	304.7	54.6	122.5	44.6%
B21-1949	LDW21-GT39-GB-0-8.8 ft	229.5	1120.6	890.6	230.0	661.1	34.8%
B21-1950	LDW21-GT39-GB-8.8-10.5 ft	234.3	1839.1	1517.6	321.5	1283.3	25.1%
B21-1951	LDW21-GT39-GB-10.5-12 ft	222.9	1270.1	1072.1	198.0	849.2	23.3%
B21-1952	LDW21-GT39-GB-10.5-20.5 ft	228.8	652.9	584.6	68.3	355.8	19.2%
B21-1953	LDW21-GT39-GB-20.5-21 ft	225.2	577.3	508.6	68.7	283.4	24.2%
B21-1954	LDW21-GT39-GB-20.5-30.5 ft	234.4	1327.0	1148.4	178.6	914.0	19.5%
B21-1955	LDW21-GT39-GB-30.5-32 ft	233.2	876.4	747.6	128.8	514.4	25.0%
B21-1956	LDW21-GT23-GB-0-1.5 ft	223.0	462.7	361.7	101.0	138.7	72.8%
B21-1957	LDW21-GT23-GB-0-8.2 ft	221.9	900.9	625.0	275.9	403.1	68.4%
B21-1958	LDW21-GT23-GB-8.5-10 ft	215.4	919.5	775.8	143.7	560.4	25.6%
B21-1959	LDW21-GT23-GB-8.5-17.6 ft	234.7	1060.0	934.4	125.6	699.7	18.0%
B21-1960	LDW21-GT23-GB-17.6-18.5 ft	217.3	972.1	771.5	200.6	554.2	36.2%
B21-1961	LDW21-GT23-GB-18.5-20 ft	270.1	687.9	581.4	106.5	311.3	34.2%
B21-1962	LDW21-GT23-GB-21.1-22.8 ft	222.3	1022.4	815.3	207.1	593.0	34.9%
B21-1963	LDW21-GT23-GB-22.8-26.8 ft	266.3	870.9	724.1	146.8	457.8	32.1%
B21-1964	LDW21-GT23-GB-27.7-28.5 ft	224.7	963.8	779.9	183.9	555.2	33.1%
B21-1965	LDW21-GT23-GB-30.5-32 ft	235.2	627.7	539.1	88.6	303.9	29.2%
				-			

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 20, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Dry Soil + Tare	Mass of Dry Soil	Pycno ID	Mass of Pycno	Volume of Pycno	Density of Water @ Tx	Mass of Pycno filled w/ water & soils	Mass of	Temp. of Water, 0.1	SpG of Soils	Temp. Correction Factor	Corrected SpG
B21-1952	LDW21-GT39-GB-10.5-20.5 ft	493.16	568.87	75.7	TSA-014	192.3	499.5	0.99858	738.22	691.08				2.6508905
B21-1957	LDW21-GT23-GB-0-8.2 ft	584.01	660.92	76.9	TSA-013	184.0	499.7	0.99858	729.36	682.95	18.1	2.5216018	1.00037	2.5225348
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

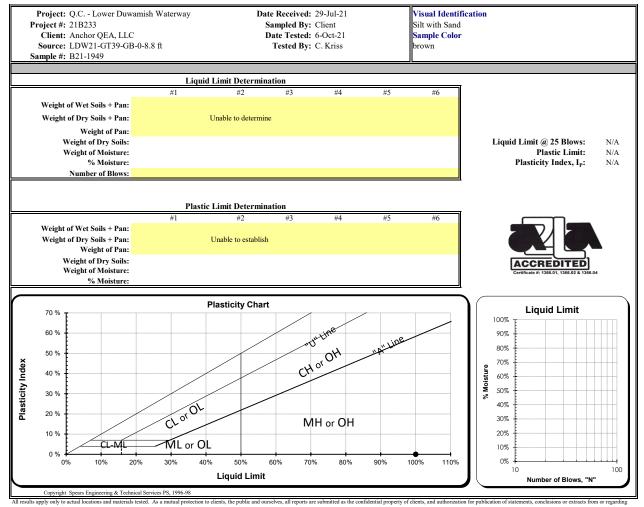
Meghan Blodgett-Carrillo

### Materials Testing & Consulting, Inc.



Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting

#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



our reports is reserved pending our written approval.

Comments: Liquid limit cannot be determined as the material displays rapid dilation. At lower moistures the sample does not spread into the cup without tearing the soil cake. Unable to establish plastic limit as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo

Visit our website: www.mtc-inc.net



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT39-GB-8.8-10.5 ft

Sample#: B21-1950

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21

Tested By: K. Mendez

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand Sample Color:

grayish-brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} D_{(5)} = 0.157 \\ D_{(10)} = 0.187 \\ D_{(15)} = 0.218 \\ D_{(30)} = 0.311 \\ D_{(50)} = 0.471 \\ D_{(60)} = 0.777 \\ D_{(60)} = 1.696 \end{array}$ % Gravel = 0.0%% Sand = 98.0% mm % Silt & Clay = 2.0% mm Liquid Limit = n/a mm mm Plasticity Index = n/a Sand Equivalent = n/a

n/a

Coeff. of Curvature,  $C_C = 0.66$ Coeff. of Uniformity,  $C_U = 4.15$ Fineness Modulus = 2.40

Plastic Limit = n/a Moisture %, as sampled = 25.0% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

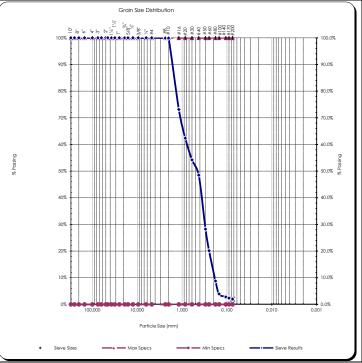
						$D_{(90)} = 1.696$	mm	F	racture %,	1 Fac	ce = n/	1
					D	oust Ratio = 1/24		Frac	cture %, 2-	+ Face	es = n/	1
				AS	STM C136, AS	TM D6913, ASTM	I C117					
		Actual	Interpolated						Grain Size Dis	tributio	n	
		-	Cumulative					Ę.				
Sieve		Percent	Percent	Specs	Specs		.0 .6 .5	± ½ ½ 3.4 = ½ 3.44	3/8"	- so-	288	2
US	Metric	Passing	Passing	Max	Min		100%	• • • • • •	•	7	-	į
12.00"	300.00		100%	100.0%	0.0%		- 1					
10.00"	250.00		100%	100.0%	0.0%		90%				\	
8.00"	200.00		100%	100.0%	0.0%		90%					***************************************
6.00"	150.00		100%	100.0%	0.0%						1	
4.00"	100.00		100%	100.0%	0.0%		80%	ШШ		$\bot \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \!$	$\perp \parallel \parallel$	
3.00"	75.00		100%	100.0%	0.0%						1 1111	
2.50"	63.00		100%	100.0%	0.0%						1	
2.00"	50.00	100%	100%	100.0%	0.0%		70%	+++++		+++	$-+\cdots$	
1.75"	45.00		100%	100.0%	0.0%		- [ ]				V	
1.50"	37.50		100%	100.0%	0.0%						•	
1.25"	31.50		100%	100.0%	0.0%		60%	mm		+++	1	1
1.00"	25.00	100%	100%	100.0%	0.0%	g g					N.	į
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%					
5/8"	16.00		100%	100.0%	0.0%	84	1					
1/2"	12.50	100%	100%	100.0%	0.0%		-					
3/8"	9.50	100%	100%	100.0%	0.0%		40%	₩₩₩	+-+++++++++++++++++++++++++++++++++++	+++		
1/4"	6.30		100%	100.0%	0.0%							
#4	4.75	100%	100%	100.0%	0.0%							
#8	2.36		100%	100.0%	0.0%		30%			+++		i
#10	2.00	100%	100%	100.0%	0.0%							
#16	1.18		73%	100.0%	0.0%		20%					
#20	0.850		62%	100.0%	0.0%		20,0					
#30	0.600		54%	100.0%	0.0%							
#40	0.425	49%	49%	100.0%	0.0%		10%	₩₩		+++		
#50	0.300		28%	100.0%	0.0%							
#60	0.250	1	20%	100.0%	0.0%							
#80	0.180	1	9%	100.0%	0.0%		0%	0.000	10.000	-	1.000	ì
#100	0.150	4%	4%	100.0%	0.0%		100					
#140	0.106		3%	100.0%	0.0%				Partic	le Size (m	nm)	
U170	0.000		20/	100.00/	0.00/	П						

100.0%

100.0%

2%

2.0%



Comments:			
	March Plabact and		

0.0%

0.0%

Meghan Blodgett-Carrillo

2.0%

0.090

0.075

#170

#200

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#30

#40 #50

#60

#80 #100

#140

#170

#200

**Comments:** 

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

42%

7.0%

Source: LDW21-GT39-GB-10.5-20.5 ft Sample#: B21-1952

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21

Tested By: K. Mendez

SP-SM, Poorly graded Sand with Silt Sample Color:

grayish-brown



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.053$   $D_{(10)} = 0.121$   $D_{(15)} = 0.178$   $D_{(30)} = 0.313$ % Gravel = 1.1% % Sand = 91.9% mm % Silt & Clay = 7.0% mm Liquid Limit = n/a mm  $D_{(50)} = 0.638$ mm Plasticity Index = n/a  $D_{(60)} = 0.919$ mm Sand Equivalent = n/a  $D_{(90)} = 1.762$ Dust Ratio = 1/6 Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

Unified Soil Classification System, ASTM-2487

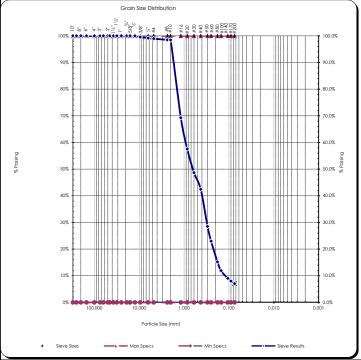
Plastic Limit = n/a Moisture %, as sampled = 19.2% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

Coeff. of Curvature,  $C_C = 0.88$ Coeff. of Uniformity,  $C_U = 7.60$ 

Fineness Modulus = 2.45

						D(90) 1.	702 111111
				4.6			1/6
		Actual Cumulative	Interpolated Cumulative	AS	TM C136, AS	1M D6913, A	STM C117
Sieve	Size	Percent	Percent	Specs	Specs	1	
US	Metric	Passing	Passing	Max	Min		È io ₹ 100% <b>♦.♦.</b> ♦.4
12.00"	300.00		100%	100.0%	0.0%	1	
10.00"	250.00		100%	100.0%	0.0%		H
8.00"	200.00		100%	100.0%	0.0%		90%
6.00"	150.00		100%	100.0%	0.0%		F
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		80%
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		70%
1.75"	45.00		100%	100.0%	0.0%		t I
1.50"	37.50		100%	100.0%	0.0%		l l
1.25"	31.50		100%	100.0%	0.0%		60%
1.00"	25.00	100%	100%	100.0%	0.0%	2	ł I
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50%
5/8"	16.00		100%	100.0%	0.0%	№	30%
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		40%
1/4"	6.30		99%	100.0%	0.0%		
#4	4.75	99%	99%	100.0%	0.0%		
#8	2.36		99%	100.0%	0.0%		30%
#10	2.00	98%	98%	100.0%	0.0%		ł I
#16	1.18		69%	100.0%	0.0%		20%
#20	0.850		58%	100.0%	0.0%		-5%



0.0%

0.0%

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0.0%

0.0%

Reviewed by: Meghan Blodgett-Carrillo

49%

42%

29%

23%

15%

12%

9%

8%

7.0%

100.0%

100.0%

100.0%

100.0%

100.0%

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100.0%

100.0%

100.0%

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1952
Sample Date:	7/16/2021
Test Date:	10/4/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT39-GB-10.5-20.5 ft

 Visual Soil Description:
 grayish-brown sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

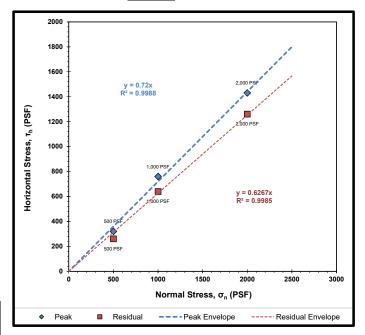
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	26.0	
	Initial	Post-Consolidation
Dry Density (PCF):	109.4	111.1
Void Ratio:	0.540	0.516
Porosity (%):	35.1	34.0
Degree of Saturation (%):	saturated	saturated

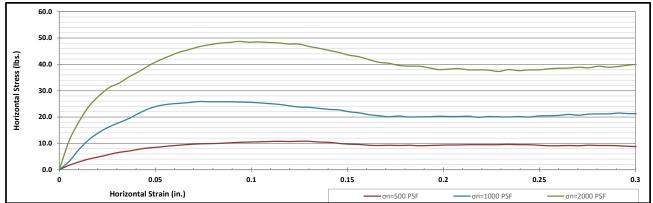
Summary of Sample	le Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	26.7	
	Initial	Post-Consolidation
Dry Density (PCF):	107.4	109.6
Void Ratio:	0.569	0.537
Porosity (%):	36.3	34.9
Degree of Saturation (%):	saturated	saturated

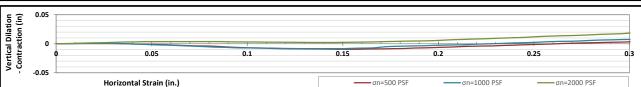
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	25.2	
	Initial	Post-Consolidation
Dry Density (PCF):	109.0	113.2
Void Ratio:	0.546	0.488
Porosity (%):	35.3	32.8
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS								
	PEAK	RESIDUAL						
Angle of Internal Friction, φ (°):	36	32						
Cohesion (PSF):	0	0						



Failure Envelope Test Values:								
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000					
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	320	760	1430					
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	260	640	1260					





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT39-GB-20.5-30.5 ft Sample#: B21-1954

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21

Tested By: K. Mendez

Sample Color:

gray

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{AS1M D4S} \\ \textbf{D}_{(5)} = 0.153 \\ \textbf{D}_{(10)} = 0.197 \\ \textbf{D}_{(15)} = 0.241 \\ \textbf{D}_{(30)} = 0.371 \\ \textbf{D}_{(50)} = 0.789 \\ \textbf{D}_{(60)} = 1.051 \\ \textbf{D}_{(90)} = 1.839 \\ \textbf{Partia} = 1.1/3 \end{array}$ % Gravel = 2.1% % Sand = 95.1% mm % Silt & Clay = 2.8% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

Coeff. of Curvature,  $C_C = 0.67$ Coeff. of Uniformity,  $C_U = 5.34$ Fineness Modulus = 2.73

Plastic Limit = n/a Moisture %, as sampled = 19.5% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

$D_{(90)} = 1.839$ mm	Fracture %, 1 Face = n/a
Dust Ratio = 1/13	Fracture $\%$ , 2+ Faces = $n/a$
C136, ASTM D6913, ASTM C117	

					D	ust Ratio =	1/13	F	racture 9	6, 2+ Fac	es = n/a		Req'd F	racture	%, 2+1	Faces =	
				AS	TM C136, AS	ΓM D6913,	ASTM C11	7									
		Actual	Interpolated						Crain Si	e Distributio	n						$\overline{}$
		Cumulative	Cumulative						GIGHT 312	e Distributio	11						1
Sieve	Size	Percent	Percent	Specs	Specs		ь	90 44 90 91	1% 1% 1. 1% 5/8% 5/8%	7.4 % 2	2089	6 88 88 <del>8</del>	28				
US	Metric	Passing	Passing	Max	Min			<b>***=****</b>		; × 4 + 4	* 4 * :	* * * * * * * * * * * * * * * * * * *	# <u>`</u>			<del>-</del> 100.0%	
12.00"	300.00		100%	100.0%	0.0%	1				T**+						- 1	
10.00"	250.00		100%	100.0%	0.0%		t									1	
8.00"	200.00		100%	100.0%	0.0%		90%	+				++-+		+		90.0%	
6.00"	150.00		100%	100.0%	0.0%		ŀ				\					1	
4.00"	100.00		100%	100.0%	0.0%		80%				\					80.0%	
3.00"	75.00		100%	100.0%	0.0%		80%									80.0%	
2.50"	63.00		100%	100.0%	0.0%		1									- 1	
2.00"	50.00	100%	100%	100.0%	0.0%		70%				111111			+-111		70.0%	
1.75"	45.00		100%	100.0%	0.0%		ŀ				<b>\</b>					1	
1.50"	37.50		100%	100.0%	0.0%		ŀ				i					1	
1.25"	31.50		100%	100.0%	0.0%		60%				-1	++-+		+		60.0%	
1.00"	25.00	100%	100%	100.0%	0.0%	p p	ŀ				NIII I					1 5	b
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				1					50.0%	j
5/8"	16.00		100%	100.0%	0.0%	96	50%				N N					50.0%	:
1/2"	12.50	99%	99%	100.0%	0.0%						N					- 1	
3/8"	9.50	99%	99%	100.0%	0.0%		40%				W\			1 11		40.0%	
1/4"	6.30		98%	100.0%	0.0%		ŀ									1	
#4	4.75	98%	98%	100.0%	0.0%		ŀ					1				1	
#8	2.36		96%	100.0%	0.0%		30%					+-				30.0%	
#10	2.00	96%	96%	100.0%	0.0%		F					1				- 1	
#16	1.18		65%	100.0%	0.0%											1	
#20	0.850		52%	100.0%	0.0%		20%					11				20.0%	
#30	0.600		43%	100.0%	0.0%							1				- 1	
#40	0.425	36%	36%	100.0%	0.0%		10%	4				++1				10.0%	
#50	0.300	,	22%	100.0%	0.0%		<b>!</b>					1				- 1	
#60	0.250		16%	100.0%	0.0%		ŀ					1 2	••			1	
#80	0.180		8%	100.0%	0.0%		0%	100.000	10.0		1.000	d do loo d 0.1	00	0.010	шш	0.0%	
#100	0.150	5%	5%	100.0%	0.0%			100.000	10.0	~	1.000	0.1		0.010		0.001	
#140	0.106		4%	100.0%	0.0%					Particle Size (n	nm)						
#170	0.090		3%	100.0%	0.0%												
#200	0.075	2.8%	2.8%	100.0%	0.0%		Sieve Size		<b>-</b> ▲ <b>-</b> Max S	pecs		- Min Specs	_	Sie	ive Results		
		chnical Services PS, 1996-9	1	100.070	0.070							.,		-			_)
PJ11B11	1 1				<del></del>							_			_		_

Reviewed by:



#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duwa roject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT23-GB- ample #: B21-1957	·		te Received: Sampled By: Date Tested: Tested By:	Client 6-Oct-21		Visual Identific Silt with Sand Sample Color brown	eation
		Liqui	d Limit Determin	nation				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	33.87	31.07	35.40				
	Weight of Dry Soils + Pan:	29.74	27.66	30.53				
	Weight of Pan:	19.98	19.72	19.51				
	Weight of Dry Soils:	9.76	7.94	11.02				Liquid Limit @ 25 Blows: 42 %
	Weight of Moisture: % Moisture:	4.13 42.3 %	3.41 43.0 %	4.87 44.2 %				Plastic Limit: N/A Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:	42.3 %	43.0 %	13				riasticity fildex, Ip: N/A
		Plastic	c Limit Determin	nation #3	#4	#5	#6	
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan:		Unable to establis					
	Weight of Dry Soils: Weight of Moisture: % Moisture:							ACCREDITED  Certificate #: 1366.01, 1366.02 & 1366.04
			Plasticity Char	<del></del> t				1:
	<sup>70 %</sup> T							Liquid Limit
	60 %				i tine			45%
				my		عمند".		40%
v	50 % -				.OH _			35%
	40 %			CH	or OH			nt 30%
g G								<del>                                  </del>
y Inde								
ticity Inde	30 %							
lasticity Inde		, OL						20%
Plasticity Index	30 %	ClorOL		M	H or OH			20%
Plasticity Inde	20 %	Ol or OL		M	H or OH			20%
Plasticity Index	20 % CL-ML	CL or O		M	H or OH			20%
Plasticity Inde	20 %	ML or O	L	M 60% 70%		90% 1	00% 110%	20% 15% 10% 5%
Plasticity Index	20 % 10 % CL-ML	ML or O	L	60% 70%		90% 1	00% 110%	20% 15% 10%

Comments: Unable to establish plastic limit as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT23-GB-8.5-17.6 ft Sample#: B21-1959

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21

Tested By: K. Mendez

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt Sample Color:

grayish-brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} \textbf{ASIN D43} \\ \textbf{D}_{(5)} = 0.056 \\ \textbf{D}_{(10)} = 0.102 \\ \textbf{D}_{(15)} = 0.142 \\ \textbf{D}_{(30)} = 0.292 \\ \textbf{D}_{(50)} = 0.667 \\ \textbf{D}_{(60)} = 1.020 \\ \textbf{D}_{(90)} = 2.624 \\ \textbf{Partia} = -7/45 \end{array}$ % Gravel = 2.5% % Sand = 90.8% mm % Silt & Clay = 6.7% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 0.82$ Coeff. of Uniformity,  $C_U = 10.03$ Fineness Modulus = 2.55

Plastic Limit = n/a Moisture %, as sampled = 18.0% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

						t Ratio = 7/45		Fracture 9	6, 2+ Fa	ces = n	/a	R	eq'd F	racture	%, 2+	Faces =
		Actual	Interpolated	AS	TM C136, AST	M D6913, ASTM C1	17									
		Cumulative			ľ			Grain Siz	e Distribu	tion						
Sieve	Cino	Percent	Percent	Su ann	Smaga			St. 1.								
US	Metric	Passing	Passing	Specs Max	Specs Min	ğ	3.4 4.60 €	27 17 17 17 17 18 18 18	7 ¥ 9	128	8 4 8 8	85458				
12.00"	300.00	rassing	100%	100.0%	0.0%	100% 🗴		(000000	No.	+ ++	<del>1</del>	***	ППТ			100.0%
10.00"	250.00		100%	100.0%	0.0%											1
8.00"	200.00		100%	100.0%	0.0%	90% -			<i>\</i>		ШШ		Ш			90.0%
6.00"	150.00		100%	100.0%	0.0%	70,0			1111111	<b>\</b>						70.0%
4.00"	100.00		100%	100.0%	0.0%					<b>\</b>						1
						80% -				4						80.0%
3.00"	75.00		100%	100.0%	0.0%					11 11						1
2.50" 2.00"	63.00	100%	100%	100.0%	0.0% 0.0%					11						1
	50.00	100%	100%	100.0%		70% -			****	1111	+++	1	HH	1-11		70.0%
1.75"	45.00		100%	100.0%	0.0%					1 1 1						1
1.50"	37.50		100%	100.0%	0.0%	60% -				\						60.0%
1.25"	31.50	1000/	100%	100.0%	0.0%					l X						1 00.00
1.00"	25.00	100%	100%	100.0%	0.0%	50% -				1 1						
3/4"	19.00	100%	100%	100.0%	0.0%	50% -					<b>!</b>		Ш.			50.0%
5/8"	16.00		100%	100.0%	0.0%	•					XIII					
1/2"	12.50	100%	100%	100.0%	0.0%						1					1
3/8"	9.50	99%	99%	100.0%	0.0%	40% -		+++-+		+-++	₩	+	+++	+-H		40.0%
1/4"	6.30		98%	100.0%	0.0%		<u> </u>				111					1
#4	4.75	97%	97%	100.0%	0.0%		[				111					1 1
#8	2.36		89%	100.0%	0.0%	30% -					111		m			30.0%
#10	2.00	88%	88%	100.0%	0.0%						1					
#16	1.18		65%	100.0%	0.0%	20% -						<b>\</b>	Ш			20.0%
#20	0.850		55%	100.0%	0.0%							<b>N</b> III				1
#30	0.600		48%	100.0%	0.0%		t I IIII									
#40	0.425	43%	43%	100.0%	0.0%	10% -		+++-+	++++	+-+++++++++++++++++++++++++++++++++++	+++		+++	+		10.0%
#50	0.300		31%	100.0%	0.0%		F									1
#60	0.250		26%	100.0%	0.0%						III I.					1
#80	0.180		19%	100.0%	0.0%	0%	100.000	10.0	00	1.000	0-0-00	0.100		0.010		0.0%
#100	0.150	16%	16%	100.0%	0.0%											
#140	0.106		11%	100.0%	0.0%				Particle Size	(mm)						
#170	0.090		9%	100.0%	0.0%											
#200	0.075	6.7%	6.7%	100.0%	0.0%	+ Sieve Si	izes •	—▲ — Max S	pecs	_	— Min	Specs	_	Si	ieve Results	
Copyright	Spears Engineering & Tec	hnical Services PS, 1996-98	3		1	_										

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-1959
Sample Date:	7/16/2021
Test Date:	10/5/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT23-GB-8.5-17.6 ft

 Visual Soil Description:
 grayish-brown sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

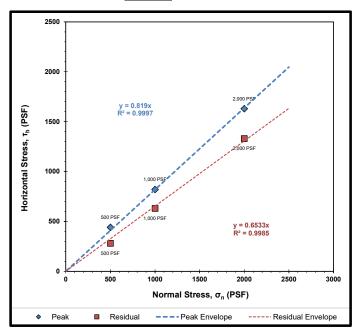
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF			
Initial Moisture Content (%):	22.6				
	Initial	Post-Consolidation			
Dry Density (PCF):	109.4	111.1			
Void Ratio:	0.539	0.517			
Porosity (%):	35.0	34.1			
Degree of Saturation (%):	saturated	saturated			

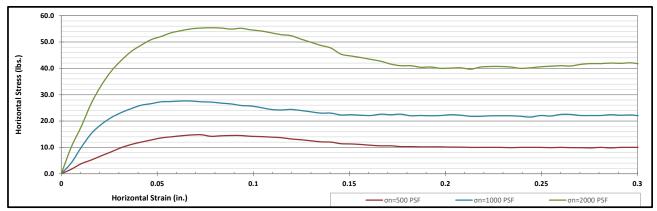
Summary of Samp	le Data:	σ <sub>n</sub> =1000 PSF			
Initial Moisture Content (%):	22.2				
	Initial	Post-Consolidation			
Dry Density (PCF):	110.1	111.8			
Void Ratio:	0.531	0.507			
Porosity (%):	34.7	33.7			
Degree of Saturation (%):	saturated	saturated			

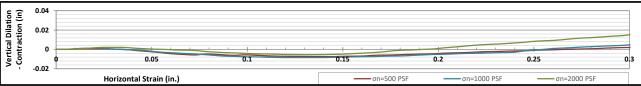
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	23.3	
	Initial	Post-Consolidation
Dry Density (PCF):	109.0	114.1
Void Ratio:	0.545	0.476
Porosity (%):	35.3	32.3
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS								
	PEAK	RESIDUAL						
Angle of Internal Friction, φ (°):	39	33						
Cohesion (PSF):	0	0						



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	440	820	1630				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	280	630	1330				





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT23-GB-17.6-18.5 ft Sample#: B21-1960

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21 Tested By: K. Mendez Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: grayish-brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

#140

#170

#200

0.106

0.090

0.075

Sample Meets Specs? N/A

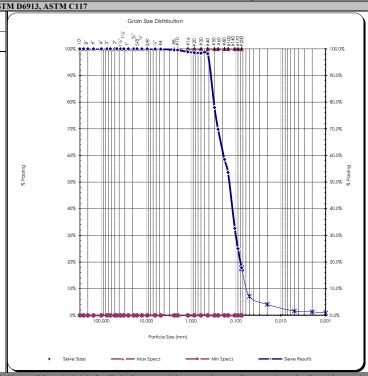
 $D_{(5)} = 0.028$   $D_{(10)} = 0.059$   $D_{(15)} = 0.069$   $D_{(30)} = 0.100$ % Gravel = 0.1% % Sand = 82.0% mm % Silt & Clay = 17.9% mm Liquid Limit = n/a mm  $D_{(50)} = 0.142$ mm Plasticity Index = n/a  $D_{(60)} = 0.189$ mm  $D_{(90)} = 0.374$ Dust Ratio = 2/11 mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Coeff. of Curvature,  $C_C = 0.90$ Coeff. of Uniformity,  $C_U = 3.20$ Fineness Modulus = 0.72

Plastic Limit = n/a Moisture %, as sampled = 36.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136, AST
		Actual	Interpolated		
		Cumulative	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		99%	100.0%	0.0%
#20	0.850		99%	100.0%	0.0%
#30	0.600		98%	100.0%	0.0%
#40	0.425	98%	98%	100.0%	0.0%
#50	0.300		78%	100.0%	0.0%
#60	0.250		70%	100.0%	0.0%
#80	0.180		59%	100.0%	0.0%
#100	0.150	54%	54%	100.0%	0.0%



0.0%

0.0%

0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

17.9%

33%

25%

17.9%

100.0%

100.0%

100.0%



### **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SM, Silty Sand Client: Anchor QEA Date Tested: 4-Oct-21 Sample Color Source: LDW21-GT23-GB-17.6-18.5 ft Tested By: K. Mendez grayish-brown Sample#: B21-1960 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 75.28 **Grain Size Distribution** Hydroscopic Moist.: Soils Particle 1.16% Sieve Percent ACCREDITED Adj. Sample Wgt: 74.42 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0537 mm 100% 25.000 mm 7.4% 1.0" 6.0% 3/4" 100% 19.000 mm 2 4.5 0.0381 mm 3.5 4.7%  $0.0243 \ mm$ 5/8" 100% 16.000 mm 15 2.5 3.3%  $0.0141 \ mm$ 1/2" 100% 12.500 mm 30 2 2.7% 0.0100 mm 3/8" 100% 9.500 mm 0.0071 mm 60 1.5 2.0% 1/4" 100% 6.300 mm 240 1.3% 0.0035 mm 100% 4.750 mm #4 #10 100%  $2.000\ mm$ 1440 1.3%  $0.0014\ mm$ #20 99% 0.850 mm Liquid Limit: n/a % Gravel: #40 98%  $0.425 \, mm$ % Sand: 82.0% Plastic Limit: n/a #100 54% 0.150 mm % Silt: 16.3% Plasticity Index: n/a #200 17.9%  $0.075 \ mm$ 17.4% 0.074 mm % Clay: 1.6% Silts 7.2% 0.050 mm 0.020 mm 4.1% 1.6% 0.005 mm Clays 1.3%  $0.002\ mm$ Colloids 0.9% $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by:

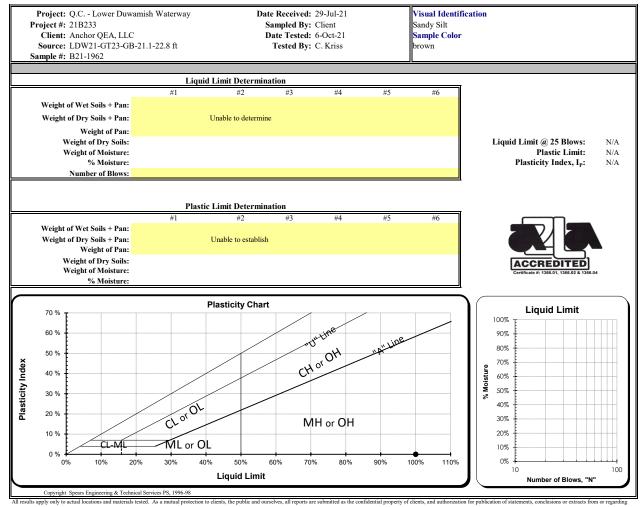
Meghan Blodgett-Carrillo

### Materials Testing & Consulting, Inc.



Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting

#### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



our reports is reserved pending our written approval.

Comments: Liquid limit cannot be determined as the material displays rapid dilation. At lower moistures the sample does not spread into the cup without tearing the soil cake. Unable to establish plastic limit as the material does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

Meghan Blodgett-Carrillo

Visit our website: www.mtc-inc.net



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT23-GB-22.8-26.8 ft Sample#: B21-1963

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 4-Oct-21 Tested By: K. Mendez Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

#140

#170

#200

0.106

0.090

0.075

Meghan Blodgett-Carrillo

Sample Meets Specs? N/A

 $D_{(5)} = 0.011$   $D_{(10)} = 0.053$   $D_{(15)} = 0.063$   $D_{(30)} = 0.090$   $D_{(50)} = 0.126$ % Gravel = 0.0%% Sand = 78.3% mm % Silt & Clay = 21.7% mm Liquid Limit = n/a mm mm Plasticity Index = n/a  $D_{(60)} = 0.143$ mm

Sand Equivalent = n/a 1 Face = n/aFaces = n/a Coeff. of Curvature,  $C_C = 1.05$ Coeff. of Uniformity,  $C_U = 2.69$ Fineness Modulus = 0.54

Plastic Limit = n/a Moisture %, as sampled = 32.1% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.353$	mm		Fracture	e %,	1
					D	ust Ratio = 7/32		Fr	acture 9	<b>%</b> , 2-	+ I
				AS	TM C136, AS	TM D6913, ASTN	1 C117				
		Actual	Interpolated						Grain Siz	ze Dis	strik
		_	Cumulative		1						
	Size	Percent	Percent	Specs	Specs			# in N 3	5/8%	e :, ,	+
US	Metric	Passing	Passing	Max	Min	_	100%	-	بمقيمة	m	-
12.00"	300.00		100%	100.0%	0.0%						
10.00"	250.00		100%	100.0%	0.0%						
8.00"	200.00		100%	100.0%	0.0%		90%	-111111		m	T
6.00"	150.00		100%	100.0%	0.0%						
4.00"	100.00		100%	100.0%	0.0%		80%				L
3.00"	75.00		100%	100.0%	0.0%		00,0				
2.50"	63.00		100%	100.0%	0.0%		-				
2.00"	50.00	100%	100%	100.0%	0.0%		70%		4-4		+
1.75"	45.00		100%	100.0%	0.0%						
1.50"	37.50		100%	100.0%	0.0%						
1.25"	31.50		100%	100.0%	0.0%		60%		+	HH	t
1.00"	25.00	100%	100%	100.0%	0.0%	D L	ł I				
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				L
5/8"	16.00		100%	100.0%	0.0%	96	30%				Т
1/2"	12.50	100%	100%	100.0%	0.0%						
3/8"	9.50	100%	100%	100.0%	0.0%		40%		44	Ш	4
1/4"	6.30		100%	100.0%	0.0%						
#4	4.75	100%	100%	100.0%	0.0%						
#8	2.36		100%	100.0%	0.0%		30%		1-1	HH	+
#10	2.00	100%	100%	100.0%	0.0%		ł I				
#16	1.18		100%	100.0%	0.0%		20%				L
#20	0.850		99%	100.0%	0.0%		20%				T
#30	0.600		99%	100.0%	0.0%						
#40	0.425	99%	99%	100.0%	0.0%		10%		4-4	-	4
#50	0.300		83%	100.0%	0.0%						
#60	0.250		77%	100.0%	0.0%						
#80	0.180		68%	100.0%	0.0%		0%	00,000	10.0	100	<u> </u>
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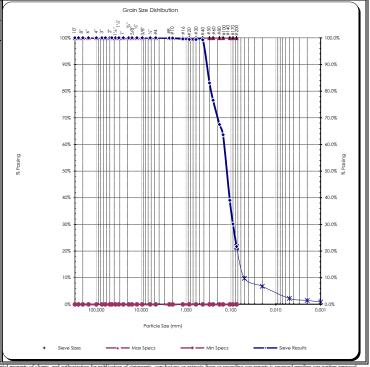
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### **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 4-Oct-21 Sample Color Source: LDW21-GT23-GB-22.8-26.8 ft Tested By: K. Mendez brown Sample#: B21-1963 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 76.06 **Grain Size Distribution** 1.08% Soils Particle Hydroscopic Moist .: Sieve Percent ACCREDITED Adj. Sample Wgt: 75.25 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0532 mm 10.0% 100% 25.000 mm 1.0" 8.6% 3/4" 100% 19.000 mm 2 6.5 0.0378 mm 5.5 7.3%  $0.0240 \ mm$ 5/8" 100% 16.000 mm 15 6.0% 0.0139 mm 1/2" 100% 12.500 mm 30 4.6% 0.0099 mm 3/8" 100% 9.500 mm 60 2.7% 0.0070 mm 1/4" 100% 6.300 mm 240 1.5 2.0% 0.0035 mm 100% 4.750 mm #4 1.3% #10 100%  $2.000\ mm$ 1440  $0.0014\ mm$ #20 99% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 99%  $0.425 \, mm$ % Sand: 78.3% Plastic Limit: n/a #100 64% 0.150 mm % Silt: 19.5% Plasticity Index: n/a #200 21.7%  $0.075 \ mm$ 21.2% 0.074 mm % Clay: 2.3% Silts 9.8% 0.050 mm 0.020 mm 6.8% 2.3% 0.005 mm Clays 1.5%  $0.002\ mm$ Colloids 0.9% $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** Reviewed by:

Meghan Blodgett-Carrillo



Client:	Anchor QEA	Date:	October 19, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-2050-2069
Revised on:		Date sampled:	8-4-21 & 8-5-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor	Trease see Tituenea Reports		Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	<del></del>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 8, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-2050	LDW21-GT44-GB-0-5 ft	341.8	1294.0	1086.4	207.6	744.6	27.9%
B21-2051	LDW21-GT44-GB-5-6.1 ft	354.2	977.3	871.3	106.0	517.1	20.5%
B21-2052	LDW21-GT44-GB-6.1-6.5 ft	359.6	665.7	593.5	72.2	233.9	30.9%
B21-2053	LDW21-GT44-GB-5-10 ft	357.1	1289.6	1063.4	226.2	706.3	32.0%
B21-2054	LDW21-GT44-GB-10-11.5 ft	360.2	1379.9	1209.6	170.3	849.4	20.0%
B21-2055	LDW21-GT44-GB-10-15 ft	346.4	1230.1	1027.5	202.6	681.1	29.7%
B21-2056	LDW21-GT44-GB-15.5-16.5 ft	225.1	974.7	803.8	170.9	578.7	29.5%
B21-2057	LDW21-GT44-GB-15-20 ft	266.4	1004.4	805.9	198.5	539.5	36.8%
B21-2058	LDW21-GT44-GB-20-21.5 ft	301.2	1328.5	1051.3	277.2	750.1	37.0%
B21-2059	LDW21-GT44-GB-20-25 ft	224.4	1222.2	950.5	271.7	726.1	37.4%
B21-2060	LDW21-GT44-GB-25-28.7 ft	270.1	1116.1	1011.0	105.1	740.9	14.2%
B21-2061	LDW21-GT44-GB-28.7-30 ft	182.4	916.9	718.4	198.5	536.0	37.0%
B21-2062	LDW21-GT44-GB-30-31.5 ft	220.5	1200.8	943.4	257.4	722.9	35.6%
B21-2063	LDW21-GT48-GB-0-5 ft	234.7	1032.0	887.3	144.7	652.6	22.2%
B21-2064	LDW21-GT48-GB-5-6.5 ft	221.5	1216.7	1036.8	179.9	815.3	22.1%
B21-2065	LDW21-GT48-GB-5-10 ft	233.9	698.1	566.7	131.4	332.8	39.5%
B21-2066	LDW21-GT48-GB-10-15 ft	233.2	798.5	665.7	132.8	432.5	30.7%
B21-2067	LDW21-GT48-GB-15-18.2 ft	224.4	960.1	827.8	132.3	603.4	21.9%
B21-2068	LDW21-GT48-GB-18.2-19.5 ft	221.9	948.5	777.2	171.3	555.3	30.8%
B21-2069	LDW21-GT48-GB-20-21.6 ft	306.7	947.8	795.3	152.5	488.6	31.2%
			Ī	1	1		

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



## **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: September 20, 2021	Tested by: A. Eifrig
Date 1 cs. d. September 20, 2021	rested by. A. Lillig

Sample #	Location	Tare	Tare	Mass of Dry Soil	Pycno ID		Pycno	Density of Water @ Tx	soils	Mass of Pycno filled w/ water	Water, 0.1 *C	SpG of Soils	Factor	SpG
B21-2055	LDW21-GT44-GB-10-15 ft	497.91	595.93	98.0	TSA-017	187.9	499.4	0.99858	747.34	686.58	18.1	2.630647		2.6316204
B21-2066	LDW21-GT48-GB-10-15 ft	510.08	607.93	97.9	TSA-011	190.3	499.5	0.99856	749.61	689.15	18.2	2.6169635	1.00035	2.6178795
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT44-GB-0-5 ft Sample#: B21-2050

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SW-SC, Well-graded Sand with Silty Clay

Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.039 \\ D_{(10)} = 0.039 \\ D_{(10)} = 0.083 \\ D_{(15)} = 0.170 \\ D_{(30)} = 0.352 \\ D_{(50)} = 0.593 \\ D_{(60)} = 0.724 \\ D_{(90)} = 1.967 \\ Dust Ratio = 9/35 \\ \end{array}$ % Gravel = 4.2% % Sand = 86.2% mm % Silt & Clay = 9.6% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 2.07$ Coeff. of Uniformity,  $C_U = 8.74$ Fineness Modulus = 2.51 Plastic Limit = n/a Moisture %, as sampled = 27.9%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

Du	ist Katio –	7/33	Fracture 70, 2   Faces = 11/a	Requiriacture 70, 2+ races =
M C136, AST	M D6913,	ASTM C117		
			Grain Size Distribution	
	II		§ .	

				AS	TM C136, AS	TM D6913, ASTM C117
			Interpolated			Grain Size Distribution
		Cumulative	Cumulative			-
Sieve	Size	Percent	Percent	Specs	Specs	10° 10° 10° 10° 10° 10° 10° 10° 10° 10°
US	Metric	Passing	Passing	Max	Min	100% ***********************************
12.00"	300.00		100%	100.0%	0.0%	
10.00"	250.00		100%	100.0%	0.0%	
8.00"	200.00		100%	100.0%	0.0%	90%
6.00"	150.00		100%	100.0%	0.0%	
4.00"	100.00		100%	100.0%	0.0%	80%
3.00"	75.00		100%	100.0%	0.0%	00%
2.50"	63.00		100%	100.0%	0.0%	
2.00"	50.00	100%	100%	100.0%	0.0%	70%
1.75"	45.00		100%	100.0%	0.0%	
1.50"	37.50		100%	100.0%	0.0%	
1.25"	31.50		99%	100.0%	0.0%	60.0%
1.00"	25.00	99%	99%	100.0%	0.0%	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
3/4"	19.00	99%	99%	100.0%	0.0%	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
5/8"	16.00		99%	100.0%	0.0%	8 30% 8
1/2"	12.50	98%	98%	100.0%	0.0%	
3/8"	9.50	98%	98%	100.0%	0.0%	40.0%
1/4"	6.30		96%	100.0%	0.0%	
#4	4.75	96%	96%	100.0%	0.0%	
#8	2.36		91%	100.0%	0.0%	30%
#10	2.00	91%	91%	100.0%	0.0%	
#16	1.18		76%	100.0%	0.0%	20.0%
#20	0.850	70%	70%	100.0%	0.0%	20,0
#30	0.600		51%	100.0%	0.0%	
#40	0.425	37%	37%	100.0%	0.0%	10%
#50	0.300		25%	100.0%	0.0%	
#60	0.250	20%	20%	100.0%	0.0%	
#80	0.180		16%	100.0%	0.0%	0% 00000 10,000 1,000 0,100 0,010 0,001
#100	0.150	14%	14%	100.0%	0.0%	
#140	0.106		11%	100.0%	0.0%	Particle Size (mm)
#170	0.090		10%	100.0%	0.0%	
#200	0.075	9.6%	9.6%	100.0%	0.0%	+ Sieve Sizes — Max Specs — Min Specs — Sieve Results
Copyright	Spears Engineering & Tec	hnical Services PS, 1996-9	3			

Comments:			
	$\Omega$ $U$		

## **Direct Shear Test Results:**

#### ASTM D-3080



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2050
Sample Date:	8/4/2021
Test Date:	10/13/2021
Technician:	M. Carrillo

Sample Source: LDW21-GT44-GB-0-5 ft
Visual Soil Description: brown silty sand with gravel
Type of Specimen: Remolded Cylindrical Shear Box
Specimen Diameter (in): 2.5

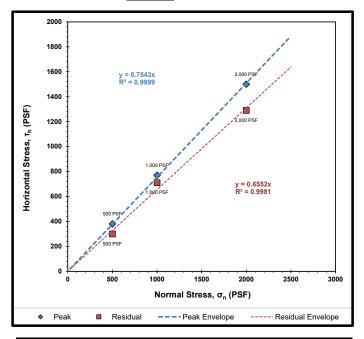
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Samp	σ <sub>n</sub> =500 PSF	
Initial Moisture Content (%):	24.6	
	Initial	Post-Consolidation
Dry Density (PCF):	109.7	110.8
Void Ratio:	0.536	0.520
Porosity (%):	34.9	34.2
Degree of Saturation (%):	saturated	saturated

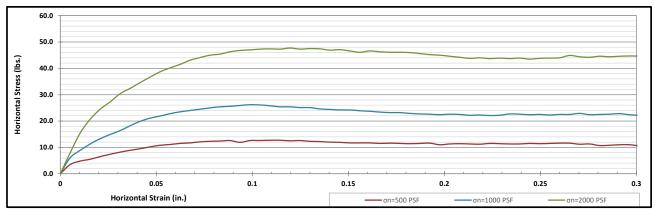
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	23.8	
	Initial	Post-Consolidation
Dry Density (PCF):	110.7	113.4
Void Ratio:	0.523	0.486
Porosity (%):	34.3	32.7
Degree of Saturation (%):	saturated	saturated

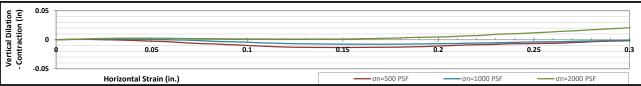
Summary of Sample	σ <sub>n</sub> =2000 PSF	
Initial Moisture Content (%):	23.8	
	Initial	Post-Consolidation
Dry Density (PCF):	110.9	114.3
Void Ratio:	0.520	0.473
Porosity (%):	34.2	32.1
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS					
	PEAK	RESIDUAL			
Angle of Internal Friction, φ (°):	37	33			
Cohesion (PSF):	0	0			



Failure Envelope Test Values:						
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000			
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	380	770	1500			
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	300	710	1290			





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT44-GB-5-10 ft Sample#: B21-2053

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: dark brown



Coeff. of Curvature,  $C_C = 1.14$ Coeff. of Uniformity,  $C_U = 2.85$ Fineness Modulus = 0.59

## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASINID43} \\ \textbf{D}_{(5)} = 0.031 \\ \textbf{D}_{(10)} = 0.062 \\ \textbf{D}_{(15)} = 0.081 \\ \textbf{D}_{(30)} = 0.112 \\ \textbf{D}_{(50)} = 0.154 \\ \textbf{D}_{(60)} = 0.178 \\ \textbf{D}_{(90)} = 0.247 \\ \textbf{$ % Gravel = 0.0%% Sand = 88.0% mm % Silt & Clay = 12.0% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Plastic Limit = n/a Moisture %, as sampled = 32.0% Req'd Sand Equivalent = Fracture %, 1 Face = n/aReq'd Fracture %, 1 Face =

Dust Ratio = 9/74	Fracture %, 2+ Faces = n/a	Req'd Fracture %, 2+ Fac
I C136, ASTM D6913, ASTM C117		

						ıst Ratio =			Fractu	ire %, 2+	Faces =	n/a		Req'd	Fractur	e %, 2-	Faces	=
				AS	TM C136, AST	M D6913,	ASTM C11	7										
		Actual	Interpolated						Gr	ain Size Distri	hution							
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1.75"	45.00		100%	100.0%	0.0%		1										1 1	
1.50"	37.50		100%	100.0%	0.0%												1 1	
1.25"	31.50		100%	100.0%	0.0%		60%					*****	i	******			+++++6	50.0%
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5/8"	16.00		100%	100.0%	0.0%	86	30% F										T	10.0% 86
1/2"	12.50	100%	100%	100.0%	0.0%								- 1 1				1 1	
3/8"	9.50	100%	100%	100.0%	0.0%		40%						-			$\blacksquare \blacksquare \blacksquare$	4	10.0%
1/4"	6.30		100%	100.0%	0.0%		1						11				1 1	
#4	4.75	100%	100%	100.0%	0.0%		1						1 1				1 1	
#8	2.36		100%	100.0%	0.0%		30%					******		ШШ			<del>     </del> 3	30.0%
#10	2.00	100%	100%	100.0%	0.0%		ŀ						i				1 1	
#16	1.18		100%	100.0%	0.0%		20%										⊥i,	20.0%
#20	0.850	100%	100%	100.0%	0.0%		20,0										1 1	.0.0,0
#30	0.600		99%	100.0%	0.0%		-							Ĭ.			1 1	
#40	0.425	99%	99%	100.0%	0.0%		10%		++++		++-		-	<del>"</del>		++++	+++1	10.0%
#50	0.300		93%	100.0%	0.0%		-										1 1	
#60	0.250	91%	91%	100.0%	0.0%												1 1	
#80	0.180		61%	100.0%	0.0%		0%	100.00		10.000	1.00	0	0.10	0	0.01	0	0.001	0.0%
#100	0.150	48%	48%	100.0%	0.0%													
#140	0.106		27%	100.0%	0.0%					Particle:	Size (mm)							
#170	0.090		19%	100.0%	0.0%													
#200	0.075	12.0%	12.0%	100.0%	0.0%		+ Sieve Size	es es		• Max Specs	_	<b>—</b> мі	in Specs	-		Sieve Resu	lts	
Copyright	Spears Engineering & Tec	chnical Services PS, 1996-9	8															



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT44-GB-10-15 ft Sample#: B21-2055

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color: dark brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D431} \\ \textbf{D}_{(5)} = 0.032 \\ \textbf{D}_{(10)} = 0.064 \\ \textbf{D}_{(15)} = 0.082 \\ \textbf{D}_{(30)} = 0.116 \\ \textbf{D}_{(50)} = 0.164 \\ \textbf{D}_{(60)} = 0.192 \\ \textbf{D}_{(90)} = 0.404 \\ \end{array}$ % Gravel = 0.0%% Sand = 88.2% mm % Silt & Clay = 11.8% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 1.11$ Coeff. of Uniformity,  $C_U = 3.02$ Fineness Modulus = 0.77 Plastic Limit = n/a

Moisture %, as sampled = 29.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

					Di	$D_{(90)} = 0.404$ ust Ratio = 11/85	mm		Fracture	ire %, 1		n/a		R				%, 1 Fa 2+ Fa	
				AS		FM D6913, ASTM	C117			, _							,		
		Actual Cumulative	Interpolated Cumulative							Size Distri	bution								
	Size	Percent	Percent	Specs	Specs		ь.	\$ 4 B S		3/8.	8 <sup>#</sup> 8 19 19	888	888	8558					
US	Metric	Passing	Passing	Max	Min	10	00%		*****	1000	<del>_</del> **-*		444	****	ПТ	T	шт		100.0%
12.00"	300.00		100%	100.0%	0.0%							N							1
10.00"	250.00		100%	100.0%	0.0%							\\							1
8.00"	200.00		100%	100.0%	0.0%	1	0%				<u> </u>	mm'	1		###		*****		90.0%
6.00"	150.00		100%	100.0%	0.0%								V.						1
4.00"	100.00		100%	100.0%	0.0%		80%					ШШ	I N.	Щ	ШШ		ШШ		80.0%
3.00"	75.00		100%	100.0%	0.0%		1												1
2.50"	63.00		100%	100.0%	0.0%														1
2.00"	50.00	100%	100%	100.0%	0.0%		70%					₩₩	$\mathbf{H}$		++++	-	++++		70.0%
1.75"	45.00		100%	100.0%	0.0%														1
1.50"	37.50		100%	100.0%	0.0%														1
1.25"	31.50		100%	100.0%	0.0%	•	50%				<del>                                     </del>	###			++++		*****		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	D C							1						50.0%
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%								ШШ				50.0%
5/8"	16.00		100%	100.0%	0.0%	96													30.0%
1/2"	12.50	100%	100%	100.0%	0.0%														1
3/8"	9.50	100%	100%	100.0%	0.0%		10%				<b></b>			1	++++				40.0%
1/4"	6.30		100%	100.0%	0.0%									1					1
#4	4.75	100%	100%	100.0%	0.0%									1					1
#8	2.36		100%	100.0%	0.0%	;	30%				++-	₩₩		1##	++++		-		30.0%
#10	2.00	100%	100%	100.0%	0.0%		H							•					1
#16	1.18		100%	100.0%	0.0%		20%							N					20.0%
#20	0.850	100%	100%	100.0%	0.0%	•	10% F								mi				20.0%
#30	0.600		95%	100.0%	0.0%									N.					1
#40	0.425	91%	91%	100.0%	0.0%		10%	$-\!$	HH-			₩₩	##		$\mathbb{H}$	-	ШН		10.0%
#50	0.300		84%	100.0%	0.0%														1
#60	0.250	81%	81%	100.0%	0.0%														1
#80	0.180		56%	100.0%	0.0%		0%	100,000	10000-00	0.000	<del>- 00 - 0</del>	000	-00-0	0.100		0.0	10		0.0%
#100	0.150	45%	45%	100.0%	0.0%			. 50.000			1.0			3.100		5.0			
#140	0.106		25%	100.0%	0.0%					Particle:	Size (mm)								
#170	0.090		18%	100.0%	0.0%														
#200	0.075	11.8%	11.8%	100.0%	0.0%	+ Sie	ve Sizes	-	м	ax Specs	_	<b>_</b>	Min Spe	ecs.	_		Sieve F	esults.	
	Spears Engineering & Tec	,	Į.		*****					•									



Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

**Source:** LDW21-GT44-GB-15-20 ft **Sample#:** B21-2057

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21 Tested By: A. Eifrig Visual Identification Sandy Silt Sample Color:

dark brown

ACCREDITED
Certificate #: 1366.0

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

Sample Meets Specs? N/A

Sand Equivalent = n/a
Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.50$ Coeff. of Uniformity,  $C_U = 6.00$ Fineness Modulus = 0.29

Plastic Limit = n/a Moisture %, as sampled = 36.8% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						2(00)		
						$D_{(90)} = 0$		
						ust Ratio = 4		_
			T	AS	TM C136, AS	TM D6913, A	STM C117	
		Actual	Interpolated					
			Cumulative		T			
Sieve		Percent	Percent	Specs	Specs		io in	50
US	Metric	Passing	Passing	Max	Min	_	100%	
12.00"	300.00		100%	100.0%	0.0%			
10.00"	250.00		100%	100.0%	0.0%			
8.00"	200.00		100%	100.0%	0.0%		90%	
6.00"	150.00		100%	100.0%	0.0%		11	
4.00"	100.00		100%	100.0%	0.0%		80%	
3.00"	75.00		100%	100.0%	0.0%		00%	
2.50"	63.00		100%	100.0%	0.0%			
2.00"	50.00	100%	100%	100.0%	0.0%		70%	
1.75"	45.00		100%	100.0%	0.0%			
1.50"	37.50		100%	100.0%	0.0%			
1.25"	31.50		100%	100.0%	0.0%		60%	
1.00"	25.00	100%	100%	100.0%	0.0%	2	ł l	
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50%	
5/8"	16.00		100%	100.0%	0.0%	96	30%	
1/2"	12.50	100%	100%	100.0%	0.0%			
3/8"	9.50	99%	99%	100.0%	0.0%		40%	
1/4"	6.30		99%	100.0%	0.0%		1 1	
#4	4.75	99%	99%	100.0%	0.0%		1 1	
#8	2.36		99%	100.0%	0.0%		30%	
#10	2.00	99%	99%	100.0%	0.0%		ł I	
#16	1.18		99%	100.0%	0.0%		20%	
#20	0.850	98%	98%	100.0%	0.0%		20%	
#30	0.600		98%	100.0%	0.0%			
#40	0.425	98%	98%	100.0%	0.0%		10%	
#50	0.300		95%	100.0%	0.0%		11	

94%

85%

81%

70%

66%

62.6%

94%

62.6%

100.0%

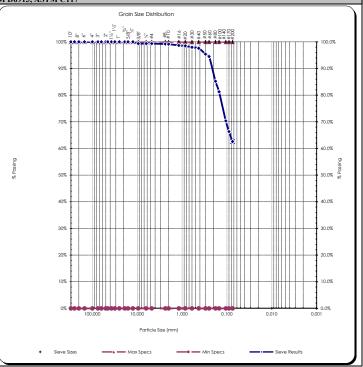
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Comments:			
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Meghan Blodgett-Carrillo

0.250

0.180

0.150

0.106

0.090

0.075

#60

#80

#100

#140

#170

#200



**Project:** Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

#16

#20

#30

#40

#50

#60

#80 #100

#140

#170

#200

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

92%

78.5%

**Source:** LDW21-GT44-GB-20-25 ft **Sample#:** B21-2059

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21 Tested By: A. Eifrig Visual Identification Sandy Silt with Clay Sample Color: brown

mm



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs ? N/A

 $D_{(90)} = 0.190$ 

Liquid Limit = n/a
Plasticity Index = n/a
Sand Equivalent = n/a
Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

% Gravel = 0.0%

% Silt & Clay = 78.5%

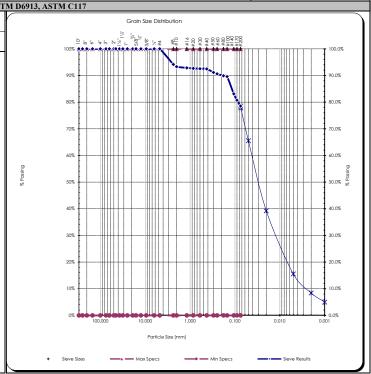
% Sand = 21.5%

Coeff. of Curvature,  $C_C = 1.61$ Coeff. of Uniformity,  $C_U = 17.87$ Fineness Modulus = 0.40

Plastic Limit = n/a Moisture %, as sampled = 37.4% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						D(90) -	0.170
						ust Ratio =	
			T	AS	STM C136, AS	ΓM D6913,	ASTM
		Actual	Interpolated				
		Cumulativ	e Cumulative				
Sieve	Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		1
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%	2	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	
5/8"	16.00		100%	100.0%	0.0%	₩.	
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		94%	100.0%	0.0%		
#10	2.00	93%	93%	100.0%	0.0%		



Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval

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Reviewed by:

| Meghan Blodgett-Carrillo

93%

93%

93%

92%

91%

91%

90%

90%

83%

81%

78.5%

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# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Project #: 21B233 Sandy Silt with Clay Sampled By: Client Client: Anchor QEA Date Tested: 8-Oct-21 Sample Color Source: LDW21-GT44-GB-20-25 ft Tested By: A. Eifrig brown Sample#: B21-2059 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp Gr: 2.65 Sieve Analysis Sample Weight: 75.15 **Grain Size Distribution** Hydroscopic Moist.: 3.83% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 72.38 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0414 mm 100% 25.000 mm 55 4% 1.0" 49.0% 0.0307 mm 3/4" 100% 19.000 mm 2 38 31 40.0%  $0.0204\ mm$ 5/8" 100% 16.000 mm 15 21 27.1%  $0.0127 \ mm$ 1/2" 100% 12.500 mm 30 23.2% 0.0091 mm 3/8" 100% 9.500 mm 60 15 19.3% 0.0065 mm 1/4" 100% 6.300 mm 240 11.6% 0.0034 mm 100% 4.750 mm #4 7.1% #10  $2.000\ mm$ 1440  $0.0014 \ mm$ 93% 5.5 #20 93%  $0.850 \ mm$ Liquid Limit: n/a % Gravel: 0.0% #40 92%  $0.425 \, mm$ % Sand: 21.5% Plastic Limit: n/a #100 90% 0.150 mm % Silt: 63.0% Plasticity Index: n/a #200 78.5%  $0.075 \ mm$ 77.8% 0.074 mm % Clay: 15.5% Silts 65.5% 0.050 mm 39.3% 0.020 mm 0.005 mm 15.5% Clays 8.4%  $0.002\ mm$ Colloids 5.0%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT44-GB-25-28.7 ft Sample#: B21-2060

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

Tested By: A. Eifrig

Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{ASIM D4318} \\ \textbf{D}_{(5)} = 0.370 \\ \textbf{D}_{(10)} = 0.495 \\ \textbf{D}_{(15)} = 0.577 \\ \textbf{D}_{(30)} = 0.822 \\ \textbf{D}_{(50)} = 1.264 \\ \textbf{D}_{(60)} = 1.490 \\ \textbf{D}_{(90)} = 14.510 \\ \textbf{Partia} = 6/23 \\ \end{array}$ % Gravel = 11.1% % Sand = 87.4% mm % Silt & Clay = 1.5% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm

SP, Poorly graded Sand

Sand Equivalent = n/a mm Fracture %, 1 Face = n/a

Unified Soils Classification System, ASTM D-2487

Coeff. of Curvature,  $C_C = 0.92$ Coeff. of Uniformity,  $C_U = 3.01$ Fineness Modulus = 3.78

Plastic Limit = n/a Moisture %, as sampled = 14.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

				AS	TM C136, AS	ust Ratio = FM D6913. A			Fracture	%, 2+	Faces:	= n/a		Req'd F	racture	%, 2+	Faces =
			Interpolated	Als	71W1 C150, A5	( D0)13, A	SIM CII7		Grain	Size Distri	bution						
		Cumulative	Cumulative							I SIZE DISIII	DOIIOIT						
Sieve	Size	Percent	Percent	Specs	Specs		b.	\$ 4 K 6	. 2 %	3/8#	m2 :	2 Q Q 2	8888	28			
US	Metric	Passing	Passing	Max	Min		= ao 100% <b></b>	<b>~\$~\$√\$~</b> \$√\$	1 = 1 S	\$ ≥ ₹ <b>4. 4.4</b>	***	= = = =	*****	# <u>`</u>			T 100.0%
12.00"	300.00		100%	100.0%	0.0%		ļ.		1								
10.00"	250.00		100%	100.0%	0.0%		į l		N								1 1
8.00"	200.00		100%	100.0%	0.0%		90%		<b>***</b>	70.00	+	₩₩	HH-				90.0%
6.00"	150.00		100%	100.0%	0.0%		-										
4.00"	100.00		100%	100.0%	0.0%												1 1
3.00"	75.00		100%	100.0%	0.0%		80%										80.0%
2.50"	63.00		100%	100.0%	0.0%		1										
2.00"	50.00	100%	100%	100.0%	0.0%		70%	Щ			111	ЩЩ			1		70.0%
1.75"	45.00		98%	100.0%	0.0%		ļ.										
1.50"	37.50		95%	100.0%	0.0%		ł l										
1.25"	31.50		93%	100.0%	0.0%		60%				+++	₩₩	HH-				60.0%
1.00"	25.00	91%	91%	100.0%	0.0%	2	-										50.0%
3/4"	19.00	91%	91%	100.0%	0.0%	% Passing	50%										
5/8"	16.00		90%	100.0%	0.0%	PG	50%										50.0%
1/2"	12.50	90%	90%	100.0%	0.0%												1 1
3/8"	9.50	90%	90%	100.0%	0.0%		40%					₩₩					40.0%
1/4"	6.30		89%	100.0%	0.0%		ļ					V					
#4	4.75	89%	89%	100.0%	0.0%		<u> </u>					Ĭ					
#8	2.36		83%	100.0%	0.0%		30%				+	<del>- 1</del> +++	<del>        -   -                          </del>				30.0%
#10	2.00	83%	83%	100.0%	0.0%		<b> </b>					N					
#16	1.18		46%	100.0%	0.0%		20%										20.0%
#20	0.850	32%	32%	100.0%	0.0%		20%										20.0%
#30	0.600		16%	100.0%	0.0%							II I					
#40	0.425	6%	6%	100.0%	0.0%		10%		HHH			1111	HH-		$+-\parallel$	##	10.0%
#50	0.300		4%	100.0%	0.0%							1111					
#60	0.250	3%	3%	100.0%	0.0%								*****				
#80	0.180		3%	100.0%	0.0%		0%	100.000	10000-00	0.000		.000		100	0.010		0.0%
#100	0.150	3%	3%	100.0%	0.0%			.00.000					0.		0.010		0.001
#140	0.106		2%	100.0%	0.0%					Particle	Size (mm)						
#170	0.090		2%	100.0%	0.0%												
#200	0.075	1.5%	1.5%	100.0%	0.0%		Sieve Sizes	_	м	ax Specs			Min Specs	_	Sie	eve Results	
Commisht	Spears Engineering & Tecl	nnical Services PS, 1996-98			1	N.											



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT44-GB-28.7-30 ft Sample#: B21-2061

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21 Tested By: A. Eifrig

Visual Identification Sandy Silt Sample Color:

brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Dust Ratio = 51/59

Specifications No Specs

19.00

16.00

12.50

9.50

6.30

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300 0.250

0.180

0.150

0.106

0.090

0.075

5/8"

1/2"

3/8"

1/4"

#4

#8

#10 #16

#20

#30

#40

#50

#60

#80 #100

#140

#170

#200

Sample Meets Specs? N/A

 $D_{(5)} = 0.005$   $D_{(10)} = 0.009$ mm  $D_{(15)} = 0.014$ mm  $D_{(30)} = 0.028$ mm  $D_{(50)} = 0.047$ mm  $D_{(60)} = 0.057$ mm  $D_{(90)} = 0.144$ mm

Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

% Gravel = 3.2%

% Silt & Clay = 79.2%

% Sand = 17.6%

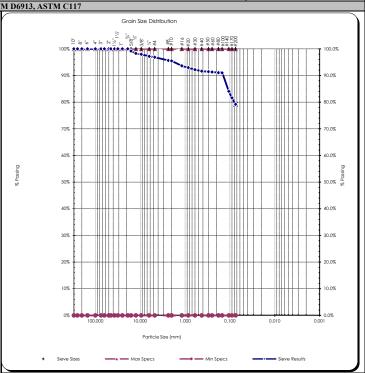
Coeff. of Curvature,  $C_C = 1.50$ Coeff. of Uniformity,  $C_U = 6.00$ Fineness Modulus = 0.41 Plastic Limit = n/a

Moisture %, as sampled = 37.0% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136, AST
		Actual Cumulativ	Interpolated Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%

Actual	Interpolated		
Cumulative	Cumulative		
Percent	Percent	Specs	Specs
Passing	Passing	Max	Min
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
100%	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
	100%	100.0%	0.0%
100%	100%	100.0%	0.0%
100%	100%	100.0%	0.0%
	99%	100.0%	0.0%
98%	98%	100.0%	0.0%
98%	98%	100.0%	0.0%
	97%	100.0%	0.0%
97%	97%	100.0%	0.0%
	96%	100.0%	0.0%
95%	95%	100.0%	0.0%
	94%	100.0%	0.0%
93%	93%	100.0%	0.0%
	92%	100.0%	0.0%
92%	92%	100.0%	0.0%
	91%	100.0%	0.0%
91%	91%	100.0%	0.0%
	91%	100.0%	0.0%
91%	91%	100.0%	0.0%
	84%	100.0%	0.0%
	82%	100.0%	0.0%



0.0%

Reviewed by: Meghan Blodgett-Carrillo

79.2%

100.0%

79.2%

## **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2065
Sample Date:	8/5/2021
Test Date:	10/15/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT48-GB-5-10 ft

 Visual Soil Description:
 brown silty sand with gravel

 Type of Specimen:
 Remolded Cylindrical Shear Box

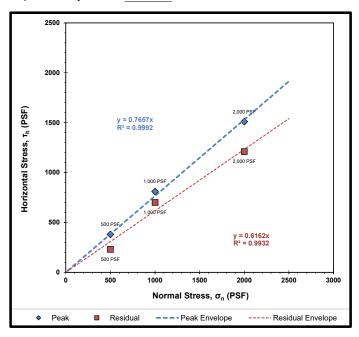
 Specimen Diameter (in):
 2.5

Summary of Samp	le Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	37.5	
	Initial	Post-Consolidation
Dry Density (PCF):	-4530.4	-4603.6
Void Ratio:	-1.037	-1.037
Porosity (%):	2789.0	2832.4
Degree of Saturation (%):	-97.6	saturated

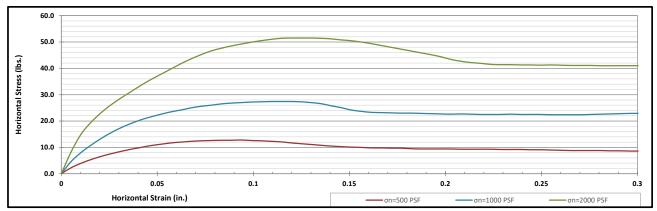
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	34.3	
	Initial	Post-Consolidation
Dry Density (PCF):	100.8	104.7
Void Ratio:	0.672	0.610
Porosity (%):	40.2	37.9
Degree of Saturation (%):	saturated	saturated

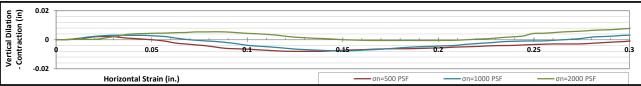
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	35.3	
	Initial	Post-Consolidation
Dry Density (PCF):	100.6	106.4
Void Ratio:	0.675	0.584
Porosity (%):	40.3	36.9
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS												
	PEAK	RESIDUAL										
Angle of Internal Friction, φ (°):	37	32										
Cohesion (PSF):	0	0										



Failure Envelope Test Values:											
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000								
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	380	810	1510								
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	230	700	1210								





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT48-GB-0-5 ft Sample#: B21-2063

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 8-Oct-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

19.00

16.00

12.50

9.50

6.30

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

3/4"

5/8"

1/2"

3/8"

1/4"

#4

#8

#10 #16

#20

#30

#40 #50

#60

#80

#100

#140

#170

#200

Sample Meets Specs? N/A

100%

100%

100%

100%

19%

 $D_{(5)} = 0.123$   $D_{(10)} = 0.234$   $D_{(15)} = 0.337$ % Gravel = 0.0%% Sand = 96.5% mm % Silt & Clay = 3.5% mm  $D_{(30)} = 0.655$ Liquid Limit = n/a mm  $D_{(50)} = 1.086$   $D_{(60)} = 1.301$   $D_{(90)} = 1.947$ mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a Dust Ratio = 7/39

Coeff. of Curvature,  $C_C = 1.41$ Coeff. of Uniformity,  $C_U = 5.55$ Fineness Modulus = 3.06

Plastic Limit = n/a Moisture %, as sampled = 22.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136, AST	ГМ D6913, ASTM C117
		Actual Cumulative	Interpolated Cumulative			Grain Size Distribution
Sieve	Size	Percent	Percent	Specs	Specs	7
US	Metric	Passing	Passing	Max	Min	1000 1125
12.00"	300.00		100%	100.0%	0.0%	1 E E HILLE HILLEN
10.00"	250.00		100%	100.0%	0.0%	<u>                                     </u>
8.00"	200.00		100%	100.0%	0.0%	90%
6.00"	150.00		100%	100.0%	0.0%	
4.00"	100.00		100%	100.0%	0.0%	80%
3.00"	75.00		100%	100.0%	0.0%	80%
2.50"	63.00		100%	100.0%	0.0%	
2.00"	50.00	100%	100%	100.0%	0.0%	70%
1.75"	45.00		100%	100.0%	0.0%	
1.50"	37.50		100%	100.0%	0.0%	
1.25"	31.50		100%	100.0%	0.0%	60%
1.00"	25.00	100%	100%	100.0%	0.0%	2

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100%

100%

100%

100%

100%

100%

93%

92%

54%

39%

27%

19%

13%

11%

7%

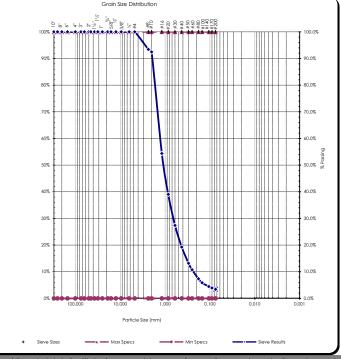
6%

4%

4%

3.5%





0.0%

0.0%

0.0%

Comments:			
•			
	M. I Balanta Ma	 	

Reviewed by: Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

Source: LDW21-GT48-GB-5-10 ft Sample#: B21-2065

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 8-Oct-21 Tested By: A. Eifrig Unified Soils Classification System, ASTM D-2487

SM, Silty Sand Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.026 \\ \textbf{D}_{(10)} = 0.051 \\ \textbf{D}_{(15)} = 0.076 \\ \textbf{D}_{(30)} = 0.102 \\ \textbf{D}_{(50)} = 0.137 \\ \textbf{D}_{(60)} = 0.171 \\ \textbf{D}_{(90)} = 0.386 \end{array}$ % Gravel = 0.7% % Sand = 84.7% mm % Silt & Clay = 14.6% mm Liquid Limit = n/a mm mm mm mm

Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Faces = n/a Coeff. of Curvature,  $C_C = 1.19$ Coeff. of Uniformity,  $C_U = 3.32$ Fineness Modulus = 0.75 Plastic Limit = n/a

Moisture %, as sampled = 39.5% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

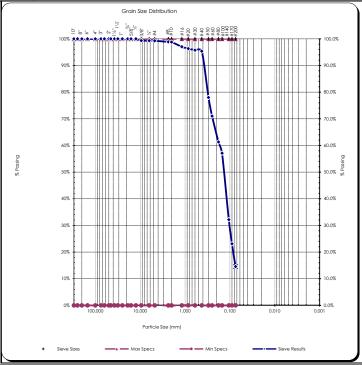
Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.386$	mm			acture		
						ust Ratio = 15/98	~		Fract	ure %	i, 2+	· Fa
			T	AS	STM C136, AS	FM D6913, ASTM	C117					
		Actual	Interpolated Cumulative			ľ			G	rain Size	e Dist	ribu
6.	G.	7		C	6	-			34			
	Size	Percent	Percent	Specs	Specs		io i <sub>60</sub> i <sub>4</sub>	o 44 % %	ر آجر <u>.</u> د آجر د		1 2 2	9
US	Metric	Passing	Passing	Max	Min	-	100%	•	• • • •		<b>-</b>	
12.00"	300.00		100%	100.0%	0.0%		ł I					
10.00"	250.00		100%	100.0%	0.0%		90%					
8.00"	200.00		100%	100.0%	0.0%		90%				Ш	П
6.00"	150.00		100%	100.0%	0.0%							
4.00"	100.00		100%	100.0%	0.0%		80%			Щ	Ш	Ш.
3.00"	75.00		100%	100.0%	0.0%		l l					
2.50"	63.00		100%	100.0%	0.0%							
2.00"	50.00	100%	100%	100.0%	0.0%		70%		+	$\vdash$	₩	₩
1.75"	45.00		100%	100.0%	0.0%							
1.50"	37.50		100%	100.0%	0.0%							
1.25"	31.50		100%	100.0%	0.0%		60%		+		###	H
1.00"	25.00	100%	100%	100.0%	0.0%	D E						
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%					Ш
5/8"	16.00		100%	100.0%	0.0%	96	30%				Ш	П
1/2"	12.50	100%	100%	100.0%	0.0%							
3/8"	9.50	99%	99%	100.0%	0.0%		40%		44	Щ	Ш	Щ.
1/4"	6.30		99%	100.0%	0.0%							
#4	4.75	99%	99%	100.0%	0.0%							
#8	2.36		99%	100.0%	0.0%		30%		++-		₩	₩
#10	2.00	99%	99%	100.0%	0.0%		-					Ш
#16	1.18		97%	100.0%	0.0%		[ ]					
#20	0.850		96%	100.0%	0.0%		20%				Ш	П
#30	0.600		96%	100.0%	0.0%							Ш
#40	0.425	95%	95%	100.0%	0.0%		10%		4		Ш	Ш
#50	0.300		78%	100.0%	0.0%							Ш
#60	0.250		71%	100.0%	0.0%		H					Ш
#80	0.180		61%	100.0%	0.0%		0%	100.000	0000	10.00	<u>ж</u>	Щ
#100	0.150	57%	57%	100.0%	0.0%			100.000		10.00	N.	
	0.150	1 2,,,,	5,7,5	100.070	0.070	П						0.

100.0%

100.0%

100.0%



0.0%

0.0%

0.0%

**Comments:** Reviewed by: Meghan Blodgett-Carrillo

14.6%

32%

23%

14.6%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#30

#40

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

Source: LDW21-GT48-GB-10-15 ft Sample#: B21-2066

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

SM, Silty Sand

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

Sample Color: dark brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs Sample Meets Specs? N/A

 $\begin{array}{c} D_{(5)} = 0.009 \\ D_{(10)} = 0.056 \\ D_{(15)} = 0.071 \\ D_{(30)} = 0.102 \\ \end{array}$ mm mm mm  $D_{(50)} = 0.141$ mm  $D_{(60)} = 0.183$ mm  $D_{(90)} = 0.369$ Dust Ratio = 8/49 mm

Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

% Gravel = 0.1%

% Silt & Clay = 16.2%

% Sand = 83.7%

Coeff. of Curvature,  $C_C = 1.02$ Coeff. of Uniformity,  $C_U = 3.29$ Fineness Modulus = 0.68 Plastic Limit = n/a

Moisture %, as sampled = 30.7% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

	,			
	11/			

_						
					AS	TM C136, AS
			Actual	Interpolated		
			Cumulative	Cumulative		
	Sieve	Size	Percent	Percent	Specs	Specs
	US	Metric	Passing	Passing	Max	Min
	12.00"	300.00		100%	100.0%	0.0%
	10.00"	250.00		100%	100.0%	0.0%
	8.00"	200.00		100%	100.0%	0.0%
	6.00"	150.00		100%	100.0%	0.0%
	4.00"	100.00		100%	100.0%	0.0%
	3.00"	75.00		100%	100.0%	0.0%
	2.50"	63.00		100%	100.0%	0.0%
	2.00"	50.00	100%	100%	100.0%	0.0%
	1.75"	45.00		100%	100.0%	0.0%
	1.50"	37.50		100%	100.0%	0.0%
	1.25"	31.50		100%	100.0%	0.0%
	1.00"	25.00	100%	100%	100.0%	0.0%
	3/4"	19.00	100%	100%	100.0%	0.0%
	5/8"	16.00		100%	100.0%	0.0%
	1/2"	12.50	100%	100%	100.0%	0.0%
	3/8"	9.50	100%	100%	100.0%	0.0%
	1/4"	6.30		100%	100.0%	0.0%
	#4	4.75	100%	100%	100.0%	0.0%
	#8	2.36		100%	100.0%	0.0%
	#10	2.00	100%	100%	100.0%	0.0%
	#16	1.18		99%	100.0%	0.0%
	#20	0.850		99%	100.0%	0.0%

99%

16.2%

99%

99%

79%

71%

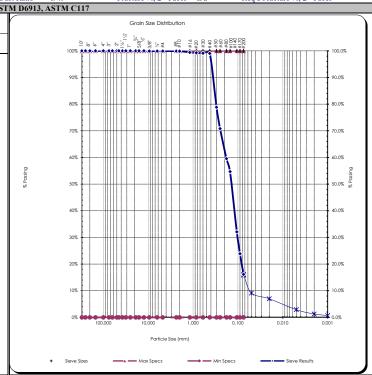
60%

55%

32%

24%

16.2%



0.0%

0.0%

0.0%

0.0%

0.0%

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0.0%

0.0%

0.0%



# **Hydrometer Report**

Project:	Q.C Lower	Duwamish Wa	terway Date Recei	ved: 29-Jul-21	<b>Unified Soils C</b>	lassification S	ystem, ASTM D-2487
Project #:	21B233		Sampled	By: Client	SM, Silty Sand		
v	Anchor QEA			sted: 8-Oct-21	Sample Color		
	-	8-GB-10-15 ft		By: A. Eifrig	dark brown		
Sample#:		0 02 10 10 11	105000	Dj. III Zillig	durit orown		
		, HYDROMI	ETER ANALYSI	S		ASTN	I D6913
Sp Gr :	2.62					Sieve A	Analysis
Sample Weight:	100.83	grams				Grain Size	Distribution
Hydroscopic Moist.:	3.02%				Sieve	Percent	Soils Particle
Adj. Sample Wgt :	97.87	grams		ACCREDITED	Size	Passing	Diameter
		_		Certificate #: 1366.01	3.0"	100%	75.000 mm
Hydrometer					2.0"	100%	50.000 mm
Reading	Corrected	Percent	Soils Particle		1.5"	100%	37.500 mm
Minutes	Reading	Passing	Diameter		1.25"	100%	31.500 mm
1	9	9.3%	0.0533 mm		1.0"	100%	25.000 mm
2	8	8.2%	0.0380 mm		3/4"	100%	19.000 mm
5	7	7.2%	0.0242 mm		5/8"	100%	16.000 mm
15	6.5	6.7%	0.0140 mm		1/2"	100%	12.500 mm
30	5.5	5.7%	0.0100 mm		3/8"	100%	9.500 mm
60	4	4.1%	0.0071 mm		1/4"	100%	6.300 mm
240	2	2.1%	0.0036 mm		#4	100%	4.750 mm
1440	1	1.0%	0.0015 mm		#10	100%	2.000 mm
					#20	99%	0.850 mm
% Gravel:	0.1%		iquid Limit: n/a		#40	99%	0.425 mm
% Sand:	83.7%		Plastic Limit: n/a		#100	55%	0.150 mm
% Silt:	13.3%	Plas	sticity Index: n/a		#200	16.2%	0.075 mm
% Clay:	2.9%				Silts	15.9%	0.074 mm
						9.1%	0.050 mm
						7.0%	0.020 mm
					Clays	2.9%	0.005 mm
						1.3%	0.002 mm
					Colloids	0.7%	0.001 mm
	USDA S	oil Textural (	Classification				
		Particle Size					
% Sand:		2.0 - 0.05 mm					
% Silt:		0.05 - 0.002 mn	1				
% Clay:		< 0.002 mm					
	HCD A C	91.00	TI 10 /1				
	USDA S	oil Textural (	lassification				
		Sanu					
			o clients, the public and ourselves,	all reports are submitted as the con	fidential property of clients, a	nd authorization for publ	ication of statements, conclusions or extracts from or
regarding our reports is reserved pen-	ding our written approv	al.					
Comments:							
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		0					
	Manda Di	deget and b					
	(1 wyn to	agen inn a					
Reviewed by:	V I						
	Meghan Blodgett	t-Carrillo					



Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

**Source:** LDW21-GT48-GB-15-18.2 ft **Sample#:** B21-2067

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP-SM, Poorly graded Sand with Silt

Sample Color: dark brown



Coeff. of Curvature,  $C_C = 0.97$ Coeff. of Uniformity,  $C_U = 3.64$ Fineness Modulus = 1.77

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs ? N/A

Liquid Limit = n/a
asticity Index = n/a
d Equivalent = n/a
are %, 1 Face = n/a

Plastic Limit = n/a
Moisture %, as sampled = 21.9%
Req'd Sand Equivalent =
Req'd Fracture %, 1 Face =

Fracture %, 1 Face = n/a Req'd Fracture %, 1 Face = racture %, 2+ Faces = n/a Req'd Fracture %, 2+ Faces =

							4/49		Fractur	e %, 2+ I	aces =	n/a		Req'd I	ractur	e %, 2-	+ Faces	=
		Actual	T . 1 . 1	AS	STM C136, AS	FM D6913, A	ASTM C11	7										
			Interpolated Cumulative			r			Grai	n Size Distrib	oution							
	a.					-			₹ .									
Sieve		Percent	Percent	Specs	Specs		ġ.	9.4.6.9	1½" 1½" 1½" 1½" 1½" 1½" 1½" 1½" 1½" 1½"	3/8,74	g2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 9 9 9	88845	3				
US	Metric	Passing	Passing	Max	Min	-1	100%			***	# + 1	+++	+ ++ ++	m	Т			100.0%
12.00"	300.00		100%	100.0%	0.0%		ł				Ĭ,						1 1	
10.00"	250.00		100%	100.0%	0.0%		90%				<b>                                   </b>						1 1.	90.0%
8.00"	200.00		100%	100.0%	0.0%		70% T							ШП			T	70.0%
6.00"	150.00		100%	100.0%	0.0%		1				l \						1 1	
4.00"	100.00		100%	100.0%	0.0%		80%					ЩЩ		Ш.				80.0%
3.00"	75.00		100%	100.0%	0.0%		ŀ				ľ	<b>\</b>					1 1	
2.50"	63.00		100%	100.0%	0.0%		ŀ					NII					1 1	
2.00"	50.00	100%	100%	100.0%	0.0%		70%					H <b>i</b> H		╫╫┼	-			70.0%
1.75"	45.00		100%	100.0%	0.0%		-										1 1	
1.50"	37.50		100%	100.0%	0.0%							1					1 1	
1.25"	31.50		100%	100.0%	0.0%		60%					<b>   </b>		####			1 1	60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0	ŀ					<b>         </b>					1 1	ing.
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%										i	50.0%
5/8"	16.00		100%	100.0%	0.0%	96	50,0					1	\				1 1	50.070 BR
1/2"	12.50	100%	100%	100.0%	0.0%		-						i II				1 1	
3/8"	9.50	100%	100%	100.0%	0.0%		40%						1					40.0%
1/4"	6.30		100%	100.0%	0.0%		1						1				1	
#4	4.75	100%	100%	100.0%	0.0%		t						1				1 1	
#8	2.36		98%	100.0%	0.0%		30%						1 1	####	-		+	30.0%
#10	2.00	98%	98%	100.0%	0.0%		ł						1				1 1	
#16	1.18		85%	100.0%	0.0%		20%						1				1 1.	20.0%
#20	0.850	80%	80%	100.0%	0.0%		20%						Ţ	mm			T	20.0%
#30	0.600		71%	100.0%	0.0%								1				1	
#40	0.425	65%	65%	100.0%	0.0%		10%									ШШ		10.0%
#50	0.300		51%	100.0%	0.0%		ŀ						1					
#60	0.250	46%	46%	100.0%	0.0%		ŀ										1 1	
#80	0.180		26%	100.0%	0.0%		0%	100,000	4000000	10.000	1,000	4000	0.100	للللو	0.010	шш	0.001	0.0%
#100	0.150	18%	18%	100.0%	0.0%			100.000		10.000	1.000	U	0.100	'	0.010	,	0.001	
#140	0.106	10/0	10%	100.0%	0.0%					Particle S	ze (mm)							
#170	0.090		8%	100.0%	0.0%													
#200	0.075	5.3%	5.3%	100.0%	0.0%		+ Sieve Size			Aax Specs		- Mi	n Specs	_		Sieve Resu	ilte	
	Spears Engineering & Tec			100.070	0.070	K	. 3/0 vo 3/20	•		nun apeca		- M	specs	_		ove vest		
				and ourselves, all reports are	1 20 1 20 61						_					_		

Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT48-GB-18.2-19.5 ft Sample#: B21-2068

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 8-Oct-21 Tested By: A. Eifrig Visual Identification

Sandy Silt Sample Color:

brown



## ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications

No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.006 \\ \textbf{D}_{(10)} = 0.011 \\ \textbf{D}_{(15)} = 0.017 \\ \textbf{D}_{(30)} = 0.033 \\ \textbf{D}_{(50)} = 0.055 \\ \textbf{D}_{(60)} = 0.066 \\ \textbf{D}_{(90)} = 0.242 \\ \end{array}$ % Gravel = 2.0%% Sand = 30.2% mm % Silt & Clay = 67.9% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 1.50$ Coeff. of Uniformity,  $C_U = 6.00$ Fineness Modulus = 0.42

Plastic Limit = n/a Moisture %, as sampled = 30.8% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face =

				AC		rust Ratio = 37/51 TM D6913, ASTN			Tractu	ne 70,	2 : Fa	ces = r	υa		Requ	l Fracti	are 70,	∠ + Γ2	ices –
		Actual Cumulative	Interpolated Cumulative	As	7 W C130, A3	TM D0913, A318				ain Size	Distributi	ion							
Sieve		Percent	Percent	Specs	Specs		io in		7 Z Z	3/8.	· 4 8	2 28	8 8 8	8888	28				
US	Metric	Passing	Passing	Max	Min		100%				1	+ ++	1	4 44 4		TT	ПППТ	П	T 100.0%
12.00"	300.00		100%	100.0%	0.0%						1	·	Ш						1
10.00"	250.00		100%	100.0%	0.0%								17						1
8.00"	200.00		100%	100.0%	0.0%		90%						m	V	*****		###		90.0%
6.00"	150.00		100%	100.0%	0.0%									N.					1
4.00"	100.00		100%	100.0%	0.0%		80%					<b>.</b>		1	ШШ		ШШ		80.0%
3.00"	75.00		100%	100.0%	0.0%		l l							١١					1
2.50"	63.00		100%	100.0%	0.0%		ŀ												1
2.00"	50.00	100%	100%	100.0%	0.0%		70%		++++			+-++	₩₩			-	╫╫┾		70.0%
1.75"	45.00		100%	100.0%	0.0%		F								r III				1
1.50"	37.50		100%	100.0%	0.0%														1
1.25"	31.50		100%	100.0%	0.0%		60%										*****		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	% Possing													1 1
3/4"	19.00	100%	100%	100.0%	0.0%	8	50%												50.0%
5/8"	16.00		100%	100.0%	0.0%	8<													1 '
1/2"	12.50	100%	100%	100.0%	0.0%		H												1
3/8"	9.50	99%	99%	100.0%	0.0%		40%		+++-	$- \mathbb{H}$		╁═╢		-					40.0%
1/4"	6.30		98%	100.0%	0.0%														1
#4	4.75	98%	98%	100.0%	0.0%		-												1
#8	2.36		97%	100.0%	0.0%		30%						mm						30.0%
#10	2.00	97%	97%	100.0%	0.0%		ļ.,												1
#16	1.18		96%	100.0%	0.0%		20%												20.0%
#20	0.850	95%	95%	100.0%	0.0%		1												1
#30	0.600		94%	100.0%	0.0%														1
#40	0.425	94%	94%	100.0%	0.0%		10%		++++	$- \mathbb{H}$		$+ \parallel$	₩₩				++++		10.0%
#50	0.300		91%	100.0%	0.0%														1
#60	0.250	91%	91%	100.0%	0.0%														1
#80	0.180		85%	100.0%	0.0%		0%	100.000	100000	10.000	-	1.000	-0-0-0	0.1	00	0.	010		0.0%
#100	0.150	82%	82%	100.0%	0.0%														
#140	0.106		74%	100.0%	0.0%					Par	ticle Size	(mm)							
#170	0.090		71%	100.0%	0.0%														
#200	0.075	67.9%	67.9%	100.0%	0.0%	+	Sieve Sizes			Max Spe	CS	_	• — мі	in Specs			Sieve I	Results	
Converight	Spears Engineering & Tec	hnical Services PS, 1996-9	8																



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#50

#60

#80 #100

#140

#170

#200

**Comments:** 

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Source: LDW21-GT48-GB-20-21.6 ft Sample#: B21-2069

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 8-Oct-21

Tested By: A. Eifrig

Unified Soils Classification System, ASTM D-2487

SP-SM, Poorly graded Sand with Silt

Sample Color: dark brown

mm



ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.057$   $D_{(10)} = 0.087$   $D_{(15)} = 0.104$   $D_{(30)} = 0.153$ mm mm mm  $D_{(50)} = 0.190$ mm  $D_{(60)} = 0.208$ mm  $D_{(90)} = 0.329$ Oust Ratio = 6/91

% Sand = 93.5% % Silt & Clay = 6.5% Liquid Limit = n/a Plasticity Index = n/a Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

% Gravel = 0.0%

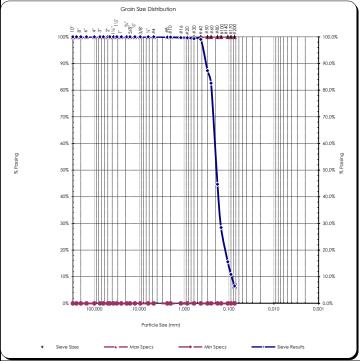
Coeff. of Curvature,  $C_C = 1.29$ Coeff. of Uniformity,  $C_U = 2.40$ Fineness Modulus = 0.85 Plastic Limit = n/a

Moisture %, as sampled = 31.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0$ .	
							6/91
		Actual	Interpolated	AS	STM C136, AST	FM D6913, A	STM C117
		Cumulative	Cumulative			_	
Sieve	Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		100%
12.00"	300.00		100%	100.0%	0.0%	1	<b>!</b>
10.00"	250.00		100%	100.0%	0.0%		11
8.00"	200.00		100%	100.0%	0.0%		90%
6.00"	150.00		100%	100.0%	0.0%		F I
4.00"	100.00		100%	100.0%	0.0%		[ ]
3.00"	75.00		100%	100.0%	0.0%		80%
2.50"	63.00		100%	100.0%	0.0%		11
2.00"	50.00	100%	100%	100.0%	0.0%		70%
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		l l
1.25"	31.50		100%	100.0%	0.0%		60%
1.00"	25.00	100%	100%	100.0%	0.0%	D <sub>O</sub>	F
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	[
5/8"	16.00		100%	100.0%	0.0%	96	50%
1/2"	12.50	100%	100%	100.0%	0.0%		<b>!</b>
3/8"	9.50	100%	100%	100.0%	0.0%		40%
1/4"	6.30		100%	100.0%	0.0%		<u> </u>
#4	4.75	100%	100%	100.0%	0.0%		1
#8	2.36		100%	100.0%	0.0%		30%
#10	2.00	100%	100%	100.0%	0.0%		
#16	1.18		100%	100.0%	0.0%		
#20	0.850	100%	100%	100.0%	0.0%		20%
#30	0.600		99%	100.0%	0.0%		
#40	0.425	99%	99%	100.0%	0.0%		10%
	25			2.2.510.70	21070	II	

83%



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Reviewed by: Meghan Blodgett-Carrillo

87%

83%

45%

28%

16%

11%

6.5%



October 19, 2021 HWA Project No. 2012-002-23 Task 51

## **Materials Testing & Consulting, Inc.**

777 Chrysler Drive Burlington, WA 98233

Attention: Ms. Meghan Blodgett-Carrillo

Subject: LABORATORY TESTING REPORT

QC - Lower Duwamish Waterway MTC Project Number: 21B233

Dear Ms. Blodgett-Carrillo;

In accordance with your request, HWA GeoSciences Inc. (HWA) performed laboratory testing for the above referenced project. Herein we present the results of our laboratory analyses, which are summarized on the attached Figures. The laboratory testing program was performed in general accordance with your instructions and appropriate ASTM Standards as outlined below.

**SAMPLE DESCRIPTION:** The subject samples were delivered to our laboratory on August 26, 2021 by MTC personnel. The samples were delivered in four Shelby tubes and were designated with exploration ID and depth of sampling. The soil samples were classified using visual-manual methods. The descriptions may be found on the attached Summary of Material Properties, Figure 1.

**MOISTURE CONTENT OF SOIL:** The moisture contents of the soil samples (percent by dry mass) were determined in general accordance with ASTM D2216. The results are shown on Figure 1.

**SPECIFIC GRAVITY OF SOILS:** The specific gravity of the selected samples was determined using method ASTM D854. The test results are shown on the attached Summary of Material Properties, Figure 1.

**LIQUID LIMIT, PLASTIC LIMIT, AND PLASTICITY INDEX OF SOILS (ATTERBERG LIMITS):** The plasticity index of each specified sample was tested using method ASTM D4318, multi-point method. The results are reported on the attached Liquid Limit, Plastic Limit, and Plasticity Index of Soils Report, Figure 2.

CONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION OF SOILS: Selected samples were tested in general accordance with method ASTM D4767 to determine the shear strength characteristics of the soil. The samples were extruded from Shelby tubes, and the test specimens were trimmed to obtain a cylindrical test sample with a length to diameter ratio between 2:1 and 2.5:1. The specimens were carefully weighed and measured prior to testing.

Three trials were run at varying confining stresses specified by the client. Each sample was run using a single specimen to perform a multi-stage shear test.

The multi-stage method was performed by first consolidating the sample at the lowest specified confining pressure. The sample was then sheared until the change in pore pressure was at or near its estimated peak. After reaching the peak change in pore pressure, the shear phase was terminated, and the specimen was reconsolidated at the middle consolidation pressure. Under the second consolidation pressure the sample was again sheared until the change in pore pressure was at or near its estimated peak, at which point the shear was terminated. The sample was reconsolidated a third and final time under the highest confining pressure and shearing was performed to sample failure, concluding the test.

For sample LDW21-GT33-GB at 6.0-8.0', the test was terminated at 20.5% strain due to a spike in pore pressure caused by a perforation in the membrane encasing the sample. As a result, the final moisture content of the sample was affected due to the ingress of water from the surrounding water filled pressure cell. The final moisture content for this sample was determined to be 70.7%.

The Consolidated Undrained test results are summarized and plotted graphically in Figures 3-6.

ONE DIMENSIONAL CONSOLIDATION PROPERTIES OF SOIL: The consolidation properties of selected soil samples were measured in general accordance with ASTM D 2435. Saturation was maintained by inundation of the sample throughout the test. The samples were subjected to increasing increments of total stress, the duration of which was selected to exceed the time required for completion of primary consolidation as defined in the Standard, Method B. Unloading of the sample was carried out incrementally. The primary compression test results are presented on the attached Consolidation Test Reports, Figures 7-10.



**CLOSURE:** Experience has shown that test values on soil and other natural materials vary with each representative sample. As such, HWA has no knowledge as to the extent and quantity of material the tested samples may represent. HWA also makes no warranty as to how representative either the samples tested or the test results obtained are to actual field conditions. It is a well-established fact that sampling methods present varying degrees of disturbance that affect sample representativeness.

No copy should be made of this report except in its entirety.

We appreciate the opportunity to provide laboratory testing services on this project. Should you have any questions or comments, or if we may be of further service, please call.

Sincerely,

HWA GEOSCIENCES INC.

Greg Barker

Materials Laboratory Supervisor

Steven E. Greene, L.G., L.E.G. Principal Engineering Geologist

Vice President

Attachments:

Figure 1

Summary of Material Properties

Figure 2

Liquid Limit, Plastic Limit and Plasticity Index of Soils

Figures 3-6

Consolidated Undrained Triaxial Compression Test for Cohesive Soils

Figures 7-10

Consolidation Test Report

		E			VITY		ATTERBERG LIMITS (%)					N O	
EXPLORATION DESIGNATION	TOP DEPTH (feet)	BOTTOM DEPT (feet)	MOISTURE CONTENT (%)	ORGANIC CONTENT (%)	SPECIFIC GRAVI	LL	PL	PI	% GRAVEL	% SAND	% FINES	ASTM SOIL CLASSIFICATION	SAMPLE DESCRIPTION
LDW21-GT23-GB,	28.5	30.5	33.3		2.617	26	25	1				SM	Dark grayish-brown, silty SAND
LDW21-GT33-GB,	6.0	8.0	58.6		2.612	38	36	2				ML	Very dark grayish-brown, SILT with sand
LDW21-GT33-GB,	21.0	23.0	35.3		2.643	31	29	2				SM	Very dark grayish-brown, silty SAND
LDW21-GT53-SPT,	30.0	32.0	43.6		2.627	38	27	11				ML	Very dark grayish-brown, SILT with sand

Notes:

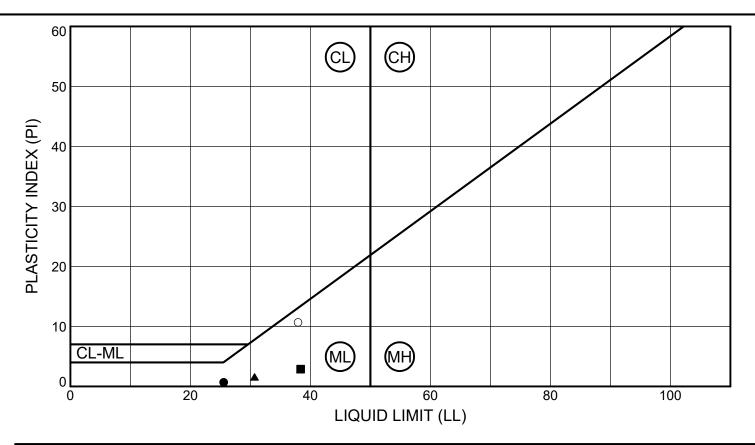
- 1. This table summarizes information presented elsewhere in the report and should be used in conjunction with the report test, other graphs and tables, and the exploration logs.
- 2. The soil classifications in this table are based on ASTM D2487 and D2488 as applicable.



MLT for MTC, Inc. QC - Lower Duwamish Waterway Client Project No.: 21B233 SUMMARY OF MATERIAL PROPERTIES

PAGE: 1 of 1

PROJECT NO.: 2012-002 T51 FIGURE: 1



SYMBOL	SAMPLE	DEPTH (ft)	CLASSIFICATION %		LL	PL	PI	% Fines
•	LDW21-GT23-GB	28.5 - 30.5	(SM) Dark grayish-brown, silty SAND	33	26	25	1	
-	LDW21-GT33-GB	6.0 - 8.0	(ML) Very dark grayish-brown, SILT with sand	59	38	36	2	
<b>A</b>	LDW21-GT33-GB	21.0 - 23.0	(SM) Very dark grayish-brown, silty SAND	35	31	29	2	
0	LDW21-GT53-SPT	30.0 - 32.0	(ML) Very dark grayish-brown, SILT with sand	44	38	27	11	

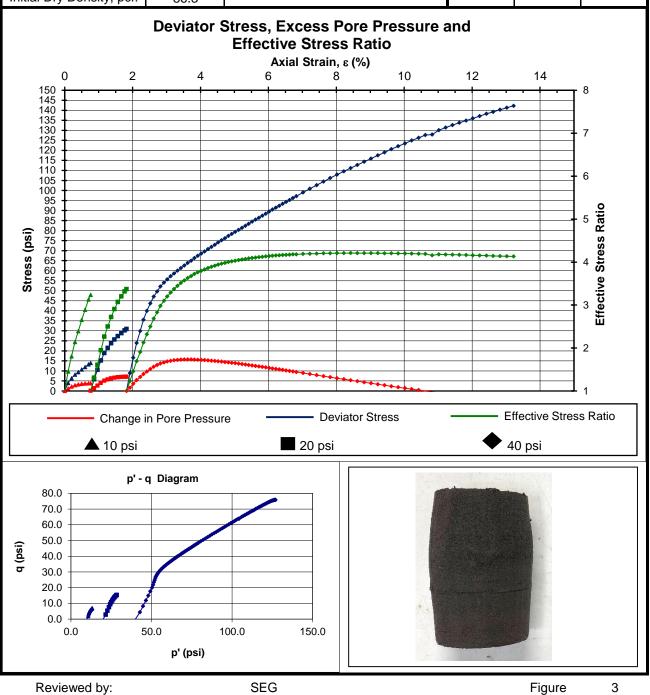


MLT for MTC, Inc. QC - Lower Duwamish Waterway Client Project No.: 21B233 LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS METHOD ASTM D4318

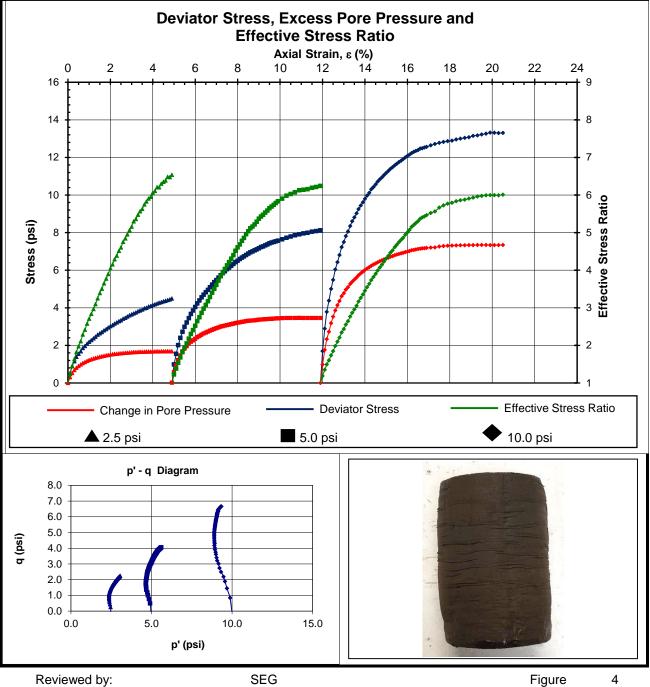
PROJECT NO.: 2012-002 T51 FIGU

FIGURE: 2

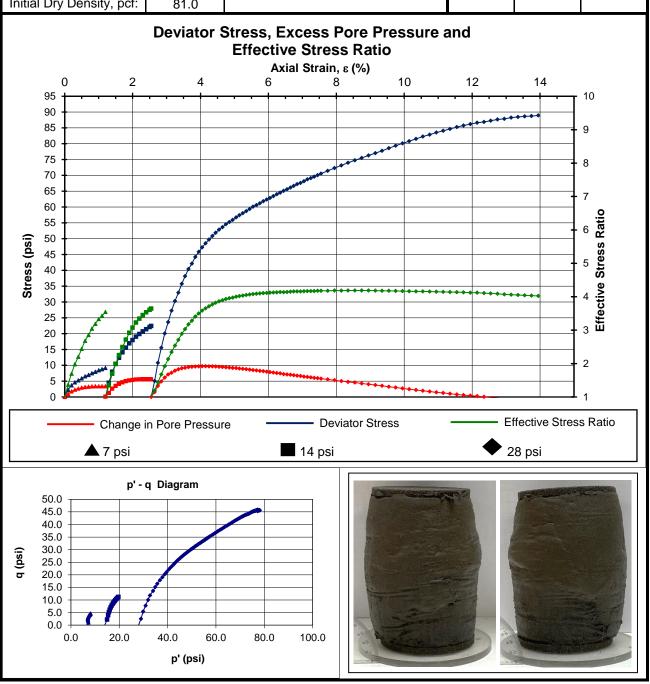
	HWA GeoSciences Inc - Materials Testing Laboratory										
Consolidated-Undrained Triaxial Compression Test for Cohesive Soils (ASTM D 4767)											
Project Name:	L	ower Duwam	ish Waterway		Date:	8/27	/2021				
Project No.:	2012-00	2-23 T51	2-23 T51 Exploration ID:			LDW21-	GT23-GB				
Technician:	D	N Sample No:				n/a					
Sample Description:	Dark (	grayish-browr	n, silty SAND (	(SM)	Sample	Depth, ft:	28.5-30.5'				
Confining Pressures:	10 psi	20 psi	40 psi		Consolidation T50 Values (minutes)						
Initial Moisture:	33.4%	Final M	Noisture:	32.4%	10 psi	20 psi	40 psi				
Initial Wet Density, pcf:	115.2				0.6	0.6	1.0				
Initial Dry Density, pcf:	86.3				0.6	0.6	1.0				



	HWA GeoSciences Inc - Materials Testing Laboratory										
Consolidated-Undrained Triaxial Compression Test for Cohesive Soils (ASTM D 4767)											
Project Name:	L	ower Duwami	ish Waterway		Date:	8/28/	2021				
Project No.:	2012-00	2-23 T51 Exploration ID:			•	LDW21-0	GT33-GB				
Technician:	G	B Sample No:				n,	n/a				
Sample Description:	Very dark	grayish-browı	n, SILT with s	and (ML)	Sample	Depth, ft:	6.0 - 8.0				
Confining Pressures:	2.5 psi	5.0 psi	10.0 psi		Consolidation T50 Values (minutes)						
Initial Moisture:	64.8%	Final M	loisture:	see report	2.5 psi	5.0 psi	10.0 psi				
Initial Wet Density, pcf:	93.4		_		04.42	02.24	162.0				
Initial Dry Density, pcf:	56.7				91.13	83.21	162.0				

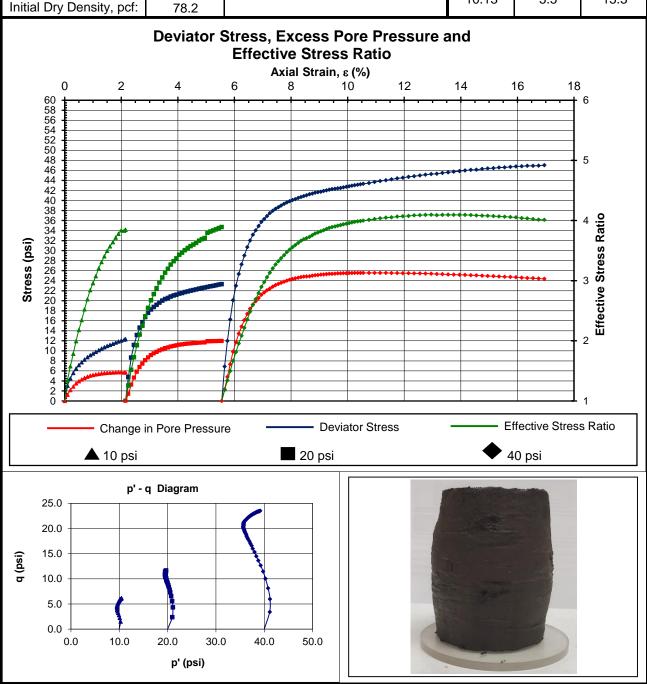


	HWA GeoSciences Inc - Materials Testing Laboratory										
Consolidated-Undrained Triaxial Compression Test for Cohesive Soils (ASTM D 4767)											
Project Name:	L	ower Duwam	ish Waterway	Date:	9/7/2	2021					
Project No.:	2012-00	2-23 T51	-23 T51 Exploration ID			LDW21-0	GT33-GB				
Technician:	G	B Sample No:				n.	/a				
Sample Description:	Very daı	k grayish-bro	wn, silty SANI	O (SM)	Sample	Depth, ft:	21.0-23.0				
Confining Pressures:	7 psi	14 psi	28 psi		Consolidation T50 Values (minutes)						
Initial Moisture:	35.3%	Final M	loisture:	34.7%	7 psi	14 psi	28 psi				
Initial Wet Density, pcf:	109.6			·	111 E	22.0	0.2				
Initial Dry Density, pcf:	81.0				144.5	23.8	0.3				



Reviewed by: SEG Figure 5

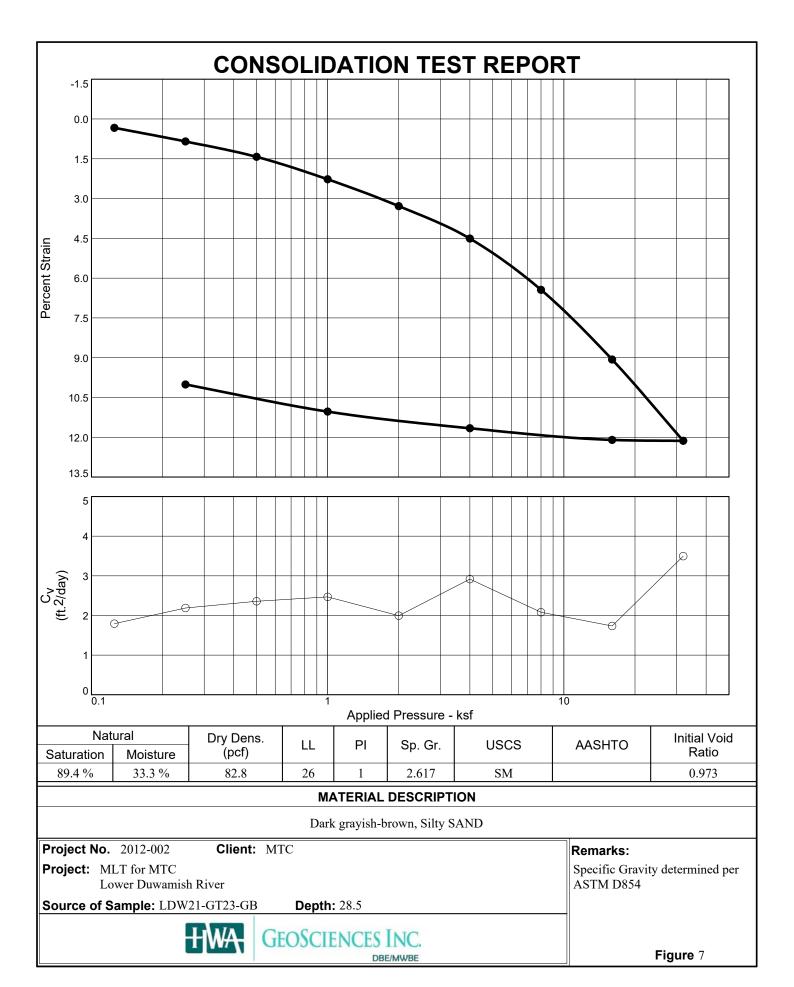
	HWA GeoSciences Inc - Materials Testing Laboratory										
Consolidated-Undrained Triaxial Compression Test for Cohesive Soils (ASTM D 4767)											
Project Name:	L	ower Duwami	sh Waterway		Date:	9/16/	6/2021				
Project No.:	2012-00	2-23 T51	2-23 T51 Exploration ID:			LDW21-0	-GT53-SPT				
Technician:	G	B Sample No:					n/a				
Sample Description:	Very dark	grayish-browr	n, SILT with s	and (ML)	Sample	Depth, ft:	30.0-32.0				
Confining Pressures:	10 psi	20 psi	40 psi		Consolidation T50 Values (minutes)						
Initial Moisture:	43.6%	Final M	loisture:	36.3%	10 psi	20 psi	40 psi				
Initial Wet Density, pcf:	112.3			·	10.12	5.5	45.0				
Initial Dry Density, pcf:	78.2				10.13	5.5	15.3				



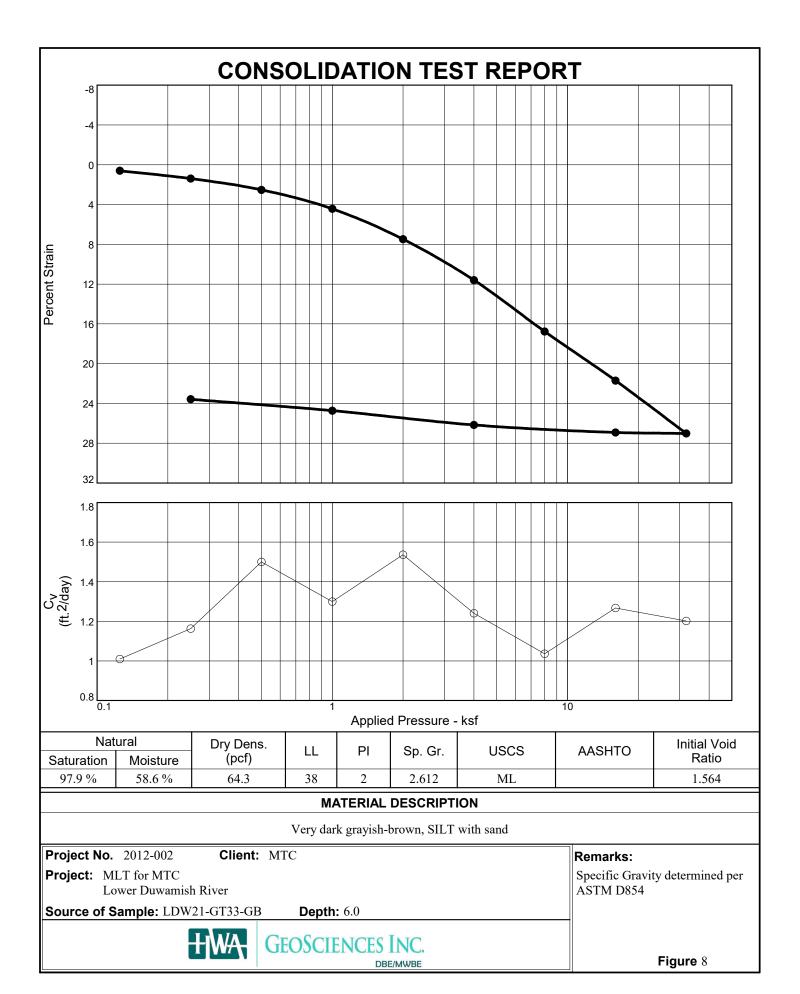
SEG

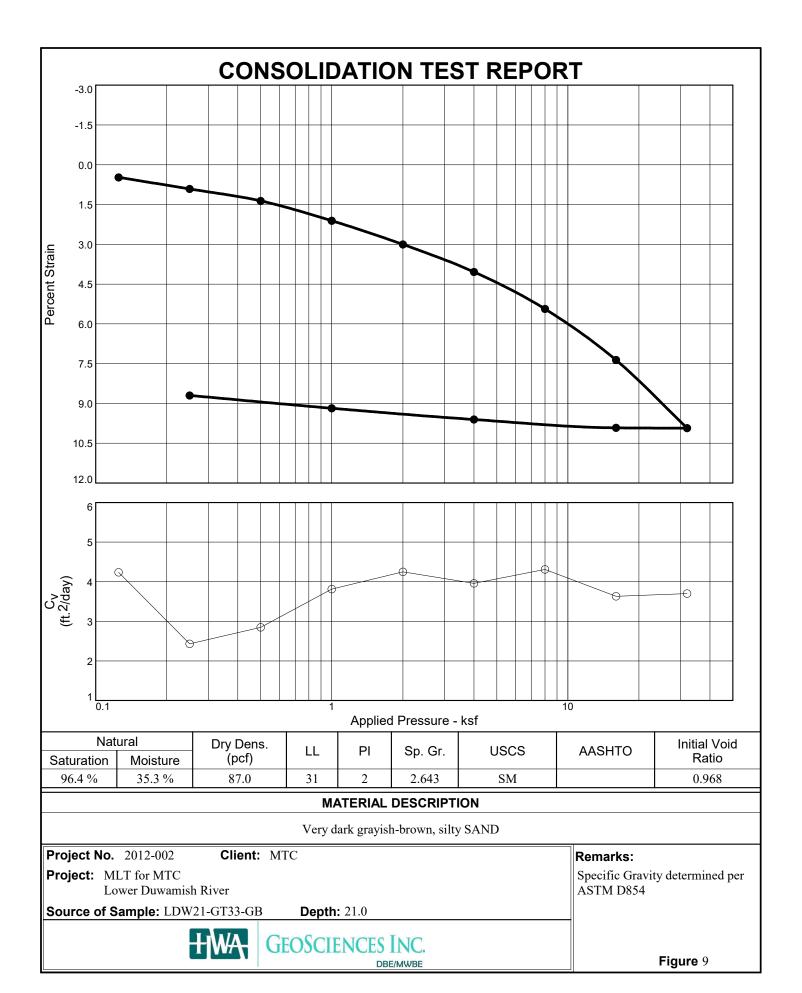
Figure

6

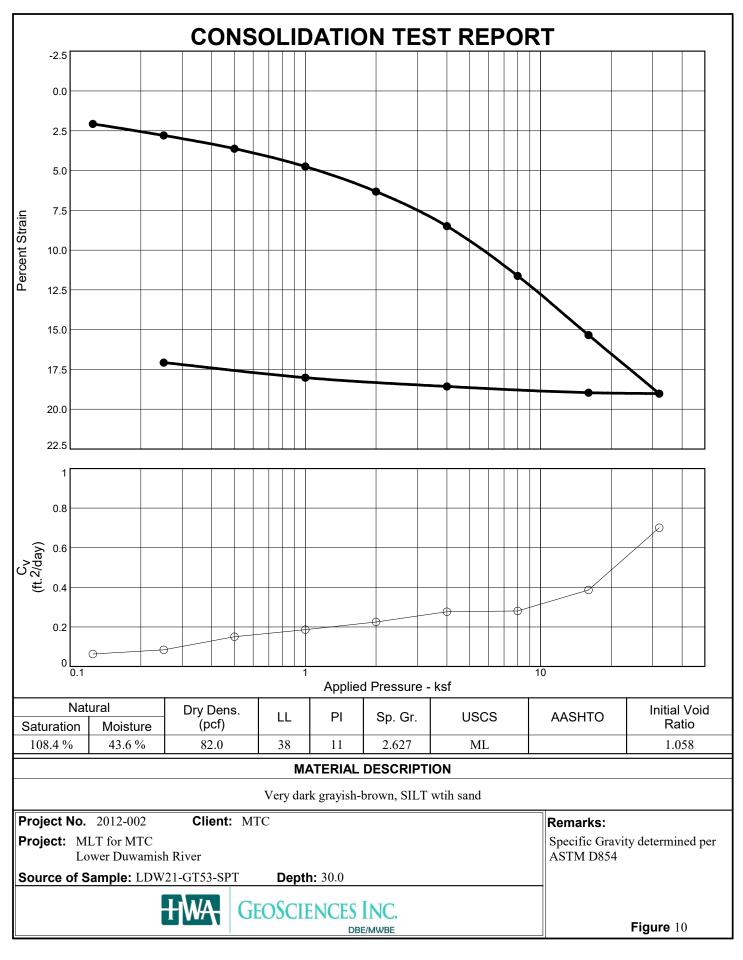


Tested By: AH/GB Checked By: SEG





Tested By: GB Checked By: SEG



Tested By: GB Checked By: SEG



Client:	Anchor QEA	Date:	October 22, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-2006 - 2020
Revised on:		Date sampled:	7-19-21 & 7-20-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor			Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



## **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 5, 2021	Tested by: M. Carrillo

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-2006	LDW21-GT5-0-1.5 ft	233.4	758.3	626.0	132.3	392.6	33.7%
B21-2007	LDW21-GT5-0-7.5 ft	266.3	675.6	572.3	103.3	306.0	33.8%
B21-2008	LDW21-GT5-7.5-9 ft	270.2	918.2	773.3	144.9	503.1	28.8%
B21-2009	LDW21-GT5-7.5-17.2ft	215.7	960.7	862.1	98.6	646.4	15.3%
B21-2010	LDW21-GT5-17.2-17.5 ft	300.9	721.1	625.3	95.8	324.4	29.5%
B21-2011	LDW21-GT5-17.5-19 ft	346.3	836.3	746.0	90.3	399.7	22.6%
B21-2012	LDW21-GT5-17.5-27.5 ft	341.8	961.5	816.3	145.2	474.5	30.6%
B21-2013	LDW21-GT5-27.5-29 ft	356.9	833.5	719.1	114.4	362.2	31.6%
B21-2014	LDW21-GT35-0-1.5 ft	360.3	821.8	607.9	213.9	247.6	86.4%
B21-2015	LDW21-GT35-5-6.5 ft	354.1	572.7	469.6	103.1	115.5	89.3%
B21-2016	LDW21-GT35-10-11.5 ft	359.4	882.4	671.2	211.2	311.8	67.7%
B21-2017	LDW21-GT35-15-16.5 ft	236.6	466.5	417.1	49.4	180.5	27.4%
B21-2018	LDW21-GT35-20-21.5 ft	237.4	947.7	793.9	153.8	556.5	27.6%
B21-2019	LDW21-GT35-25-26.5 ft	224.2	733.1	614.5	118.6	390.3	30.4%
B21-2020	LDW21-GT35-30-31.5 ft	225.1	669.4	560.4	109.0	335.3	32.5%

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



## **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 5, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Tare	Mass of Dry Soil	Pycno ID		Volume of Pycno	Water @ Tx		Mass of Pycno filled w/ water	Water, 0.1 *C	SpG of Soils	Factor	SpG
B21-2009	LDW21-GT5-7.5-17.2ft	601.79	703.81	102.0	TSA-022	198.0	499.5	0.99865	760.54	696.77				2.6686868
B21-2012	LDW21-GT5-17.5-27.5 ft	497.70	600.26	102.6	TSA-021	183.4	499.4	0.99869	744.61	682.18			1.00048	
B21-2017	LDW21-GT35-15-16.5 ft	509.68	611.88	102.2	TSA-023	163.9	498.7	0.99865	724.72	661.99	17.7	2.5895248	1.00045	2.5906901
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Pı	Project: Q.C Lower Duw roject #: 21B233 Client: Anchor QEA Source: LDW21-GT5-GB- ample #: B21-2007	-0-7.5 ft	5	te Received: Sampled By: Date Tested: Tested By:	Client 14-Oct-21	1	Visual Identific Sand with Silt Sample Color brown	cation
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan: Weight of Pry Soils: Weight of Moisture: % Moisture: Number of Blows:	Liquid I	imit cannot be est	tablished				Liquid Limit @ 25 Blows: N/A Plastic Limit: N/A Plasticity Index, I <sub>P</sub> : N/A
			mit Determinat					
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture:	#1 Plastic li	#2 mit cannot be det	#3	#4	#5	#6	ACCREDITED  Cartificato #: 1366.01, 1366.02 & 1366.04
Plasticity Index	70 % 60 % 50 % 40 % 20 % 10 % Copyright Spears Engineering & Tech	O O O L 20% 30% 40% L	sticity Chart  50% 6 iquid Limit	CH	or OH H or OH	90% 100	0% 110%	Liquid Limit  100% 90% 80% 70% 60% 40% 30% 100 Number of Blows, "N"

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumblind. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT5-GB-7.5-17.2 ft Sample#: B21-2009

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 6-Oct-21 Tested By: K. Mendez

SW-SM, Well-graded Sand with Silt and Gravel

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#10 #16

#20

#30

#40

#50

#60

#80

#100

#140

#170

#200

**Comments:** 

Sample Meets Specs? N/A

 $D_{(5)} = 0.034$   $D_{(10)} = 0.068$   $D_{(15)} = 0.162$   $D_{(30)} = 0.370$ % Gravel = 24.4% % Sand = 64.6% mm % Silt & Clay = 11.0% mm Liquid Limit = n/a mm  $D_{(50)} = 0.801$ mm Plasticity Index = n/a  $D_{(60)} = 1.580$ mm Sand Equivalent = n/a  $D_{(90)} = 12.641$ mm Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Unified Soil Classification System, ASTM-2487

Coeff. of Curvature,  $C_C = 1.27$ Coeff. of Uniformity,  $C_U = 23.13$ Fineness Modulus = 3.41 Plastic Limit = n/aMoisture %, as sampled = 15.3%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

					D	nust Datio =	22/72
Dust Ratio = 23/72 ASTM C136, ASTM D6913, ASTM C1							
		Actual Cumulativ	Interpolated Cumulative	Ac	51W C130, A3	1 10 100 113, 1	ASTM CITY
Sieve	Sieve Size		Percent Percent		Specs Specs		
US	Metric	Passing	Passing	Max	Min		ે છે. • • • • જાળા
12.00"	300.00		100%	100.0%	0.0%		T T
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		90%
6.00"	150.00		100%	100.0%	0.0%		F 1
4.00"	100.00		100%	100.0%	0.0%		- 1
3.00"	75.00		100%	100.0%	0.0%		80%
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		70%
1.75"	45.00		100%	100.0%	0.0%		11
1.50"	37.50		100%	100.0%	0.0%		<u> </u>
1.25"	31.50		100%	100.0%	0.0%		60%
1.00"	25.00	100%	100%	100.0%	0.0%	2	
3/4"	19.00	96%	96%	100.0%	0.0%	% Possing	50%
5/8"	16.00		93%	100.0%	0.0%	PG	30% F
1/2"	12.50	90%	90%	100.0%	0.0%		[ ]
3/8"	9.50	86%	86%	100.0%	0.0%		40%
1/4"	6.30		79%	100.0%	0.0%		
#4	4.75	76%	76%	100.0%	0.0%		
#8	2.36		66%	100.0%	0.0%		30%

65%

56%

52%

42%

34%

24%

20%

16%

14%

12%

12%

11.0%

100.0%

100.0%

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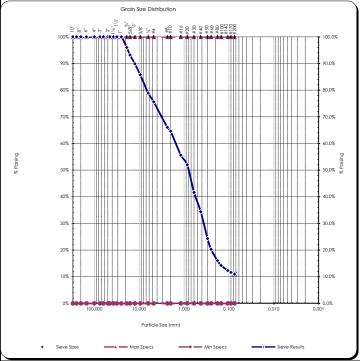
65%

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Reviewed by: Meghan Blodgett-Carrillo

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2009
Sample Date:	7/19/2021
Test Date:	10/12/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT5-GB-7.5-17.2 ft

 Visual Soil Description:
 brown sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

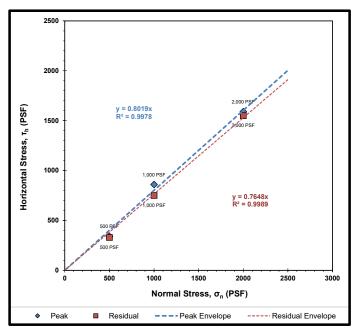
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	25.3	
	Initial	Post-Consolidation
Dry Density (PCF):	106.6	108.7
Void Ratio:	0.580	0.549
Porosity (%):	36.7	35.5
Degree of Saturation (%):	saturated	saturated

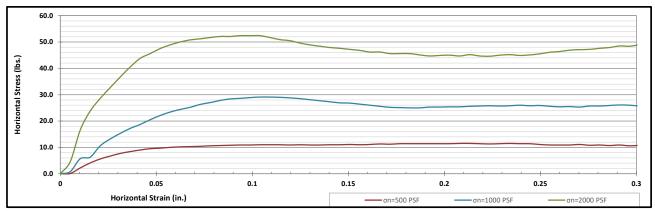
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	25.2	
	Initial	Post-Consolidation
Dry Density (PCF):	107.2	109.2
Void Ratio:	0.571	0.543
Porosity (%):	36.3	35.2
Degree of Saturation (%):	saturated	saturated

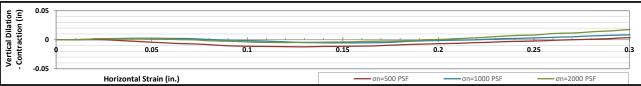
Summary of Sample	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	25.8	
	Initial	Post-Consolidation
Dry Density (PCF):	106.6	109.4
Void Ratio:	0.581	0.540
Porosity (%):	36.7	35.1
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS					
	PEAK	RESIDUAL			
Angle of Internal Friction, φ (°):	39	37			
Cohesion (PSF):	0	0			



Failure Envelope Test Values:						
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000			
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	340	860	1590			
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	330	750	1550			





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# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project #: Client:	Anchor QEA LDW21-GT5-GB-	·	Sa Da	Received: ampled By: ate Tested: Tested By:	Client 14-Oct-21		Visual Identific Sand with Silt Sample Color brown	ration
		Liquid Lim	t Determination	on				
		#1	#2	#3	#4	#5	#6	
Weight o	of Wet Soils + Pan:							
Weight	of Dry Soils + Pan:	Liquid lin	it cannot be estal	blished				
	Weight of Pan:							** *** *** ** *** ***
	eight of Dry Soils: eight of Moisture:							Liquid Limit @ 25 Blows: N/A Plastic Limit: N/A
	% Moisture:							Plasticity Index, I <sub>P</sub> : N/A
	Number of Blows:							
Weight	Plastic Limit Determination  #1 #2 #3 #4 #5 #6  Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Weight of Pan: Weight of Pan: Weight of Dry Soils: Weight of Moisture:				#6	ACCREDITED		
	% Moisture:							
70 % -	•	Plast	city Chart					Liquid Limit
60 % <b>-</b> 50 % -				- N	or OH	- Litipe		90% 80% 2 70%
city Ind								en to to to to to to to to to to to to to
Plasticity Index		O or OL		М	H or OH			30% - 20% -
0 % -	CL-M₽ % 10%	ML or OL 20% 30% 40%	50% 60°	% 70%	80%	90% 1	00% 110%	10%
			uid Limit		00.0	-5/0 1		10 100
Copyright	Spears Engineering & Techi							Number of Blows, "N"

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumblind. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo

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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233

Source: LDW21-GT5-GB-17.5-27.5 ft Sample#: B21-2012

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

82%

11.0%

#20

#30

#40 #50

#60

#80 #100

#140

#170

#200

**Comments:** 

Client: Anchor QEA

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 6-Oct-21

Tested By: K. Mendez

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

tions			
s			
Sample Meets Specs ? N/A			
	S	s	s

 $D_{(5)} = 0.022$   $D_{(10)} = 0.068$   $D_{(15)} = 0.088$ % Gravel = 0.6%% Sand = 88.5% mm % Silt & Clay = 11.0% mm  $D_{(30)} = 0.136$ Liquid Limit = n/a mm  $D_{(50)} = 0.239$ mm Plasticity Index = n/a  $D_{(60)} = 0.297$ mm Sand Equivalent = n/a  $D_{(90)} = 1.161$ ust Ratio = 2/15Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

Coeff. of Curvature,  $C_C = 0.91$ Coeff. of Uniformity,  $C_U = 4.38$ Fineness Modulus = 1.33 Plastic Limit = n/a

Moisture %, as sampled = 30.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				4.6	TM C126
		Actual Cumulativ	Interpolated Cumulative	AS	TM C136,
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	99%	99%	100.0%	0.0%
#8	2.36		99%	100.0%	0.0%
#10	2.00	99%	99%	100.0%	0.0%

90%

87%

84%

82%

61%

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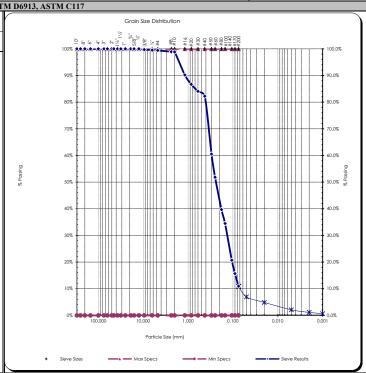
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Reviewed by: Meghan Blodgett-Carrillo



## **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SP-SM, Poorly graded Sand with Silt Client: Anchor QEA Date Tested: 6-Oct-21 Sample Color Source: LDW21-GT5-GB-17.5-27.5 ft Tested By: K. Mendez brown Sample#: B21-2012 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr. 2.56 Sieve Analysis Sample Weight: 100.01 Grain Size Distribution grams Hydroscopic Moist.: 1.52% Soils Particle Sieve Percent Adj. Sample Wgt: Passing 98.51 grams Size Diameter 75.000 mm 3.0" 100% 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 31.500 mm 1.25" 100% Minutes Reading **Passing** Diameter 0.0545 mm 100% 25.000 mm 8 8.2% 1.0" 0.0389 mm 3/4" 6 6.1% 100% 19.000 mm 5 5 5.1%  $0.0248\ mm$ 5/8" 100% 16.000 mm 15 4.5 4.6%0.0144 mm 1/2" 100% 12.500 mm 30 4 4 1%  $0.0102\ mm$ 3/8" 100% 9.500 mm 60 3.1%  $0.0072\ mm$ 1/4" 100% 6.300 mm 240 1.5 1.5% 0.0036 mm #4 99% 4.750 mm 1440 1.0% 0.0015 mm #10 99% 2.000 mm #20 87% 0.850 mm Liquid Limit: n/a 82% 0.425 mm % Gravel: % Sand: 88.5% Plastic Limit: n/a #100 35% 0.150 mm % Silt: 8.9% Plasticity Index: n/a #200 11.0% 0.075 mm 0.074 mm % Clay: 2.1% 10.8% 0.050 mm 6.9% 0.020 mm 4.9% 2.1% 0.005 mm Clavs 0.002 mm 1.1% Colloids 0.7% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding Comments:

Reviewed by:

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Pı	Project: Q.C Lower Duv roject #: 21B233 Client: Anchor QEA Source: LDW21-GT35-G ample #: B21-2015	•		te Received: Sampled By: Date Tested: Tested By:	Client 14-Oct-21		Visual Identific Clay Sample Color brown	cation
		Liquid I.	imit Determina	tion				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	30.42	27.71	26.95				
	Weight of Dry Soils + Pan:	27.89	24.44	23.66				
	Weight of Pan:	19.88	15.05	14.81				
	Weight of Dry Soils:	8.01	9.39	8.85				Liquid Limit @ 25 Blows: 32 %
	Weight of Moisture:	2.53	3.27	3.29				Plastic Limit: 9 %
	% Moisture:	31.6 %	34.8 %	37.2 %				Plasticity Index, I <sub>P</sub> : 23 %
	Number of Blows:	25	20	15				
		Plastic L	imit Determina	tion				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	37.34	36.36					
	Weight of Dry Soils + Pan: Weight of Pan:	36.82 31.03	35.86 30.33					
	Weight of Dry Soils:	5.79	5.53					ACCREDITED
	Weight of Moisture:	0.52	0.50					Certificate #: 1366.01, 1366.02 & 1366.04
	% Moisture:	9.0 %	9.0 %					
		Pla	sticity Chart					Liquid Limit
	<sup>70 %</sup> [							40% T
	60 %				Line			35%
				l l		"ALLIAB		
×	50 %				or OH	- PA		30%
<del>g</del>	40 %			CH	0,			25%
<u>-</u>								25% 150 W 20%
Plasticity Index	30 %							≥ 20% ÷
last	20 %	Cholor						15%
	20 %	Cror		M	H or OH			10%
	10 %							
	CL-MÉ	ML or OL						5%
	0 % 10%	20% 30% 40%	50% 6	60% 70%	80%	90%	100% 110%	0%
			Liquid Limit					10 100
$\overline{}$	0							Number of Blows, "N"
			s, the public and oursel	ves, all reports are sub	mitted as the confident	ial property of cl	lients, and authorization for	publication of statements, conclusions or extracts from or regarding our
	reserved pending our written approval.	•		-				, , , , , , , , , , , , , , , , , , ,
Comm	ents:							

Corporate ~ 777 Chrysler Drive • Burlington, WA 98233 • Phone (360) 755-1990 • Fax (360) 755-1980

Meghan Blodgett-Carrillo

**Regional Offices:** Olympia ~ 360.534.9777 Bellingham ~ 360.647.6111 Silverdale ~ 360.698.6787 Tukwila ~ 206.241.1974 Visit our website: www.mtc-inc.net



Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

#100

#140

#170

#200

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

35.1%

**Source:** LDW21-GT35-GB-15-16.5 ft **Sample#:** B21-2017

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 6-Oct-21 Tested By: K. Mendez Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

gray



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

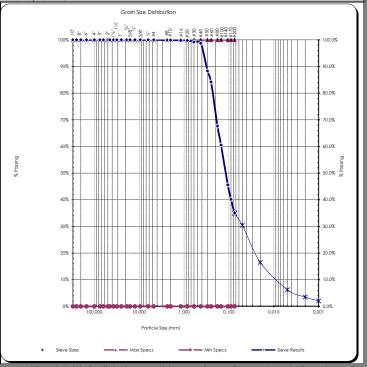
Sand Equivalent = n/a
Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 2.36$ Coeff. of Uniformity,  $C_U = 16.11$ Fineness Modulus = 0.52

Plastic Limit = n/a Moisture %, as sampled = 27.4% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						$D_{(90)} = 0$	.320 m	m		Fractu	re %	ı,
					Di	ust Ratio = 1	1/31		Fra	acture	%, 2	
				AS	STM C136, AST	ГМ D6913, <i>A</i>	ASTM C11	7				į
		Actual Cumulative	Interpolated Cumulative							Grain	Size D	i
Sieve	Size	Percent	Percent	Specs	Specs		ь	90 40 44 W	2	- State	ān -	
US	Metric	Passing	Passing	Max	Min		100%	90 -0 -4 W	, ∾ <u>≥</u>	= 15 ••••••	§ ≥ ••••••••••••••••••••••••••••••••••••	ì
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8.00"	200.00		100%	100.0%	0.0%		90%	-	₩₩	-	-##	ł
6.00"	150.00		100%	100.0%	0.0%		-					ı
4.00"	100.00		100%	100.0%	0.0%							ı
3.00"	75.00		100%	100.0%	0.0%		80%		m		1111	İ
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1.50"	37.50		100%	100.0%	0.0%		ŀ					l
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1.00"	25.00	100%	100%	100.0%	0.0%	20	-					l
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%					l
5/8"	16.00		100%	100.0%	0.0%	96	30%				IIII	İ
1/2"	12.50	100%	100%	100.0%	0.0%							ı
3/8"	9.50	100%	100%	100.0%	0.0%		40%	4	₩.	₽	-##	-
1/4"	6.30		100%	100.0%	0.0%		1					ı
#4	4.75	100%	100%	100.0%	0.0%		t					ı
#8	2.36		100%	100.0%	0.0%		30%	+-+	₩	-	₩	ł
#10	2.00	100%	100%	100.0%	0.0%		ŀ					ı
#16	1.18		100%	100.0%	0.0%		20%					ı
#20	0.850	100%	100%	100.0%	0.0%		20%		Ш			I
#30	0.600		99%	100.0%	0.0%							l
#40	0.425	99%	99%	100.0%	0.0%		10%	$+-\parallel$	##-		-##	-
#50	0.300		88%	100.0%	0.0%		1					
#60	0.250	84%	84%	100.0%	0.0%		ţ					
#80	0.180		68%	100.0%	0.0%		0%	100,000	0 000	10-00-0	0.000	(



Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval

0.0%

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0.0%

100.0%

100.0%

100.0%

100.0%

61%

46%

40%

35.1%



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project #: 21B233 Sampled By: Client SM, Silty Sand Client: Anchor QEA Date Tested: 6-Oct-21 Sample Color Source: LDW21-GT35-GB-15-16.5 ft Tested By: K. Mendez gray Sample#: B21-2017 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp Gr. 2.59 Sieve Analysis Sample Weight: 102.29 grams **Grain Size Distribution** Hydroscopic Moist.: 1.10% Soils Particle Sieve Percent Adj. Sample Wgt: ACCREDITED Passing 101.18 grams Size Diameter 75.000 mm 3.0" 100% Hydrometer 2.0" 100% 50.000 mm Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 31.500 mm 1.25" 100% Minutes Reading **Passing** Diameter 0.0486 mm 100% 25.000 mm 27.5 27.7% 1.0" 3/4" 23 23.2% 0.0352 mm 100% 19.000 mm 18 18.1% 0.0230 mm 5/8" 100% 16.000 mm 15 13 13.1%  $0.0137\ mm$ 1/2" 100% 12.500 mm 30 10.5 10.6% 0.0099 mm 3/8" 100% 9.500 mm 60 8.1% $0.0070 \, \text{mm}$ 1/4" 100% 6.300 mm 240 5 5.0% 0.0036 mm #4 100% 4.750 mm 1440 3.0% 0.0015 mm #10 100% 2.000 mm #20 100% 0.850 mm % Gravel: 0.0% Liquid Limit: n/a 99% 0.425 mm % Sand: 64.9% Plastic Limit: n/a #100 61% 0.150 mm % Silt: 28.8% Plasticity Index: n/a #200 35.1% 0.075 mm 0.074 mm % Clay: 34.8% 30.4% 0.050 mm 0.020 mm 16.5% 6.3% 0.005 mm Clavs 0.002 mm 3.5% Colloids 2.0% 0.001 mm **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding Comments:

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2017
Sample Date:	7/20/2021
Test Date:	10/6/2021
Technician:	M. Carrillo

 Sample Source:
 LDW21-GT35-GB-15-16.5 ft

 Visual Soil Description:
 gray sand

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

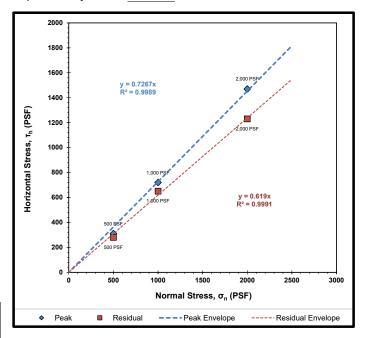
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Samp	le Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	29.5	
	Initial	Post-Consolidation
Dry Density (PCF):	109.5	110.5
Void Ratio:	0.539	0.525
Porosity (%):	35.0	34.4
Degree of Saturation (%):	saturated	saturated

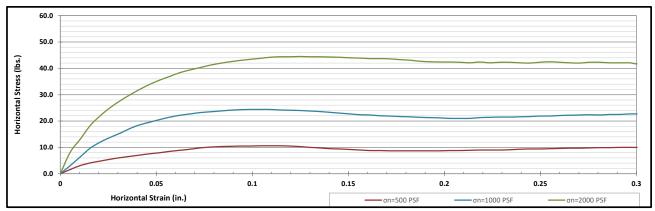
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF		
Initial Moisture Content (%):	30.1			
	Initial	Post-Consolidation		
Dry Density (PCF):	108.1	110.4		
Void Ratio:	0.559	0.527		
Porosity (%):	35.8	34.5		
Degree of Saturation (%):	saturated	saturated		

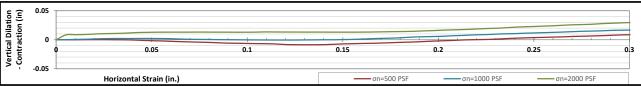
Summary of Sampl	e Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	32.2	
	Initial	Post-Consolidation
Dry Density (PCF):	107.5	110.7
Void Ratio:	0.567	0.522
Porosity (%):	36.2	34.3
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS							
PEAK RESIDUAL							
Angle of Internal Friction, φ (°):	36	32					
Cohesion (PSF):	0	0					



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	310	720	1470				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	280	650	1230				





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#140

#170

#200

0.106

0.090

0.075

Meghan Blodgett-Carrillo

19.5%

Source: LDW21-GT35-GB-20-21.5 ft Sample#: B21-2018

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 6-Oct-21

Tested By: K. Mendez

SM, Silty Sand

Sample Color:

brown

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.019$   $D_{(10)} = 0.038$   $D_{(15)} = 0.058$   $D_{(30)} = 0.108$   $D_{(50)} = 0.166$ % Gravel = 0.0%% Sand = 80.5% mm % Silt & Clay = 19.5% mm Liquid Limit = n/a mm mm Plasticity Index = n/a  $D_{(60)} = 0.189$ mm

Unified Soil Classification System, ASTM-2487

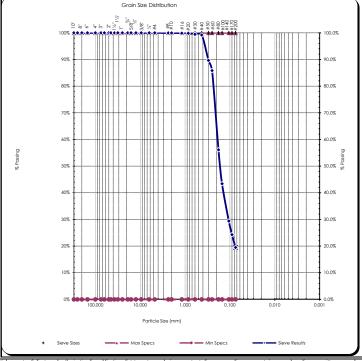
Sand Equivalent = n/a

Coeff. of Curvature,  $C_C = 1.60$ Coeff. of Uniformity,  $C_U = 4.92$ Fineness Modulus = 0.68

Plastic Limit = n/a Moisture %, as sampled = 27.6% Req'd Sand Equivalent =

Req'd Fracture %, 1 Face = Req'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.304$	mn	n	F	racture	e %, 1	Face	= n/	a
						ust Ratio = 13/66			Fra	cture %	6, 2+	Faces	= n/	'a
				AS	STM C136, AST	ΓM D6913, ASTN	M C117	1						
		Actual	Interpolated							Grain Siz	ze Distri	bution		
		_	Cumulative											
	Size	Percent	Percent	Specs	Specs		b;	. !	<u> </u>	5/8%	) :- <del>-</del> 4	∞2	91 #19	3 :
US	Metric	Passing	Passing	Max	Min		100%	***		فعقعه	; > = ininini	<b>-44</b>	***	Ť
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1/2"	12.50	100%	100%	100.0%	0.0%		-							Ш
3/8"	9.50	100%	100%	100.0%	0.0%		40%		444	4			-##	Ш
1/4"	6.30		100%	100.0%	0.0%									Ш
#4	4.75	100%	100%	100.0%	0.0%		- 1							Ш
#8	2.36		100%	100.0%	0.0%		30%		###	-	###	++-	-##	Ħ
#10	2.00	100%	100%	100.0%	0.0%		ŀ							Ш
#16	1.18		100%	100.0%	0.0%		20%							Ш
#20	0.850	100%	100%	100.0%	0.0%		20% F				IIII			П
#30	0.600		99%	100.0%	0.0%		- 1							Ш
#40	0.425	99%	99%	100.0%	0.0%		10%		444	+	$\mathbb{H}$	+	-##	Н
#50	0.300		90%	100.0%	0.0%									
#60	0.250	86%	86%	100.0%	0.0%									
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Comments.			
Reviewed by:	Nagh Bladget anillo		

100.0%

100.0%

100.0%

29%

24%

19.5%

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



# ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

P	Project: Q.C Lower Duv roject #: 21B233 Client: Anchor QEA Source: LDW21-GT35-Gl ample #: B21-2020	•	5	te Received: Sampled By: Date Tested: Tested By:	Client 14-Oct-21		Visual Identific Silty Sand Sample Color brown	cation	
			nit Determinat						
	W ' 14 (W 46 ') + D	#1	#2	#3	#4	#5	#6		
	Weight of Wet Soils + Pan:	** ***	5 AL -	101 1					
	Weight of Dry Soils + Pan: Weight of Pan:	Liquid ii	mit cannot be est	abiisned					
	Weight of Dry Soils:							Liquid Limit @ 25 Blows: N/A	
	Weight of Moisture:							Plastic Limit: N/A	
	% Moisture: Number of Blows:							<b>Plasticity Index, I<sub>P</sub>:</b> N/A	
	Number of Blows.								
			nit Determinat						
	Weight of Wet Soils + Pan:	#1	#2	#3	#4	#5	#6		
	Weight of Dry Soils + Pan:	Plastic lii	nit cannot be det	ermined					
	Weight of Pan:								
	Weight of Dry Soils: Weight of Moisture:							ACCREDITED  Certificate #: 1366.01, 1366.02 & 1366.04	
	% Moisture:							Certificate #: 1306.01, 1306.02 & 1306.04	
							$\overline{}$		\
	70 % <b>T</b>	Plas	ticity Chart					Liquid Limit	1
								100%	
	60 %				I LINE	سعمد ر		90%	
	50 %				NY -	WHITE THE		80%	
ğ	40.0/			CH	or OH			2 70%	
Ě	40 %			<u> </u>				9 60%	
icit	30 %								
Plasticity Index	20 %	OL						40%	I
<u> </u>		CL or OL		M	H or OH			30%	
	10 %							20%	
	0 % CL-ML	ML or OL					<b>—</b>	10%	
	0% 10%	20% 30% 40%		0% 70%	80%	90% 10	00% 110%	0%   10 100	
		Li	quid Limit					Number of Blows, "N"	
	Copyright Spears Engineering & Tech	inical Services PS, 1996-98							

All results apply only to actual tocations and mate reports is reserved pending our written approval.

Liquid limit cannot be established as the material displays rapid dilation upon spreading into the cup. At lower moistures the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the material does not roll down to 1/8" threads before cracking or crumblind. Non-plastic.

Reviewed by: Meghan Blodgett-Carrillo



Client:	Anchor QEA	Date:	October 25, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-2143-2162
Revised on:		Date sampled:	August 5, 2021

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor	Trease see Tituenea Reports		Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 15, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-2143	LDW21-GT48-GB-21.6-25 ft	234.6	512.3	437.5	74.8	202.9	36.9%
B21-2144	LDW21-GT48-GB-25-30 ft	221.6	1232.1	959.0	273.1	737.4	37.0%
B21-2145	LDW21-GT48-GB-30-35 ft	215.3	1034.5	826.3	208.2	611.0	34.1%
B21-2146	LDW21-GT48-GB-35-36.5 ft	235.3	1073.2	832.7	240.5	597.4	40.3%
B21-2147	LDW21-GT53-GB-0-1.5 ft	228.9	845.1	638.7	206.4	409.8	50.4%
B21-2148	LDW21-GT53-GB-0-5 ft	208.5	682.6	526.4	156.2	317.9	49.1%
B21-2149	LDW21-GT53-GB-5-6.5 ft	222.9	1006.1	801.8	204.3	578.9	35.3%
B21-2150	LDW21-GT53-GB-5-10 ft	229.4	762.5	595.5	167.0	366.1	45.6%
B21-2151	LDW21-GT53-GB-10-15 ft	221.1	1092.3	749.6	342.7	528.5	64.8%
B21-2152	LDW21-GT53-GB-15-20 ft	220.4	805.0	678.3	126.7	457.9	27.7%
B21-2153	LDW21-GT53-GB-20-23.5 ft	222.9	998.0	819.4	178.6	596.5	29.9%
B21-2154	LDW21-GT53-GB-23.5-25 ft	217.3	990.1	795.4	194.7	578.1	33.7%
B21-2155	LDW21-GT53-GB-25-28.6 ft	222.6	807.8	656.4	151.4	433.8	34.9%
B21-2156	LDW21-GT53-GB-28.6-30 ft	224.3	929.6	800.4	129.2	576.1	22.4%
B21-2157	LDW21-GT48-SPT-0-0.7 ft	268.9	742.1	658.8	83.3	389.9	21.4%
B21-2158	LDW21-GT48-SPT-0.7-1.5 ft	310.9	685.1	612.8	72.3	301.9	23.9%
B21-2159	LDW21-GT48-SPT-10-11.5 ft	319.8	870.6	717.8	152.8	398.0	38.4%
B21-2160	LDW21-GT48-SPT-15-16.5 ft	301.0	852.0	723.3	128.7	422.3	30.5%
B21-2161	LDW21-GT48-SPT-20-20.6 ft	302.0	675.6	567.7	107.9	265.7	40.6%
B21-2162	LDW21-GT48-SPT-20.6-21.5 ft	303.2	829.7	715.1	114.6	411.9	27.8%
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is

Reviewed by:



#### **Moisture Content - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 16, 2021	Tested by: A. Eifrig

Sample # B21-2143	Location LDW21-GT48-GB-21.6-25 ft	Tare 420.68	Tare 495.04	Mass of Dry Soil 74.4	Pycno ID TSA-010	Mass of Pycno 180.3	Volume of Pycno 499.5	Water @ Tx 0.99854	725.29	Mass of Pycno filled w/ water 679.12	Water, 0.1 *C 18.3	SpG of Soils 2.6377506	Factor 1.00034	
B21-2148	LDW21-GT53-GB-0-5 ft	413.74	512.57	98.8	TSA-011	190.3	499.5	0.99856	747.85	689.15			1.00035	
B21-2152	LDW21-GT53-GB-15-20 ft	379.63	483.20	103.6	TSA-017	187.9	499.4	0.99841	751.03	686.50		2.6531994		2.65373
B21-2155	LDW21-GT53-GB-25-28.6 ft	394.13	472.87	78.7	TSA-022	198.0	499.5	0.99856	743.69	696.72	18.3	2.478377	1.00035	2.4792444
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT48-GB-21.6-25 ft

Sample#: B21-2143

Date Received: 29-Jul-21 Sampled By: Client

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

Date Tested: 15-Oct-21 Tested By: A. Eifrig

Visual Identification Silt with Sand and Clay Sample Color:

brown

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#50

#60

#80 #100

#140

#170

#200

Sample Meets Specs? N/A

 $D_{(5)} = 0.001$   $D_{(10)} = 0.003$   $D_{(15)} = 0.004$ mm % Silt & Clay = 87.7% mm  $D_{(30)} = 0.010$ Liquid Limit = n/a mm  $D_{(50)} = 0.023$ mm Plasticity Index = n/a  $D_{(60)} = 0.040$ mm  $D_{(90)} = 0.090$ Dust Ratio = 29/33 mm

Sand Equivalent = n/a Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

% Gravel = 0.0%

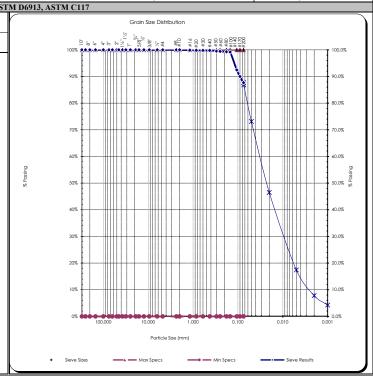
% Sand = 12.3%

Coeff. of Curvature,  $C_C = 0.94$ Coeff. of Uniformity,  $C_U = 14.64$ Fineness Modulus = 0.02

Plastic Limit = n/a Moisture %, as sampled = 36.9% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				AS	TM C136,
		Actual Cumulative	Interpolated Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		100%	100.0%	0.0%
#20	0.850		100%	100.0%	0.0%
#30	0.600		100%	100.0%	0.0%
#40	0.425	100%	100%	100.0%	0.0%
	1				



0.0%

0.0%

0.0%

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0.0%

0.0%

**Comments:** Reviewed by: \_ Meghan Blodgett-Carrillo

100%

99%

99%

99%

92%

90%

87.7%



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Project #: 21B233 Silt with Sand and Clay Sampled By: Client Client: Anchor QEA Date Tested: 15-Oct-21 Sample Color Source: LDW21-GT48-GB-21.6-25 ft Tested By: A. Eifrig brown Sample#: B21-2143 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Sp. Gr 2.64 Sieve Analysis Sample Weight: 50.35 **Grain Size Distribution** Hydroscopic Moist.: 2.46% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 49.14 Size Passing Diameter 3.0" 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 63 7% 0.0464 mm 100% 25.000 mm 31 1.0" 56.5% 0.0338 mm 3/4" 100% 19.000 mm 2 27.5 24 49 3%  $0.0218\ mm$ 5/8" 100% 16.000 mm 15 17.5 36.0%  $0.0131\ mm$ 1/2" 100% 12.500 mm 30 14 28.8% 0.0095 mm 3/8" 100% 9.500 mm 60 11.5 23.6% 0.0068 mm 1/4" 100% 6.300 mm 240 12.3% 0.0035 mm 100% 4.750 mm #4 #10 100%  $2.000\ mm$ 1440 6.2%  $0.0015 \ mm$ #20 100% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 100%  $0.425 \, mm$ % Sand: 12.3% Plastic Limit: n/a #100 99% 0.150 mm % Silt: 70.2% Plasticity Index: n/a #200 87.7%  $0.075 \ mm$ 86.8% 0.074 mm % Clay: 17.5% Silts 73.1% 0.050 mm 0.020 mm 46.5% 17.5% 0.005 mm Clays 7.8%  $0.002\ mm$ Colloids 4.2%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:



### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Silt with Sand and Clay **Project #:** 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 15-Oct-21 Sample Color Source: LDW21-GT48-GB-21.6-25 ft Tested By: A. Eifrig Sample #: B21-2143 **Liquid Limit Determination** Weight of Wet Soils + Pan: ACCREDITED Weight of Dry Soils + Pan: Unable to establish liquid limit Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: N/A Number of Blows: Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Cannot determined plastic limit Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 100% 60 % 90% 50 % Plasticity Index 40 % 60% 30 % 50% 20 % 20% 100% 110% 10% **Liquid Limit** 10 100

Liquid limit cannot be established as the material displays rapid dilation. At lower moistures, the material does not spread into the liquid limit device without

tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Silt with Sand and Clay **Project #:** 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 15-Oct-21 Sample Color Source: LDW21-GT48-GB-25-30 ft Tested By: A. Eifrig Sample #: B21-2144 **Liquid Limit Determination** Weight of Wet Soils + Pan: ACCREDITED Weight of Dry Soils + Pan: Unable to establish liquid limit Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: N/A Number of Blows: Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Cannot determined plastic limit Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Plasticity Chart Liquid Limit** 100% 60 % 90% 50 % Plasticity Index 40 % 60% 30 % 50% 20 % 20% 100% 110% 10% **Liquid Limit** 10 100

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough control of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our enough of the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our extracts.

Comments: Liquid limit cannot be established as the material displays rapid dilation. At lower moistures, the material does not spread into the liquid limit device without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:

# Materials Testing & Consulting, Inc. Geotechnical Engineering • Special Inspections • Materials Testing • Environmental Consulting



## ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Pr	Project: Q.C Lower Duwamis oject #: 21B233 Client: Anchor QEA, LLC Source: LDW21-GT48-GB-30 mple #: B21-2145	·		ate Received: Sampled By: Date Tested: Tested By:	Client	1	Visual Identific Silt with Clay Sample Color brown	ation
		Liquid 1	Limit Determin	ation				
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan:	29.11	30.59	34.12				
	Weight of Dry Soils + Pan:	25.96	26.90	30.59				
	Weight of Pan:	15.19	14.77	19.81				
	Weight of Dry Soils:	10.77	12.13	10.78				Liquid Limit @ 25 Blows: 30 %
	Weight of Moisture:	3.15	3.69	3.53				Plastic Limit: 24 %
	% Moisture: Number of Blows:	29.3 %	30.4 %	32.8 % 18				Plasticity Index, I <sub>P</sub> : 6 %
	Number of Blows:	30	23	10				
			Limit Determin					
		#1	#2	#3	#4	#5	#6	
	Weight of Wet Soils + Pan: Weight of Dry Soils + Pan:	34.58 33.37	35.80 34.35					
	Weight of Pan:	28.28	28.60					
	Weight of Dry Soils:	5.09	5,75					ACCREDITED
	Weight of Moisture:	1.21	1.45					Certificate #: 1366.01, 1366.02 & 1366.04
	% Moisture:	23.8 %	25.2 %					
		P	asticity Char	t				Liquid Limit
	<sup>70 %</sup> [							35% T
	60 %				, time			•
				M	5	علينيه.		30%
Ų	50 %				,OH _	<b>L</b>		25%
ê	40 %		/   /	CH	or OH			
툿	40 /0							woistness 20%
ici	30 %							× 1507
Plasticity Index		(N)						15%
ä	20 %	CLorOL		LΛ	H or OH			10%
	10 %			I Y I				
	CL-ML	ML or OL						5%
	0 %	<del></del>		000/		2001	1100	0%
	0% 10% 20%	30% 40%	50%	60% 70%	80%	90% 1	00% 110%	10 100
			Liquid Limit					Number of Blows, "N"
	Copyright Spears Engineering & Technical S	ervices PS, 1996-98	•		·			

Comments:

Reviewed by: Meghan Blodgett-Carrillo

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### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils



Liquid limit cannot be established as the material displays rapid dilation. At lower moistures, the material does not spread into the liquid limit device without

tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT53-GB-5-10 ft Sample#: B21-2150

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 15-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.005 \\ \textbf{D}_{(10)} = 0.028 \\ \textbf{D}_{(15)} = 0.056 \\ \textbf{D}_{(30)} = 0.081 \\ \textbf{D}_{(50)} = 0.113 \\ \textbf{D}_{(60)} = 0.129 \\ \textbf{D}_{(90)} = 0.335 \\ \textbf{P}_{(15)} = 10/37 \\ \textbf{D}_{(27)} = 10/37 \\ \textbf{D}_{(37)} = 10$ % Gravel = 0.0%% Sand = 73.4% mm % Silt & Clay = 26.6% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a Coeff. of Curvature,  $C_C = 1.81$ Coeff. of Uniformity,  $C_U = 4.67$ Fineness Modulus = 0.43 Plastic Limit = n/a

Moisture %, as sampled = 45.6% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

						ust Ratio =				e %, 2+ F						e %, 2+	
				AS	TM C136, AS	FM D6913, A	ASTM C117	1									
			Interpolated						Grai	n Size Distrib	ution						
		Cumulative			1	4			Ę.,								
Sieve		Percent	Percent	Specs	Specs		. 0.	0 je je je 0	7. 7.	3/8 74	<u>\$</u> 2 2 8	8 8 8	88888	8			
US	Metric	Passing	Passing	Max	Min	4	100%	****		•••	**	***		<u> </u>		ППП	100.0%
12.00"	300.00		100%	100.0%	0.0%		F					1					1
10.00"	250.00		100%	100.0%	0.0%		}					1					1
8.00"	200.00		100%	100.0%	0.0%		90%					T V					90.0%
6.00"	150.00		100%	100.0%	0.0%		1					III Ì					1
4.00"	100.00		100%	100.0%	0.0%		80%					3					80.0%
3.00"	75.00		100%	100.0%	0.0%		1						X I				
2.50"	63.00		100%	100.0%	0.0%		ŀ						A				1
2.00"	50.00	100%	100%	100.0%	0.0%		70%	1	+++-			++++	+	HHHH		+++-	70.0%
1.75"	45.00		100%	100.0%	0.0%		ŀ										1
1.50"	37.50		100%	100.0%	0.0%		1										1
1.25"	31.50		100%	100.0%	0.0%		60%										60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	0	ŀ										1 3
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	50%										50.0%
5/8"	16.00		100%	100.0%	0.0%	P6	50,0						N				B 50.0%
1/2"	12.50	100%	100%	100.0%	0.0%		-						li				1
3/8"	9.50	100%	100%	100.0%	0.0%		40%	<b></b>	HHHH				+		_	###	40.0%
1/4"	6.30		100%	100.0%	0.0%		1										1
#4	4.75	100%	100%	100.0%	0.0%		t										
#8	2.36		100%	100.0%	0.0%		30%	1						₩₩			30.0%
#10	2.00	100%	100%	100.0%	0.0%		ŀ							*			1
#16	1.18		99%	100.0%	0.0%									IN III			
#20	0.850		99%	100.0%	0.0%		20%							Y I			20.0%
#30	0.600		99%	100.0%	0.0%									*			1
#40	0.425	98%	98%	100.0%	0.0%		10%	1						$\square \backslash \backslash$	4	4444	10.0%
#50	0.300		87%	100.0%	0.0%		t									11.11.1	
#60	0.250		82%	100.0%	0.0%		ŀ									T*	
#80	0.180		76%	100.0%	0.0%		0%	100.000	debde be	10.000	1.000		0.10	MITT	0.010	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.0%
#100	0.150	73%	73%	100.0%	0.0%			100.000		10.000	1.000	,	0.10		0.010	,	0.001
#140	0.106		46%	100.0%	0.0%					Particle Si	e (mm)						
#170	0.090		36%	100.0%	0.0%												
#200	0.075	26.6%	26.6%	100.0%	0.0%		Sieve Sizes			Max Specs	_	• — Mir	n Specs	_		iieve Results	
		hnical Services PS, 1996-9		100.070	0.070		. 5,0,0 31263			υρουσ		- 711	pocs				
				and ourselves, all reports are	submitted as the confide	ntial property of cli	ents and authorize	tion for pul	dication of st	atements, conc	usions or ex	ctracts from	m or regar	rding our p	enorts is res	erved nendi	ng our written an

Reviewed by:



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 15-Oct-21 Sample Color Source: LDW21-GT53-GB-5-10 ft Tested By: A. Eifrig brown Sample#: B21-2150 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 Assumed Sp. Gr 2.65 Sieve Analysis Sample Weight: 100.03 **Grain Size Distribution** Hydroscopic Moist.: 2.23% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 97.85 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0516 mm 100% 25.000 mm 12 12.3% 1.0" 3/4" 100% 19.000 mm 2 11.5 11.8% 0.0368 mm 9.2%  $0.0235\ mm$ 5/8" 100% 16.000 mm 15 8.2%  $0.0137 \ mm$ 1/2" 100% 12.500 mm 30 7.2% 0.0097 mm 3/8" 100% 9.500 mm 60 6.5 6.6% 0.0069 mm 1/4" 100% 6.300 mm 240 3.1% 0.0035 mm 100% 4.750 mm #4 #10 100%  $2.000\ mm$ 1440 2.0%  $0.0014\ mm$ #20 99% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 98%  $0.425 \, mm$ % Sand: 73.4% Plastic Limit: n/a #100 73% 0.150 mm % Silt: 22.0% Plasticity Index: n/a #200 26.6%  $0.075 \ mm$ 0.074 mm % Clay: 4.6% Silts 26.0% 14.3% 0.050 mm 0.020 mm 8.8% 4.6% 0.005 mm Clays 2.3%  $0.002\ mm$ Colloids 1.4%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Loamy Sand All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2150
Sample Date:	8/5/2021
Test Date:	10/18/2021
Technician:	M. Carrillo

Sample Source: LDW21-GT53-GB-5-10 ft
Visual Soil Description: brown silty sand with gravel
Type of Specimen: Remolded Cylindrical Shear Box
Specimen Diameter (in): 2.5

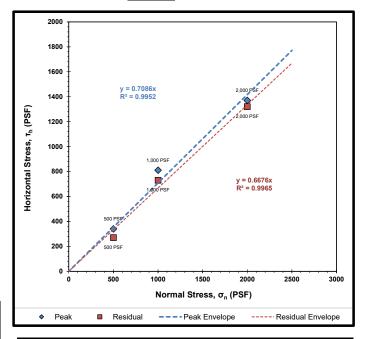
Specimen Height (in): 1
Rate of Strain (in/min): 0.0208
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	30.0	
	Initial	Post-Consolidation
Dry Density (PCF):	109.7	110.6
Void Ratio:	0.536	0.523
Porosity (%):	34.9	34.3
Degree of Saturation (%):	saturated	saturated

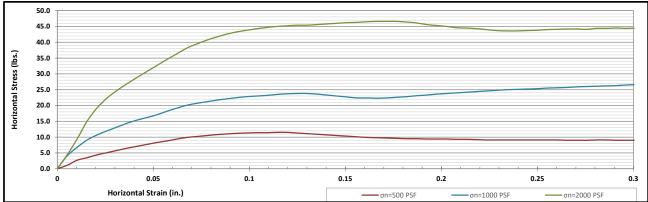
Summary of Sample	Data:	: $\sigma_n$ =1000 PSF				
Initial Moisture Content (%):	29.9					
	Initial	Post-Consolidation				
Dry Density (PCF):	110.2	112.7				
Void Ratio:	0.529	0.495				
Porosity (%):	34.6	33.1				
Degree of Saturation (%):	saturated	saturated				

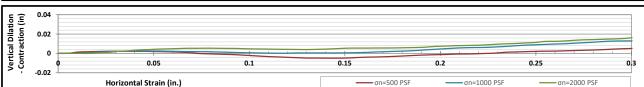
Summary of Sample	le Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	29.3	
	Initial	Post-Consolidation
Dry Density (PCF):	110.5	114.2
Void Ratio:	0.524	0.475
Porosity (%):	34.4	32.2
Degree of Saturation (%):	saturated	saturated

ESTIMATED STRENGTH PARAMETERS											
PEAK RESIDUAL											
Angle of Internal Friction, φ (°):	35	34									
Cohesion (PSF):	0	0									



Failure Envelope Test Values:											
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000								
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	340	810	1370								
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	270	730	1320								





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT53-GB-10-15 ft Sample#: B21-2151

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 15-Oct-21

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color: brown

mm

ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

#40

#50

#60

#80 #100

#140

#170

#200

80%

61%

Sample Meets Specs? N/A

 $D_{(5)} = 0.022$   $D_{(10)} = 0.044$   $D_{(15)} = 0.066$ % Gravel = 3.1% % Sand = 79.8% mm % Silt & Clay = 17.1% mm  $D_{(30)} = 0.118$ Liquid Limit = n/a mm  $D_{(50)} = 0.199$ mm Plasticity Index = n/a  $D_{(60)} = 0.246$   $D_{(90)} = 0.735$ mm Sand Equivalent = n/a

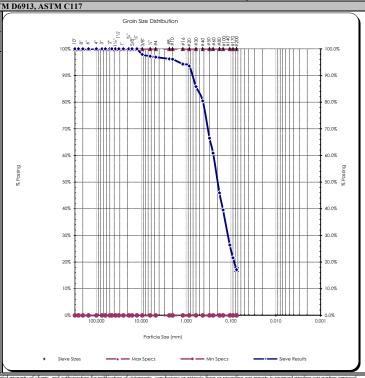
Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Coeff. of Curvature,  $C_C = 1.30$ Coeff. of Uniformity,  $C_U = 5.62$ Fineness Modulus = 1.23 Plastic Limit = n/a

Moisture %, as sampled = 64.8% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} =$	0.735
						ust Ratio =	
				AS	TM C136, AS	TM D6913,	ASTM
		Actual	Interpolated				
		1	Cumulative		1	4	
Sieve		Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min	4	1
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		
6.00"	150.00		100%	100.0%	0.0%		
4.00"	100.00		100%	100.0%	0.0%		
3.00"	75.00		100%	100.0%	0.0%		
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		
1.00"	25.00	100%	100%	100.0%	0.0%	20	
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing	
5/8"	16.00		100%	100.0%	0.0%	96	
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	98%	98%	100.0%	0.0%		
1/4"	6.30		97%	100.0%	0.0%		
#4	4.75	97%	97%	100.0%	0.0%		
#8	2.36		96%	100.0%	0.0%		
#10	2.00	96%	96%	100.0%	0.0%		
#16	1.18		94%	100.0%	0.0%		
#20	0.850	94%	94%	100.0%	0.0%		
#30	0.600		86%	100.0%	0.0%		



0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

Comments: Reviewed by: Meghan Blodgett-Carrillo

80%

66%

61%

46%

40%

26%

22%

17.1%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#30

#40

#50

#60

#80 #100

#140

#170

#200

Comments:

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

97%

71%

6.8%

Source: LDW21-GT53-GB-15-20 ft Sample#: B21-2152

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 15-Oct-21 Tested By: A. Eifrig

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

brown

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.055$   $D_{(10)} = 0.087$   $D_{(15)} = 0.106$   $D_{(30)} = 0.158$ % Gravel = 0.1% % Sand = 93.2% mm % Silt & Clay = 6.8% mm Liquid Limit = n/a mm  $D_{(50)} = 0.203$ mm Plasticity Index = n/a  $D_{(60)} = 0.226$ mm Sand Equivalent = n/a  $D_{(90)} = 0.376$ Oust Ratio = 3/43 Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a mm

Coeff. of Curvature,  $C_C = 1.27$ Coeff. of Uniformity,  $C_U = 2.59$ Fineness Modulus = 0.98 Plastic Limit = n/a Moisture %, as sampled = 27.7%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face = Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0$	).5/6 mm
					D	Oust Ratio =	3/43
				AS	STM C136, AS	TM D6913, A	ASTM C117
		Actual	Interpolated				
		7	Cumulative			_	
	e Size	Percent	Percent	Specs	Specs		
US	Metric	Passing	Passing	Max	Min		100%
12.00"	300.00		100%	100.0%	0.0%		
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%		90%
6.00"	150.00		100%	100.0%	0.0%		ł l
4.00"	100.00		100%	100.0%	0.0%		80%
3.00"	75.00		100%	100.0%	0.0%		80%
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%		70%
1.75"	45.00		100%	100.0%	0.0%		11
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%		60%
1.00"	25.00	100%	100%	100.0%	0.0%	20	
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%
5/8"	16.00		100%	100.0%	0.0%	96	30% FT
1/2"	12.50	100%	100%	100.0%	0.0%		
3/8"	9.50	100%	100%	100.0%	0.0%		40%
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		11
#8	2.36		100%	100.0%	0.0%		30%
#10	2.00	100%	100%	100.0%	0.0%		ł l
#16	1.18		100%	100.0%	0.0%		20%
#20	0.850	99%	99%	100.0%	0.0%		20%

98%

97%

78%

71%

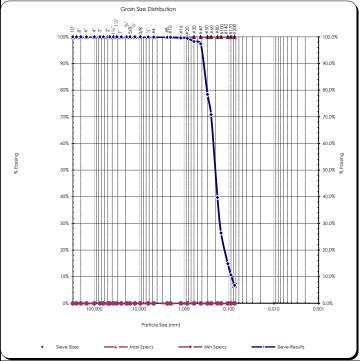
40%

26%

15%

11%

6.8%



0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

0.0%

Reviewed by: Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#80

#100

#140

#170

#200

Comments:

0.180

0.150

0.106

0.090

0.075

Meghan Blodgett-Carrillo

24%

6.2%

Source: LDW21-GT53-GB-20-23.5 ft Sample#: B21-2153

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 15-Oct-21

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.060$   $D_{(10)} = 0.091$   $D_{(15)} = 0.112$   $D_{(30)} = 0.166$   $D_{(50)} = 0.217$ % Gravel = 0.6%% Sand = 93.2% mm % Silt & Clay = 6.2% mm Liquid Limit = n/a mm mm Plasticity Index = n/a  $D_{(60)} = 0.243$ mm Sand Equivalent = n/a

 $\sqrt{6}$ , 1 Face = n/a2+ Faces = n/a Coeff. of Curvature,  $C_C = 1.24$ Coeff. of Uniformity,  $C_U = 2.67$ Fineness Modulus = 1.20

Plastic Limit = n/a Moisture %, as sampled = 29.9% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						D <sub>(90)</sub> =				racture	
						ust Ratio =			Frac	ture %	6, 2
		Actual Cumulative	Interpolated Cumulative	AS	STM C136, AS	IM D6913,	ASTM C117		(	Grain Siz	ze Di
Sieve	Size Metric	Percent Passing	Percent Passing	Specs Max	Specs Min		i⊃ io 100% <b>.◆◆</b>	\$ 4 th 6	7 Z :-	2/8/2	3 1
12.00"	300.00	rassing	100%	100.0%	0.0%	1	100%	~~~			T
10.00"	250.00		100%	100.0%	0.0%		F 1				
8.00"	200.00		100%	100.0%	0.0%		90%		₩-	-	##
6.00"	150.00		100%	100.0%	0.0%		ļ. ļ				
4.00"	100.00		100%	100.0%	0.0%						
3.00"	75.00		100%	100.0%	0.0%		80%		$^{\dagger\dagger}$	1	M
2.50"	63.00		100%	100.0%	0.0%						
2.00"	50.00	100%	100%	100.0%	0.0%		70%		Ш		Ш
1.75"	45.00		100%	100.0%	0.0%		1				
1.50"	37.50		100%	100.0%	0.0%		<u> </u>				
1.25"	31.50		100%	100.0%	0.0%		60%		++-	-	Ш
1.00"	25.00	100%	100%	100.0%	0.0%	g g	F 1				
3/4"	19.00	100%	100%	100.0%	0.0%	% Passing					
5/8"	16.00		100%	100.0%	0.0%	96	50%		Ш		Ш
1/2"	12.50	100%	100%	100.0%	0.0%						
3/8"	9.50	100%	100%	100.0%	0.0%		40%		##	4	Ш
1/4"	6.30		100%	100.0%	0.0%						
#4	4.75	99%	99%	100.0%	0.0%		11				
#8	2.36		99%	100.0%	0.0%		30%		++-	+	Ш
#10	2.00	99%	99%	100.0%	0.0%		ł l				
#16	1.18		97%	100.0%	0.0%		20%				Ш
#20	0.850	96%	96%	100.0%	0.0%		20% F		Ш		Ш
#30	0.600		92%	100.0%	0.0%		F 1				
#40	0.425	88%	88%	100.0%	0.0%		10%		##	+	Ш
#50	0.300		70%	100.0%	0.0%						
#60	0.250	63%	63%	100.0%	0.0%		1				

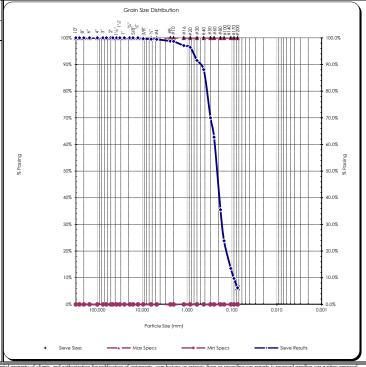
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Reviewed by:

36%

24%

14%

10%

6.2%



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

5/8"

1/2"

3/8"

1/4"

#4

#8

#10

#16

#20

#30

#40 #50

#60

#80

#100

#140

#170

#200

Comments:

Source: LDW21-GT53-GB-23.5-25 ft Sample#: B21-2154

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 15-Oct-21

Tested By: A. Eifrig

SM, Silty Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Dust Ratio = 39/79

Specifications No Specs

16.00

12.50

9.50

6.30

4.75

2.36

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

Sample Meets Specs? N/A

 $D_{(5)} = 0.008$   $D_{(10)} = 0.015$ % Gravel = 0.0%% Sand = 51.1% mm  $D_{(15)} = 0.023$ % Silt & Clay = 48.9% mm  $D_{(30)} = 0.046$ Liquid Limit = n/a mm  $D_{(50)} = 0.077$ mm Plasticity Index = n/a  $D_{(60)} = 0.098$ mm Sand Equivalent = n/a  $D_{(90)} = 0.186$ mm Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

Unified Soil Classification System, ASTM-2487

Coeff. of Curvature,  $C_C = 1.41$ Coeff. of Uniformity,  $C_U = 6.38$ Fineness Modulus = 0.17 Plastic Limit = n/aMoisture %, as sampled = 33.7%

Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

				2 %h,	1111 (150, 1151
		Actual Cumulative	Interpolated Cumulative		
Sieve	e Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%

100%

100%

100%

100%

100%

99%

98%

48.9%

100%

100%

100%

100%

100%

100%

100%

100%

100%

99%

99%

98%

98%

89%

85%

64%

56%

48.9%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

100.0%

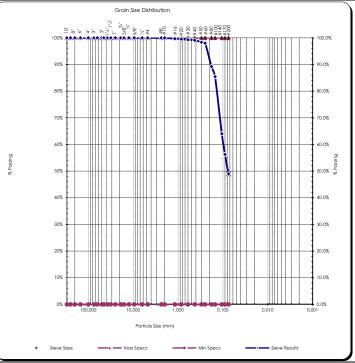
100.0%

100.0%

100.0%

100.0%

		st Ratio = 39/79	
AS	TM C136, AST	M D6913, ASTM C1	17
	Specs	È	2 %
	Min	100%	•
	0.0%		
	0.0%		
	0.0%	90% -	
	0.0%		
	0.0%	80% -	
	0.0%		
	0.0%		H
	0.0%	70% -	$\vdash$
	0.0%		Н
	0.0%		
	0.0%	60% -	П
	0.0%	gris	
	0.0%	50% -	Ш
	0.0%	Bc	
	0.0%		H
	0.0%	40% -	$\vdash$
	0.0%		Н
	0.0%		
	0.0%	30% -	П
	0.0%		
	0.0%	20% -	Ш
	0.0%		
	0.0%		
	0.0%	10% -	H
	0.0%		
	0.0%		Ц
	0.0%	0%	100
	0.0%		
	0.0%		
	0.0%		



0.0%

Reviewed by: Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233

Source: LDW21-GT53-GB-25-28.6 ft Sample#: B21-2155

Client: Anchor QEA

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 15-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications	
No Specs	

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.003 \\ \textbf{D}_{(10)} = 0.008 \\ \textbf{D}_{(15)} = 0.013 \\ \textbf{D}_{(30)} = 0.049 \\ \textbf{D}_{(50)} = 0.093 \\ \textbf{D}_{(60)} = 0.116 \\ \textbf{D}_{(90)} = 0.316 \\ \textbf{Partice} = 11/26 \end{array}$ % Gravel = 0.0%% Sand = 57.7% mm % Silt & Clay = 42.3% mm Liquid Limit = n/a mm mm Plasticity Index = n/a mm Sand Equivalent = n/a mm

Fracture %, 1 Face = n/a

Coeff. of Curvature,  $C_C = 2.78$ Coeff. of Uniformity,  $C_U = 15.33$ Fineness Modulus = 0.37

Plastic Limit = n/a Moisture %, as sampled = 34.9% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

					Dı	ast Ratio = 11/26	Fracture %, 2+ Faces = n/a Req'd Fracture %, 2+ Faces =
				AS	TM C136, AST	TM D6913, ASTM C1	117
			Interpolated				Grain Size Distribution
		1	Cumulative				
Sieve		Percent	Percent	Specs	Specs		20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
US	Metric	Passing	Passing	Max	Min	100%	**************************************
12.00"	300.00		100%	100.0%	0.0%		-
10.00"	250.00		100%	100.0%	0.0%		
8.00"	200.00		100%	100.0%	0.0%	90%	% <del>                                    </del>
6.00"	150.00		100%	100.0%	0.0%		-
4.00"	100.00		100%	100.0%	0.0%	80%	80.0%
3.00"	75.00		100%	100.0%	0.0%	30,0	`
2.50"	63.00		100%	100.0%	0.0%		
2.00"	50.00	100%	100%	100.0%	0.0%	70%	% <del>                                    </del>
1.75"	45.00		100%	100.0%	0.0%		
1.50"	37.50		100%	100.0%	0.0%		
1.25"	31.50		100%	100.0%	0.0%	60%	% 60.0%
1.00"	25.00	100%	100%	100.0%	0.0%	p p	-
3/4"	19.00	100%	100%	100.0%	0.0%	D	5.005 (4.00)
5/8"	16.00		100%	100.0%	0.0%	b6 20%	5 30.0% <sub>be</sub>
1/2"	12.50	100%	100%	100.0%	0.0%		- I
3/8"	9.50	100%	100%	100.0%	0.0%	40%	% 40.0%
1/4"	6.30		100%	100.0%	0.0%		
#4	4.75	100%	100%	100.0%	0.0%		
#8	2.36		100%	100.0%	0.0%	30%	30.0%
#10	2.00	100%	100%	100.0%	0.0%		
#16	1.18		100%	100.0%	0.0%	007	_ {
#20	0.850		100%	100.0%	0.0%	20%	75 20.0%
#30	0.600		100%	100.0%	0.0%		
#40	0.425	100%	100%	100.0%	0.0%	10%	% 10.0%
#50	0.300		89%	100.0%	0.0%		:
#60	0.250		84%	100.0%	0.0%		<u> </u>
#80	0.180		78%	100.0%	0.0%	0%	7 desde de de de de de de de de de de de de d
#100	0.150	75%	75%	100.0%	0.0%		100,000 10,000 1,000 0,100 0,010 0,001
#140	0.106		56%	100.0%	0.0%		Particle Size (mm)
#170	0.090		49%	100.0%	0.0%		
#200	0.075	42.3%	42.3%	100.0%	0.0%	+ Sieve S	e Sizes — Max Specs — Min Specs — Sieve Results
	Spears Engineering & Tec	1	U				

Reviewed by:



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 SM, Silty Sand Project #: 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 15-Oct-21 Sample Color Source: LDW21-GT53-GB-25-28.6 ft Tested By: A. Eifrig brown Sample#: B21-2155 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 2.48 Sp. Gr Sieve Analysis Sample Weight: 75.36 **Grain Size Distribution** Hydroscopic Moist.: 0.35% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 75.10 Size Passing Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading Passing Diameter 0.0519 mm 30.8% 100% 25.000 mm 1.0" 26.6% 3/4" 100% 19.000 mm 2 19 0.0374 mm 17 23.8% 0.0239 mm 5/8" 100% 16.000 mm 15 16.8% 0.0142 mm 1/2" 100% 12.500 mm 30 12.6% 0.0102 mm 3/8" 100% 9.500 mm 0.0073 mm 60 9.8% 1/4" 100% 6.300 mm 240 5.6% 0.0037 mm 100% 4.750 mm #4 #10 100%  $2.000\ mm$ 1440 2.8%  $0.0015 \ mm$ #20 100% 0.850 mm Liquid Limit: n/a % Gravel: 0.0% #40 100%  $0.425 \, mm$ % Sand: 57.7% Plastic Limit: n/a #100 75% 0.150 mm % Silt: 35.2% Plasticity Index: n/a #200 42.3%  $0.075 \ mm$ 41.8% 0.074 mm % Clay: 7.1% Silts 29.2% 0.050 mm 0.020 mm 20.9% 7.1% 0.005 mm Clays 3.4%  $0.002\ mm$ Colloids 1.8%  $0.001 \ mm$ **USDA Soil Textural Classification** Particle Size % Sand: 2.0 - 0.05 mm % Silt: 0.05 - 0.002 mm < 0.002 mm % Clay: **USDA Soil Textural Classification** Sandy Loam All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or **Comments:** 

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Source: LDW21-GT53-GB-28.6-30 ft

Sample#: B21-2156

#80

#100

#140

#170

#200

0.180

0.150

0.106

0.090

0.075

25%

6.8%

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 15-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP-SM, Poorly graded Sand with Silt

Sample Color: grayish-brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.055$   $D_{(10)} = 0.088$   $D_{(15)} = 0.109$   $D_{(30)} = 0.160$ % Gravel = 0.0%% Sand = 93.2% mm % Silt & Clay = 6.8% mm Liquid Limit = n/a mm  $D_{(50)} = 0.197$   $D_{(60)} = 0.216$   $D_{(90)} = 0.348$ mm Plasticity Index = n/a mm Sand Equivalent = n/a

mm Fracture %, 1 Face = n/a = n/a Coeff. of Curvature,  $C_C = 1.34$ Coeff. of Uniformity,  $C_U = 2.44$ Fineness Modulus = 0.92

Plastic Limit = n/a Moisture %, as sampled = 22.4% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

					D.,	$D_{(90)} = 0.348$ ist Ratio = 2/29	111111		0/ 2	
				A C				FE	racture %, 2	.+ Faces =
		Actual Cumulative	Interpolated Cumulative	AS	81 WI C136, AS1	M D6913, ASTN			Grain Size D	
Sieve	Size	Percent	Percent	Specs	Specs			. 5	3/8"	0 4
US	Metric	Passing	Passing	Max	Min		2 % ₹	• 4 9 9 ½	- 8, 8, 5,	# ## #
12.00"	300.00		100%	100.0%	0.0%					
10.00"	250.00		100%	100.0%	0.0%		l l			
8.00"	200.00		100%	100.0%	0.0%		90%		+	++++
6.00"	150.00		100%	100.0%	0.0%		- [ ]			
4.00"	100.00		100%	100.0%	0.0%					
3.00"	75.00		100%	100.0%	0.0%		80%			
2.50"	63.00		100%	100.0%	0.0%					
2.00"	50.00	100%	100%	100.0%	0.0%		70%			<b>           </b>
1.75"	45.00		100%	100.0%	0.0%					
1.50"	37.50		100%	100.0%	0.0%					
1.25"	31.50		100%	100.0%	0.0%		60%		++	-
1.00"	25.00	100%	100%	100.0%	0.0%	2	1			
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%			
5/8"	16.00		100%	100.0%	0.0%	P6	30%			
1/2"	12.50	100%	100%	100.0%	0.0%					
3/8"	9.50	100%	100%	100.0%	0.0%		40%			
1/4"	6.30		100%	100.0%	0.0%					
#4	4.75	100%	100%	100.0%	0.0%					
#8	2.36		100%	100.0%	0.0%		30%			
#10	2.00	100%	100%	100.0%	0.0%					
#16	1.18		100%	100.0%	0.0%		20%			
#20	0.850	100%	100%	100.0%	0.0%		10%			
#30	0.600		99%	100.0%	0.0%		-			
#40	0.425	99%	99%	100.0%	0.0%		10%	-	+	+++-
#50	0.300		84%	100.0%	0.0%					
#60	0.250	78%	78%	100.0%	0.0%				J_ L	

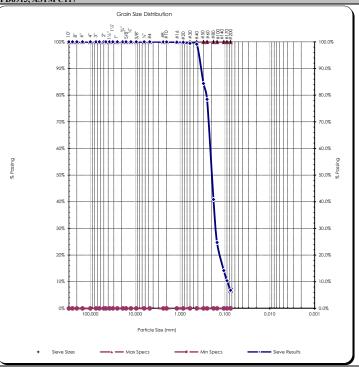
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Comments:		
Reviewed by	Nayh Baketaille	
reviewed by:	Meghan Blodgett-Carrillo	

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14%

10%

6.8%



Client:	Anchor QEA	Date:	October 25, 2021
Address:	21328 2nd Drive SE	Project:	Q.C Lower Duwamish Waterway
	Bothell, WA 98021	Project #:	21B233
Attn:	Garrett Timm	Sample #:	B21-2164-2174
Revised on:		Date sampled:	8-3-21 & 8-5-21

As requested MTC, Inc. has performed the following test(s) on the sample referenced above. The testing was performed in accordance with current applicable AASHTO or ASTM standards as indicated below. The results obtained in our laboratory were as follows below or on the attached pages:

	Test(s) Performed:	Test Results		Test(s) Performed:	Test Results
X	Sieve Analysis	Please See Attached Reports		Sulfate Soundness	
	Proctor	Trease see Tituenea Reports		Bulk Density & Voids	
	Sand Equivalent			WSDOT Degradation	
	Fracture Count			LA Abrasion	
X	Moisture Content	Please See Attached Report	X	Direct Shear	Please See Attached Reports
	Specific Gravity, Coarse		X	Specific Gravity, Soils	Please See Attached Reports
	Specific Gravity, Fine				
X	Hydrometer Analysis	Please See Attached Reports			
X	Atterberg Limits	Please See Attached Reports			

If you have any questions concerning the test results, the procedures used, or if we can be of any further assistance please call on us at the number below.

Respectfully Submitted, Meghan Blodgett-Carrillo

WABO Supervising Laboratory Technician



#### **Moisture Content - ASTM C566, ASTM D2216**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
<b>Project #:</b> 21B233	<u> </u>
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 18, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Wet + Tare	Dry + Tare	Wgt. Of Moisture	Wgt. Of Soil	% Moisture
B21-2164	LDW21-GT48-SPT-25-26.5 ft	233.1	1048.4	832.6	215.8	599.5	36.0%
B21-2165	LDW21-GT48-SPT-30-31.5 ft	182.3	1308.3	1004.2	304.1	821.9	37.0%
B21-2166	LDW21-GT53-SPT-10-11.5 ft	260.3	653.6	537.2	116.4	276.9	42.0%
B21-2167	LDW21-GT53-SPT-15-16.5 ft	270.1	1295.8	1089.8	206.0	819.7	25.1%
B21-2168	LDW21-GT53-SPT-20-21.5 ft	266.3	1049.6	853.9	195.7	587.6	33.3%
B21-2169	LDW21-GT53-SPT-25-26.5 ft	360.2	1271.6	1074.8	196.8	714.6	27.5%
B21-2170	LDW21-GT41-GH-0-1.3 ft	359.4	527.4	488.8	38.6	129.4	29.8%
B21-2171	LDW21-GT41-GH-1.3-2 ft	354.2	2105.6	1668.8	436.8	1314.6	33.2%
B21-2172	LWD21-GT42-GH-0-0.3 ft	341.5	409.5	366.7	42.8	25.2	169.8%
B21-2173	LWD21-GT42-GH-0.3-1.5 ft	356.9	581.1	525.1	56.0	168.2	33.3%
B21-2174	LWD21-GT42-GH-1.5-2.3 ft	224.0	439.0	407.7	31.3	183.7	17.0%
	_						
							·

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:



#### **Specific Gravity - ASTM D854**

Project: Q.C Lower Duwamish Waterway	Client: Anchor QEA
Project #: 21B233	
Date Received: July 29, 2021	Sampled by: Client
Date Tested: October 18, 2021	Tested by: A. Eifrig

Sample #	Location	Tare	Dry Soil + Tare	Mass of Dry Soil	Pycno ID	Mass of Pycno	Volume of Pycno	Density of Water @ Tx	Mass of Pycno filled w/ water & soils	Mass of Pycno filled w/ water	*C	Soils	Factor	SpG
B21-2170	LDW21-GT41-GH-0-1.3 ft	416.85	491.39	74.5	TSA-020	195.0	499.5	0.99850	738.69	693.77	18.5	2.516483	1.00030	2.5172379
B21-2174	LDW21-GT42-GH-1.5-2.3 ft	415.34	491.53	76.2	TSA-015	187.6	499.5	0.99835	733.52	686.28	19.4	2.632154	1.00014	2.6325225
									ļ					
								<del>                                     </del>	<del> </del>					
							1	<del> </del>	1	1				
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All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Reviewed by:

Meghan Blodgett-Carrillo



Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#80

#140

#170

#200

0.180

0.150

0.106

0.090

0.075

Source: LDW21-GT41-GH-0-1.3 ft Sample#: B21-2170

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 18-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.008$   $D_{(10)} = 0.022$   $D_{(15)} = 0.068$ % Gravel = 0.0%% Sand = 84.3% mm % Silt & Clay = 15.7% mm  $D_{(30)} = 0.152$ Liquid Limit = n/a mm  $D_{(50)} = 0.264$ mm Plasticity Index = n/a  $D_{(60)} = 0.320$ mm Sand Equivalent = n/a  $D_{(90)} = 1.271$ Dust Ratio = 1/5 mm

Fracture %, 1 Face = n/a Fracture %, 2+ Faces = n/a

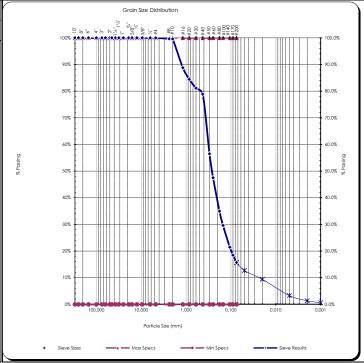
Coeff. of Curvature,  $C_C = 3.31$ Coeff. of Uniformity,  $C_U = 14.63$ Fineness Modulus = 1.44 Plastic Limit = n/a

Moisture %, as sampled = 29.8% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

STM D6913, ASTM C117

					Di
				AS	STM C136, AST
		Actual	Interpolated		
		,	Cumulative		
Sieve	Size	Percent	Percent	Specs	Specs
US	Metric	Passing	Passing	Max	Min
12.00"	300.00		100%	100.0%	0.0%
10.00"	250.00		100%	100.0%	0.0%
8.00"	200.00		100%	100.0%	0.0%
6.00"	150.00		100%	100.0%	0.0%
4.00"	100.00		100%	100.0%	0.0%
3.00"	75.00		100%	100.0%	0.0%
2.50"	63.00		100%	100.0%	0.0%
2.00"	50.00	100%	100%	100.0%	0.0%
1.75"	45.00		100%	100.0%	0.0%
1.50"	37.50		100%	100.0%	0.0%
1.25"	31.50		100%	100.0%	0.0%
1.00"	25.00	100%	100%	100.0%	0.0%
3/4"	19.00	100%	100%	100.0%	0.0%
5/8"	16.00		100%	100.0%	0.0%
1/2"	12.50	100%	100%	100.0%	0.0%
3/8"	9.50	100%	100%	100.0%	0.0%
1/4"	6.30		100%	100.0%	0.0%
#4	4.75	100%	100%	100.0%	0.0%
#8	2.36		100%	100.0%	0.0%
#10	2.00	100%	100%	100.0%	0.0%
#16	1.18		89%	100.0%	0.0%
#20	0.850		84%	100.0%	0.0%
#30	0.600		81%	100.0%	0.0%
#40	0.425	79%	79%	100.0%	0.0%
#50	0.300		56%	100.0%	0.0%
#60	0.250		48%	100.0%	0.0%
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Comments: Reviewed by: \_ Meghan Blodgett-Carrillo

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15.7%

35%

30%

21%

19%

15.7%

100.0%

100.0%

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100.0%



# **Hydrometer Report**

Date Received: 29-Jul-21 Unified Soil Classification System, ASTM-2487 Project: Q.C. - Lower Duwamish Waterway Sampled By: Client SM, Silty Sand Project #: 21B233 Client: Anchor QEA Date Tested: 18-Oct-21 Sample Color Source: LDW21-GT41-GH-0-1.3 ft Tested By: A. Eifrig brown Sample#: B21-2170 ASTM D7928, HYDROMETER ANALYSIS ASTM D6913 2.52 Sp Gr: Sieve Analysis Sample Weight: 100.37 **Grain Size Distribution** Hydroscopic Moist.: 0.83% Soils Particle Sieve Percent ACCREDITED Adj. Sample Wgt: 99.54 Size **Passing** Diameter 100% 75.000 mm 2.0" 100% 50.000 mm Hydrometer Reading Soils Particle 1.5" 100% 37.500 mm Corrected Percent 1.25" 100% 31.500 mm Minutes Reading **Passing** Diameter 13.4% 0.0539 mm 100% 25.000 mm 13 1.0" 0.0385 mm 3/4" 100% 19.000 mm 2 11.5 11.9% 10.5 10.8%  $0.0245\ mm$ 5/8" 100% 16.000 mm 15 7.5 7.7% 0.0144 mm 1/2" 100%12.500 mm 30 6.5 6.7% 0.0102 mm 3/8" 100% 9.500 mm 0.0073 mm 60 4.5 4.6% 1/4" 100% 6.300 mm

00	1.5	1.070	0.0075 111111	1/1	10070	0.500 11111
240	2.5	2.6%	0.0037 mm	#4	100%	4.750 mm
1440	1	1.0%	0.0015 mm	#10	100%	2.000 mm
				#20	84%	0.850 mm
% Gravel:	0.0%		Liquid Limit: n/a	#40	79%	0.425 mm
% Sand:	84.3%		Plastic Limit: n/a	#100	30%	0.150 mm
% Silt:	12.4%	Pl	asticity Index: n/a	#200	15.7%	0.075 mm
% Clay:	3.3%			Silts	15.6%	0.074 mm
					12.7%	0.050 mm
					9.4%	0.020 mm
				Clays	3.3%	0.005 mm

1.4%

0.7%

Colloids

 $0.002\ mm$ 

0.001 mm

#### **USDA Soil Textural Classification**

 % Sand:
 2.0 - 0.05 mm

 % Silt:
 0.05 - 0.002 mm

 % Clay:
 < 0.002 mm</td>

#### **USDA Soil Textural Classification**

Sand

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Comments:		
D : 11	Maybe Chilget wills	
Reviewed by:	Meghan Blodgett-Carrillo	

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

Project Number:	21B233
Laboratory Sample ID:	B21-2170
Sample Date:	8/3/2021
Test Date:	10/18/2021
Technician:	M. Carrillo

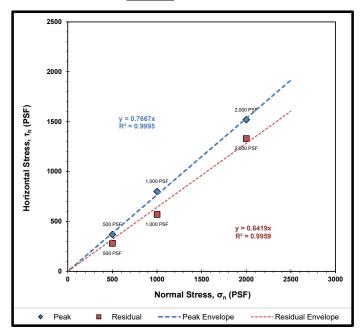
Sample Source: LDW21-GT41-GH-0-1.3 ft
Visual Soil Description: brown sand with silt and gravel
Type of Specimen: Remolded Cylindrical Shear Box
Specimen Diameter (in): 2.5

Summary of Sample	e Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	28.1	
	Initial	Post-Consolidation
Dry Density (PCF):	109.2	111.5
Void Ratio:	0.543	0.510
Porosity (%):	35.2	33.8
Degree of Saturation (%):	saturated	saturated

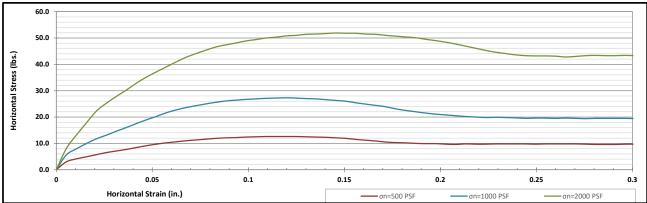
Summary of Sample	Data:	σ <sub>n</sub> =1000 PSF			
Initial Moisture Content (%):	27.3				
	Initial	Post-Consolidation			
Dry Density (PCF):	110.2	115.1			
Void Ratio:	0.529	0.464			
Porosity (%):	34.6	31.7			
Degree of Saturation (%):	saturated	saturated			

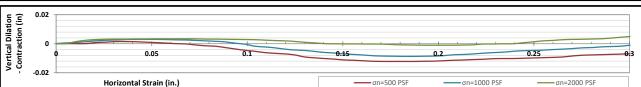
Summary of Sampl	e Data:	σ <sub>n</sub> =2000 PSF			
Initial Moisture Content (%):	28.4				
	Initial	Post-Consolidation			
Dry Density (PCF):	109.1	119.9			
Void Ratio:	0.545	0.405			
Porosity (%):	35.3	28.8			
Degree of Saturation (%):	saturated	saturated			

ESTIMATED STRENGTH PARAMETERS								
	PEAK	RESIDUAL						
Angle of Internal Friction, φ (°):	37	33						
Cohesion (PSF):	0	0						



Failure Envelope Test Values:							
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000				
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	370	800	1520				
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	280	570	1330				





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

Sample#: B21-2171

Source: LDW21-GT41-GH-1.3-2.0 ft

Date Received: 29-Jul-21 Sampled By: Client

Date Tested: 18-Oct-21 Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SM, Silty Sand Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications No Specs

Sample Meets Specs? N/A

 $\begin{array}{l} \textbf{D}_{(5)} = 0.022 \\ \textbf{D}_{(10)} = 0.044 \\ \textbf{D}_{(15)} = 0.066 \\ \textbf{D}_{(30)} = 0.170 \\ \textbf{D}_{(50)} = 0.277 \\ \textbf{D}_{(60)} = 0.330 \\ \textbf{D}_{(90)} = 0.824 \\ \textbf{Partia} = 7/22 \end{array}$ % Gravel = 1.1% % Sand = 81.8% mm % Silt & Clay = 17.1% mm Liquid Limit = n/a mm Plasticity Index = n/a mm Sand Equivalent = n/a

Fracture %, 1 Face = n/a
Fracture %, 2+ Faces = n/a mm Dust Ratio = 7/32

Coeff. of Curvature,  $C_C = 2.00$ Coeff. of Uniformity,  $C_U = 7.51$ Fineness Modulus = 1.48

Plastic Limit = n/a Moisture %, as sampled = 33.2% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

						ust Ratio = 7/32	Fracture %, 2+ Faces =	n/a Re	q'd Fracture %, 2	+ Faces =
		Actual	Interpolated	AS	TM C136, AST	TM D6913, ASTM C117				
			Cumulative				Grain Size Distribution			
Sieve	Size	Percent	Percent	Specs	Specs	ا ا	33.78. 1.72.	83 <del>2</del> 58888888888		
US	Metric	Passing	Passing	Max	Min	100%	* 5 2 2 2 2 3 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4	# # # # # # # # # # # # # # # # # # # #		
12.00"	300.00		100%	100.0%	0.0%					1 1
10.00"	250.00		100%	100.0%	0.0%					1 1
8.00"	200.00		100%	100.0%	0.0%	90%		î de la companya de la companya de la companya de la companya de la companya de la companya de la companya de		90.0%
6.00"	150.00		100%	100.0%	0.0%	<u> </u>		<b>                                     </b>		1 1
4.00"	100.00		100%	100.0%	0.0%	80%		N		80.0%
3.00"	75.00		100%	100.0%	0.0%	80%				00.0%
2.50"	63.00		100%	100.0%	0.0%					1 1
2.00"	50.00	100%	100%	100.0%	0.0%	70%				70.0%
1.75"	45.00		100%	100.0%	0.0%					1
1.50"	37.50		100%	100.0%	0.0%					
1.25"	31.50		100%	100.0%	0.0%	60%		### <b>#</b>		60.0%
1.00"	25.00	100%	100%	100.0%	0.0%					50.0%
3/4"	19.00	100%	100%	100.0%	0.0%	Di 50 80 80 80 80				1 50 0%
5/8"	16.00		100%	100.0%	0.0%	be 30%				1 30.00
1/2"	12.50	100%	100%	100.0%	0.0%			1		1 1
3/8"	9.50	100%	100%	100.0%	0.0%	40%		₩₩₩₩		40.0%
1/4"	6.30		99%	100.0%	0.0%					
#4	4.75	99%	99%	100.0%	0.0%					
#8	2.36		97%	100.0%	0.0%	30%				30.0%
#10	2.00	97%	97%	100.0%	0.0%					1
#16	1.18		92%	100.0%	0.0%	20%		IIII N		20.0%
#20	0.850	91%	91%	100.0%	0.0%	10,0				1 1
#30	0.600		83%	100.0%	0.0%	[				1 1
#40	0.425	78%	78%	100.0%	0.0%	10%		<del>                                     </del>	<del>                                     </del>	10.0%
#50	0.300		54%	100.0%	0.0%					
#60	0.250	45%	45%	100.0%	0.0%					
#80	0.180		32%	100.0%	0.0%	0%	0.000 10.000 1.0	00 0.100	0.010	0.0%
#100	0.150	26%	26%	100.0%	0.0%					
#140	0.106		21%	100.0%	0.0%		Particle Size (mm)			
#170	0.090		19%	100.0%	0.0%					
#200	0.075	17.1%	17.1%	100.0%	0.0%	+ Sieve Sizes	—▲ — Max Specs —	→ Min Specs	Sieve Resi	ults

Reviewed by:



### ASTM D4318 - Liquid Limit, Plastic Limit and Plasticity Index of Soils

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification Silt with Organics **Project #:** 21B233 Sampled By: Client Client: Anchor QEA Date Tested: 18-Oct-21 Sample Color Source: LDW21-GT42-GH-0-0.3 ft Tested By: A. Eifrig Sample #: B21-2172 **Liquid Limit Determination** Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Unable to establish liquid limit Weight of Pan: Liquid Limit @ 25 Blows: Weight of Dry Soils: N/A Weight of Moisture: Plastic Limit: N/A % Moisture: Plasticity Index, I<sub>P</sub>: N/A Number of Blows: Weight of Wet Soils + Pan: Weight of Dry Soils + Pan: Cannot determined plastic limit Weight of Pan: Weight of Dry Soils: Weight of Moisture: % Moisture: **Liquid Limit Plasticity Chart** 0.7 100% 90% 0.6 0.5 Plasticity Index 60% 0.3 50% 0.2 0.1 20% 10% 50% **Liquid Limit** 10 100

variestus appropury o vicua nocamos ani materias tested. As a matan protection o circus, tie punic ani ourserves, an reports are summer as the confineman property of circus, ani autorization to punication of saucinetias, concursos of extracts from or regarding our reports is reserved pending our writer approval.

Comments: Liquid limit cannot be established as the material displays rapid dilation. At lower moistures the material does not spread into the cup without tearing the soil cake. Plastic limit cannot be determined as the sample does not roll down to 1/8" threads before cracking or crumbling. Non-plastic.

Reviewed by:



Project: Q.C. - Lower Duwamish Waterway

Project #: 21B233 Client: Anchor QEA

#10

#16

#20

#30

#40

#50

#60

#80

#100

#140

#170

#200

Comments:

Reviewed by:

2.00

1.18

0.850

0.600

0.425

0.300

0.250

0.180

0.150

0.106

0.090

0.075

**Source:** LDW21-GT42-GH-0.3-1.5 ft **Sample#:** B21-2173

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 18-Oct-21 Tested By: A. Eifrig Visual Identification Sandy Silt with Clay Sample Color: brown



Coeff. of Curvature,  $C_C = 0.79$ Coeff. of Uniformity,  $C_U = 37.10$ 

Fineness Modulus = 0.92

#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

Sample Meets Specs? N/A

 $D_{(5)} = 0.000$   $D_{(10)} = 0.001$ % Gravel = 4.1%% Sand = 32.0% mm  $D_{(15)} = 0.002$ % Silt & Clay = 63.8% mm  $D_{(30)} = 0.005$ Liquid Limit = n/a mm  $D_{(50)} = 0.017$ mm Plasticity Index = n/a  $D_{(60)} = 0.037$ mm Sand Equivalent = n/a

Plastic Limit = n/a Moisture %, as sampled = 33.3% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

 $D_{(90)} = 1.643$  mm Fracture %, 1 Face = n/a Req'd Fracture %, 1 Face = Dust Ratio = 39/50 Fracture %, 2+ Faces = n/a Req'd Fracture %, 2+ Faces =

ASTM C136, ASTM D6913, ASTM C117 Actual Interpolated Cumulative Cumulative Sieve Size Percent Specs Percent Specs Min Metric Passing Max Passing 12.00 100.0% 10.00" 250.00 100% 100.0% 0.0% 100% 100.0% 200.00 0.0% 8.00" 6.00" 150.00 100% 100.0% 0.0% 4.00" 100.00 100% 100.0% 0.0% 3.00" 75.00 100% 100.0% 0.0% 2.50" 63.00 100% 100.0% 0.0% 2.00" 50.00 100% 100% 100.0% 0.0% 45.00 37.50 1.75" 100% 100.0% 0.0% 1.50" 100% 100.0% 0.0% 1.25" 100% 100.0% 0.0% 31.50 1.00" 25.00 100% 100% 100.0% 0.0% 3/4" 19.00 100% 100.0% 0.0% 100% 5/8" 16.00 100% 100.0% 0.0% 1/2" 12.50 100% 100% 100.0% 0.0%3/8" 9.50 99% 99% 100.0% 0.0% 97% 1/4" 100.0% 0.0% 6.30 4.75 100.0% 96% 96% 0.0% #4 93% 100.0% 0.0% 2.36 #8

92%

87%

85%

83%

82%

78%

76%

74%

73%

67%

66%

63.8%

100.0%

100.0%

100.0%

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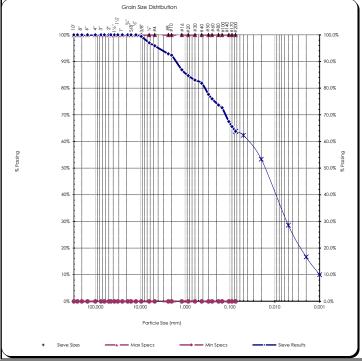
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Il results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval

Manh Blakget and b

82%

63.8%



# **Hydrometer Report**

Project: Q.C. - Lower Duwamish Waterway Date Received: 29-Jul-21 Visual Identification **Project #:** 21B233 Sampled By: Client Sandy Silt with Clay

Project #:				i By: Client	Sandy Silt With	Clay		
Client: Anchor QEA				sted: 18-Oct-21	Sample Color			
Source:	LDW21-GT4	2-GH-0.3-1.5 ft	Testeo	l By: A. Eifrig	brown			
Sample#:	B21-2173							
A	STM D792	8, HYDROM		ASTM 1	D6913			
Assumed Sp Gr:	2.65					Sieve Ar	nalysis	
Sample Weight:	75.38	grams				Grain Size D	istribution	
Hydroscopic Moist.:	1.68%				Sieve	Percent	Soils Particle	
Adj. Sample Wgt :	74.13	grams		ACCREDITED	Size	Passing	Diameter	
				Certificate #: 1366.01	3.0"	100%	75.000 mm	
Hydrometer					2.0"	100%	50.000 mm	
Reading	Corrected	Percent	Soils Particle		1.5"	100%	37.500 mm	
Minutes	Reading	Passing	Diameter		1.25"	100%	31.500 mm	
1	49	61.1%	0.0393 mm		1.0"	100%	25.000 mm	
2	45	56.1%	0.0288 mm		3/4"	100%	19.000 mm	
5	42.5	53.0%	0.0187 mm		5/8"	100%	16.000 mm	
15	34.5	43.0%	0.0115 mm		1/2"	100%	12.500 mm	
30	30.5	38.0%	0.0084 mm		3/8"	99%	9.500 mm	
60	26	32.4%	0.0061 mm		1/4"	97%	6.300 mm	
240	18	22.4%	0.0032 mm		#4	96%	4.750 mm	
1440	11	13.7%	0.0014 mm		#10	92%	2.000 mm	
					#20	85%	0.850 mm	
% Gravel:	4.1%		L <b>iquid Limit:</b> n/a		#40	82%	0.425 mm	
% Sand:	32.0%		Plastic Limit: n/a		#100	73%	0.150 mm	
% Silt:	35.2%	Pla	sticity Index: n/a		#200	63.8%	0.075 mm	
% Clay:	28.6%				Silts	63.8%	0.074 mm	
						62.3%	0.050 mm	
						53.4%	0.020 mm	
					Clays	28.6%	0.005 mm	
					a	16.7%	0.002 mm	
					Colloids	10.0%	0.001 mm	
	USDA S	Soil Textural (	Classification					
		Particle Size			1			
% Sand:		2.0 - 0.05 mm						
% Silt:		0.05 - 0.002 mm						
% Clay:		< 0.002 mm						
	USDA S	Soil Textural (	Classification					
		Loam						

All results apply only to actual locations and materials tested. As a mutual protection to clients, the public and ourselves, all reports are submitted as the confidential property of clients, and authorization for publication of statements, conclusions or extracts from or regarding our reports is reserved pending our written approval.

Comments:			
	1 100 D.M.		
Reviewed by:	Magh Bladgettarillo		
	Meghan Blodgett-Carrillo		

#### **Direct Shear Test Results:**

#### **ASTM D-3080**



Project: Q.C. - Lower Duwamish Waterway

| Project Number: 21B233 | B21-2173 | B21-2173 | Sample Date: 8/3/2021 | Test Date: 10-19-21 through 10-21-21 | Technician: M. Carrillo

 Sample Source:
 LDW21-GT42-GH-0.3-1.5 ft

 Visual Soil Description:
 brown clay with silt

 Type of Specimen:
 Remolded Cylindrical Shear Box

 Specimen Diameter (in):
 2.5

 Specimen Height (in):
 1

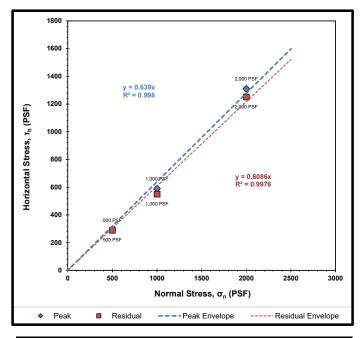
Rate of Strain (in/min): 0.0012
Estimated Specific Gravity of Solids: 2.65

Summary of Sample	Data:	σ <sub>n</sub> =500 PSF
Initial Moisture Content (%):	34.0	
	Initial	Post-Consolidation
Dry Density (PCF):	102.5	106.8
Void Ratio:	0.644	0.578
Porosity (%):	39.2	36.6
Degree of Saturation (%):	saturated	saturated

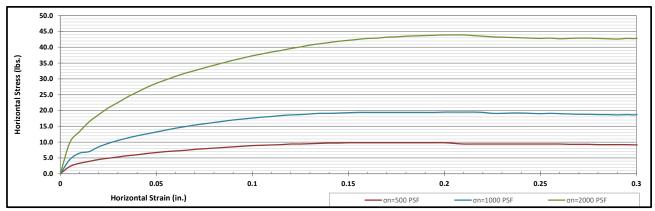
Summary of Samp	le Data:	σ <sub>n</sub> =1000 PSF
Initial Moisture Content (%):	31.5	
	Initial	Post-Consolidation
Dry Density (PCF):	104.6	114.9
Void Ratio:	0.611	0.467
Porosity (%):	37.9	31.8
Degree of Saturation (%):	saturated	saturated

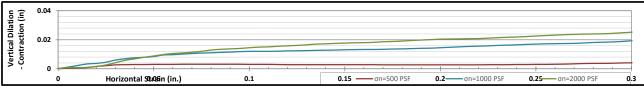
Summary of Sample	Data:	σ <sub>n</sub> =2000 PSF
Initial Moisture Content (%):	28.9	
	Initial	Post-Consolidation
Dry Density (PCF):	107.0	120.1
Void Ratio:	0.574	0.403
Porosity (%):	36.5	28.7
Degree of Saturation (%):	saturated	saturated

ESTIMATED STR	ESTIMATED STRENGTH PARAMETERS							
	PEAK	RESIDUAL						
Angle of Internal Friction, φ (°):	33	31						
Cohesion (PSF):	0	0						



Failure Envelope Test Values:									
Normal Stress, σ <sub>n</sub> (PSF):	500	1000	2000						
Peak Horizontal Stress, τ <sub>h</sub> (PSF):	290	590	1310						
Residual Horizontal Stress, τ <sub>h</sub> (PSF):	290	550	1250						





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Project: Q.C. - Lower Duwamish Waterway

**Project #:** 21B233 Client: Anchor QEA

#170

#200

0.090

0.075

4.6%

Source: LDW21-GT42-GH-1.5-2.3 ft

Sample#: B21-2174

Date Received: 29-Jul-21 Sampled By: Client Date Tested: 18-Oct-21

Tested By: A. Eifrig

Unified Soil Classification System, ASTM-2487

SP, Poorly graded Sand

Sample Color:

brown



#### ASTM D2216, ASTM D2419, ASTM D4318, ASTM D5281

Specifications
No Specs

Sample Meets Specs ? N/A

 $D_{(5)} = 0.079$   $D_{(10)} = 0.130$   $D_{(15)} = 0.167$   $D_{(30)} = 0.251$   $D_{(50)} = 0.334$ % Gravel = 0.0%% Sand = 95.4% mm % Silt & Clay = 4.6% mm Liquid Limit = n/a mm mm Plasticity Index = n/a  $D_{(60)} = 0.376$ mm

Sand Equivalent = n/a racture %, 1 Face = n/a aces = n/a Coeff. of Curvature,  $C_C = 1.29$ Coeff. of Uniformity,  $C_U = 2.90$ Fineness Modulus = 1.67

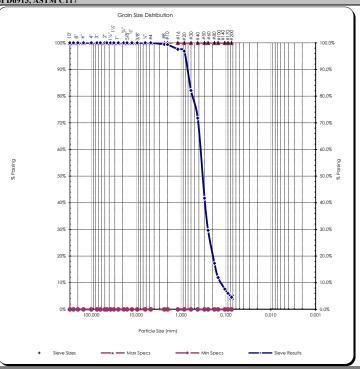
Plastic Limit = n/a Moisture %, as sampled = 17.0% Req'd Sand Equivalent = Req'd Fracture %, 1 Face =

Reg'd Fracture %, 2+ Faces =

						$D_{(90)} = 0.733$	mm	F	racture '	%, 1	Fa
					D	ust Ratio = 3/47		Frac	cture %,	, 2+ F	ac
				AS	STM C136, AS	TM D6913, ASTM	C117				
		Actual Cumulative	Interpolated Cumulative						Grain Size	Distrib	ottic
Sieve	Size	Percent	Percent	Specs	Specs		i.	7 2 3 4 7 2 3 4	\$		~c
US	Metric	Passing	Passing	Max	Min	1	್ ಚೆ ಆ ≖.♦.♦.♦.೩ ೫001	<b>◆^**</b>	- 15 5 *******	≥ ¥ ••••••••••••••••••••••••••••••••••••	##
12.00"	300.00		100%	100.0%	0.0%	1				m	
10.00"	250.00		100%	100.0%	0.0%						
8.00"	200.00		100%	100.0%	0.0%		90%				Н
6.00"	150.00		100%	100.0%	0.0%						
4.00"	100.00		100%	100.0%	0.0%						
3.00"	75.00		100%	100.0%	0.0%		80%			Ш	П
2.50"	63.00		100%	100.0%	0.0%						
2.00"	50.00	100%	100%	100.0%	0.0%		70%			ШШ	Ш
1.75"	45.00		100%	100.0%	0.0%						
1.50"	37.50		100%	100.0%	0.0%						
1.25"	31.50		100%	100.0%	0.0%		60%			-	Н
1.00"	25.00	100%	100%	100.0%	0.0%	2					
3/4"	19.00	100%	100%	100.0%	0.0%	% Possing	50%				
5/8"	16.00		100%	100.0%	0.0%	PG	50%			Ш	П
1/2"	12.50	100%	100%	100.0%	0.0%						
3/8"	9.50	100%	100%	100.0%	0.0%		40%		4	ШШ	Ш
1/4"	6.30		100%	100.0%	0.0%						
#4	4.75	100%	100%	100.0%	0.0%						
#8	2.36		99%	100.0%	0.0%		30%			++++	Н
#10	2.00	99%	99%	100.0%	0.0%		<b>+</b>				
#16	1.18		98%	100.0%	0.0%		20%				
#20	0.850	97%	97%	100.0%	0.0%		20%				П
#30	0.600		82%	100.0%	0.0%						
#40	0.425	72%	72%	100.0%	0.0%		10%		+	Щ.	Ш
#50	0.300		42%	100.0%	0.0%						
#60	0.250	30%	30%	100.0%	0.0%						
#80	0.180		17%	100.0%	0.0%		0%	0.000	10.000		-01
#100	0.150	12%	12%	100.0%	0.0%		100		10.000		
#140	0.106		8%	100.0%	0.0%				Po	article Si	ze (ı
W170	0.000	1	60/	100.00/	0.00/	ll .					

100.0%

100.0%



0.0%

0.0%

Comments:		
Reviewed by:	Nagh Chilget Brills	
	Meghan Blodgett-Carrillo	

6%

4.6%

# Attachment C Supplemental Geotechnical Information by Others

Table C-1
Historical Geotechnical Investigations and Geologic Information

File Title	Identification No. <sup>1</sup>	River Mile	Document Title	Document type	Date Document Creation	Project Location	Sample Types/Report Info	Author
RM 2.9_Boeing_east bank	1	2.9	n/a	partial report/figures	9.11.1990	1135 S. Webster Street (Boeing Company), east bank	CPT logs, MW logs, grain size analysis, boring logs	Geoengineers
Boeing Plant 2_east bank	2, 8, 9, 10	3.1-3.5	Appendix C: Geotechnical Engineering Report, Habitat Project	report	10.2012	Boeing Plant 2 (Seattle/Tukwila)	Subsurface conditions, seismic conditions, liquefaction and lateral spreading analysis, slope stability analysis, shoreline excavation and dredging	AMEC, Floyd Snider, Dalton Olmsted & Fuglevand
RM 3.1-3.3 Boeing Technology Complex_east bank	3	3.1-3.3	Report of Geotechnical Investigation, Proposed Boeing Materials Technology Complex	report	8.13.1992	Boeing North Duwamish Campus, East Bank	Site conditions, subsurface/groundwater conditions, CPT logs, grain size, excavations, pile foundations, seismic aspects	Dames & Moore
RM 3.02_S Monroe St_west bank	4	3.12	Site plan	figures	8.22.1986	South Monroe Street, southwest side Duwamish	Site plan, 2 boring logs with blow counts, observation well install	Geoengineers
RM 3.3-3.6_Boeing Plant 2_east bank	5	3.3-3.6	Boeing Plant 2 RFI	figures (site thickness map, boring logs)	07.3.1997	Boeing Plant 2 (E Marginal Way S and 16th Ave S)	Boring logs, silt thickness and till units	Weston
RM 3_South Park Neighborhood_west bank	6	3.3	South Park Neighborhood Development Program Subsurface Investigations	report	8.1973	South Park Neighborhood	11 test boings (HSA), SPTs, 2 observation well installs, cross sections	Shannon & Wilson
RM 3.33-South Park Bridge	7	3.3	South Park Bridge Replacement Volume 3: Geotechnical Report	compiled reports	8.2007	South Park Bridge	Full geotechnical study (boring logs, seismic, liquefaction, soil motion, soil surface response spectra, shear wave velocity, rock input, etc.)	PB Americas, Shannon & Wilson
Terminal 117 Site Restoration GT Report - Rev 1	11	3.55	Terminal 117 Site Restoration	report	05.07.2014	Terminal 117: Duwamish waterway to the east, Dallas Avenue to the south. South Park marina to the north, parking lot to the west. (Flat around 15 ft)	Subsurface/surface conditions, GW, SPTs, earthquake engineering, liquefaction, design soil parameters, slope stability, ground improvement, shallow foundations, pile design, retaining walls, site development and earthwork	Geoengineers
RM 4.4_Transmission Towers	12	3.5-3.6	Geotechnical and Environmental Engineering Design Study Proposed Duwamish Transmission Towers	report	9.19.2003	Boeing Plant 2. Each bank of the Duwamish River south of the 14th Street bridge (south park bridge)	2 borings, existing geotechnical data, soil/GW subsurface, engineering analysis: seismic, foundations, deep foundations, SPTs	Hart Crowser
RM 3.6 Basin Oil_west bank	13	3.6	Geotechnical Engineering Study for Basin Oil	partial report/logs	02.07.1994	Basin Oil: 8661 Dallas Avenue South, Seattle	Site map and log	Lorilla Engineering
RM 3.6 _Dallas Ave S_west bank	14	3.6	Geotechnical Memorandum	memo	06.10.2014	Dallas Avenue South	10 test pits, 10 pilot infiltration tests, includes figures and logs, grain size	Seattle Public Utilities Geotechnical Engineering
RM 3.6_Jorgensen Forge MWs_east bank	15	3.6	Jorgensen Forge Boring Logs	figure/logs	12.05.1994	8531 E. Marginal Way, Seattle	2 HSA borings to 30 ft	SECOR
Final Inv Data Summ Rpt_021306	16	3.65	Final Investigation Data Summary Report Jorgensen Forge Facility	report	2.13.2006	Jorgenson: 8531 East Marginal Way South	Surface/subsurface samples analyzed for grain size (no deviations)	Farallon Consulting and Anchor Environmental

File Title	Identification No. <sup>1</sup>	River Mile	Document Title	Document type	Date Document Creation	Project Location	Sample Types/Report Info	Author
RM 3.7_Boeing S Park Facility_west bank	17	3.7	Report of Foundation Investigation	figures/logs	06.17.1980	1420 S. Trenton Street	7 boring logs and figures	Dames & Moore
Boeing Plant 2 CPT Locations	18	3.7	CPT Locations	figure	02.09.2015	POS Parcel Boeing Isaacson	CPTs (up to 60 feet bgs)	Kennedy/Jenks
RM 3.8_1600 S Henderson St_west bank	19	3.8	Supplemental Laboratory Testing	figures/logs	09.20.1984	South Park Site: 1600 S. Henderson St.	7 boring logs	Dames & Moore
RM 4.25_Delta Boat Lift Pier_west bank	20	4.25	Limited Geotechnical Engineering Report	report	5.8.2002	Boat Lift Pier 1608 S 96th Street	1 bore hole, two grain size, 200-wash analysis, Atterberg limits	AMEC
RM_4.4_Duwamish Substation_west bank	21	4.4	Geotechnical Report Duwamish Substation Bank 79 Foundation Retrofit	report	2.28.2003	Bank 79 Transformer: (near west marginal way)	1 PCPT, 2 geophysical surveys, 3 soil borings and analysis, borings completed for MWs	Earth Technology Corporation
RM_4.4_Duwamish Substation_west bank2	22	4.4	n/a	figures/logs	10.07.1969	Duwamish Substation	47 borings (logs with coordinates)	Seattle Engineering Department
Draft Duwamish Substation Geotech Rpt	23	4.45	Draft Geotechnical Report Seattle Substation Evaluation	draft report	11.2012	Duwamish Substation	Surface/subsurface conditions, environmentally critical areas, seismic considerations, foundations, earthwork	Seattle Public Utilities Geotechnical Engineering
RM 4.4-4.6_Boeing_east bank	24	4.4-4.6	Boeing Developmental Center Logs	figures/logs	2.1.2001	East Marginal Way South (Boeing Developmental Center)	MW well as-builts, site map, lithology logs (about 30 wells)	Landau Associates
USACE Dredging 2018	25	4.0-4.7	Memorandum For Record: DMMP Suitability Determination	report	05.24.2018	Duwamish River: Stations 242+00 and 275+56 (turning basin and navigation channel)	Vibracore samples (grain size/conventional) page 18	USACE
RM 4.6-7.7_Hwy 99_west bank	26	4.6-7.7	Report on Geotechnical Exploration	report	05.30.1985	Renton Effluent Transfer System. West Marginal Way Southwest, extending from about 1,500 south of South 102nd Street to 800 feet north of Des Moines Way South	Plan and profile maps, 21 exploration borings, trench excavation, chemical testing, GW conditions, geotechnical impacts	Converse Consultants
RM 5_Oxbow bridge	27	5.0	Geotechnical Design Report	report	4.1988	North Oxbow Bridge, Boeing Developmental Center	Surface/subsurface conditions, SPTs, GW, seismic considerations, vertical/lateral pile capacity, liquefaction potential, excavation	Rittenhouse-Zeman & Associates
RM +5_Boeing Oxbow Parking Lot_west bank	South of study area	5.1	Report of Geotechnical Investigation	report	7.23.1985	Boeing Developmental Center Oxbow Parking lot (west side Duwamish)	2 CPT, 5 borings, deepest boring 54.0 ft	Converse Consultants
LDW-Final-FS-Sections-8- 13_october-31-2012_ADA	n/a	n/a	Lower Duwamish Waterway Final Feasibility Study (sections 8-13)	report	10.2012	Duwamish River	Table 8-6: prior geotechnical analyses from projects in the LDW, around Harbor Island, and adjacent Elliott Bay	LDWG
LDW-Final-FS-Sections-1- 7_october-31-2012_ADA	n/a	n/a	Lower Duwamish Waterway Final Feasibility Study (sections 1-7)	report	10.2012.	Duwamish River	Section 2.6: additional considerations, sediment physical properties: grain size, Atterberg limits, TOC, porosity, bulk density, etc.	LDWG

File Title	Identification No. <sup>1</sup>	River Mile	Document Title	Document type	Date Document Creation	Project Location	Sample Types/Report Info	Author
Final_LDW-RI	n/a	n/a	Lower Duwamish Waterway Remedial Investigation Report	report	7.9.2010	Duwamish River	Section 2.5.4: sediment lithology: geotechnical parameter tests and results (moisture, specific gravity, Atterberg limits, bulk density, porosity).  Also physical properties. Section 9.1.6: bank erosion	LDWG
2015_11_POS_Silver_DSR_Ecology	28	3.8	Boeing Isaacson-Thompson Site, Port of Seattle Sliver Data Summary Report	report	11.12.2015	Port of Seattle Sliver Property located west of the Boeing Isaacson Property	10 soil borings (direct push) to 25 ft bgs. 41 soil samples collected. No geotechnical analysis. Includes section on lithologic conditions of site and borings logs, page 5.	Kennedy/Jenks Consultants
Boeing_I- T_Landau_042114_Final_RI	29	3.8	Final Remedial Investigation Report Boeing Isaacson- Thompson Site	report	4.21.2014	Boeing Isaacson-Thompson Site	No geotechnical analysis. Descriptions of Geologic Conditions on page 107. Discuss soil conditions at 50 exploratory locations. Summary of depth to alluvium documented in Table 9 page 290	Landau Associates, AMEC
AppJ_Basin of Design Report_08162012	30	3.5 - 3.7	Appendix J Geotechnical Basis of Design Report (Terminal 117 Cleanup Design Sediment and Upland Areas)	report	8.1.2012	Port of Seattle, Terminal 117	Six borings and 8 CPTs. 3 completed on barge, 3 completed upland. 5 SPTs completed on barge, 3 completed in upland (locations figure 1 page 23). Geologic soil units described page 10.  Engineering soil properties section 3 page 14.  Subsurface profile figures begin page 25.	Crete Consulting, Jacobs Associates
2012_12-19_Final Shoreline Investigation	31	4.1-4.2	Shoreline Soil and Groundwater Characterization Report	report	3.12.2012	Former Rhone-Poulenc Site, Tukwila Washington: 9229 East Marginal Way	15 direct push upland borings for soil/GW from shoreline areas. 5 areas collected geotechnical samples between 11 and 15 feet. Section 3.1 soil lithology (page 14). Section 3.5 geotechnical analysis (moisture, density, grain size, atterberg). Results table 8 page 43. Geotech locations figure 3 page 47.	AMEC
Final Interm Measures Contruction Work Plan V1/V2	32	4.1-4.2	Final Interm Measures Contruction Work Plan V1/V2	report	10.25.2002	Former Rhone-Poulenc Site, Tukwila Washington: 9229 East Marginal Way	Samples to confirm depth and characterisics of uppermost aquitard. CPTs for soil strength at 3 locations alongside borings GT-5, B-1-02, B-7-02 (Section 2.4 Geotech Characterization page 15). Figures page 21. Table 2-1 summarizes analytical. V2: Appendix B: Geotechnical Data	URS
2021.03.05 Figures AppA-1_B- Boeing DC Thompson Geotech Report-01052021_Final_reduced	33	3.7; 4.6; 4.9	Boeing DC Thompson Geotech Report	figures/logs	1.5.2021	Boeing Thompson Site	3 CPTs at Thompson site; 3 CPTs at Boeing Development Center; 3 CPTs near Norfolk outfall	Golder
8801 Final FS July 27, 2020	34	3.9-4.0	Final Feasibility Study 8801 East Marginal Way S., Tukwila, Washington	report	7.27.2020	Centerpoint Properties	Geologic cross sections perpendicular and parallel to the river bank through Centerpoint Properties	Shannon & Wilson

#### Notes:

1. The study identification number is shown on Maps 5-2a and 5-2b. Studies with "n/a" in this field are site-wide studies.

CPT: cone penetration testing
DMMP: Dredged Material Management Program

GW: groundwater

HSA: hollow stem auger

LDW: Lower Duwamish Waterway

MW: monitoring well

n/a: not applicable RFI: request for information RI: remedial investigation RM: river mile SPT: standard penetration test USACE: US Army Corps of Engineers