Figure A-1. Probability of deposition for cohesive sediment using the Krone formulation.
Figure A-2. Probability of deposition for non-cohesive sediment as a function of bed shear stress and particle diameter.
Figure A-3. Settling speed of discrete sediment particles as a function of particle diameter.
Figure A-4. Probability of suspension as a function of bed shear stress for particle diameters of 130 and 540 µm.
Particle shielding factor is calculated as: $S_k = (d_k/d_m)^{0.85}$, when $d_k < d_m$, otherwise set $S_k = 1$.

where $d_k = \text{particle size}$, $d_m = \text{mean particle diameter}$. 

**Figure A-5. Particle shielding factor as a function of particle size**
Figure A-6. Schematic of interactions between the water column, active layer, and parent-bed layer when the active-buffer layer is present.
Figure A-7. Schematic of interactions between the water column, active layer, and parent-bed layer when the active-buffer layer is not present.
Figure A-8. Initial structure of bed with no active-buffer layer at time = $t_1$. 
Figure A-9. Active-surface layer thickness increases as shear stress increases ($\tau_2 > \tau_1$) at time $= t_2$. 
Figure A-10. Active-surface layer thickness decreases and active-buffer layer is created as shear stress decreases ($\tau_3 < \tau_2$) at time = $t_3$. 
Figure A-11. Active-surface layer thickness decreases and active-buffer layer thickness increases as shear stress continues to decrease ($\tau_4 < \tau_3$) at time = $t_4$. 
Figure A-12. Active-surface layer thickness increases and active-buffer layer thickness decreases as shear stress increases ($\tau_5 > \tau_4$) at time = $t_5$. 
Figure A-13. Active-surface layer thickness increases and active-buffer layer is destroyed as shear stress increases ($\tau_6 > \tau_5$, $\tau_6 > \tau_2$) at time $= t_6$. 
Figure A-14. Active-surface layer thickness decreases and new active-buffer layer is created as shear stress decreases ($\tau_7 < \tau_6$) at time $= t_7$. 
Figure A-15. Initiation of motion and suspension for a current over a plane bed, $\Theta = f(D_*)$, from Van Rijn (1989).
Figure A-16: Critical shear stress for initiation of suspended and bed load transport as a function of particle diameter.